



- (I) Progress in humidity time lag experiments
- (II) Use of ground check results in RS41 GDP

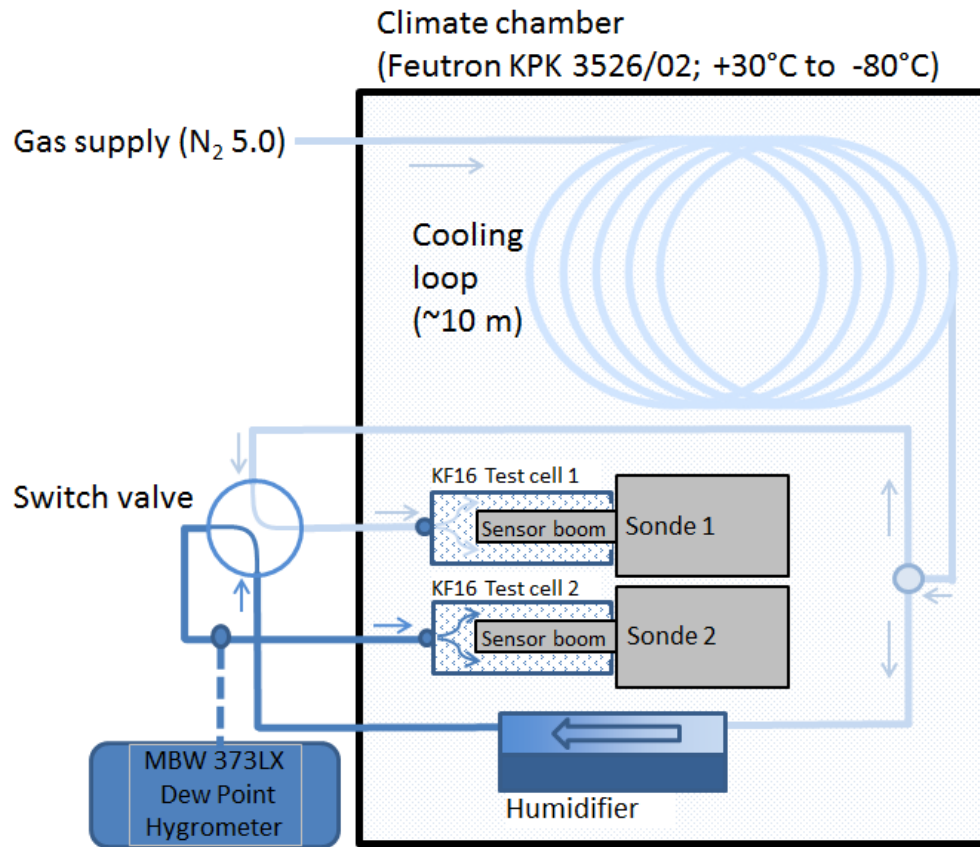
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**Michael Sommer, Tatjana Naebert, Rico Tietz**

13<sup>th</sup> GRUAN Implementation and Coordination Meeting (ICM-13)  
15-19 November 2021

# (I) Time-lag: Objective

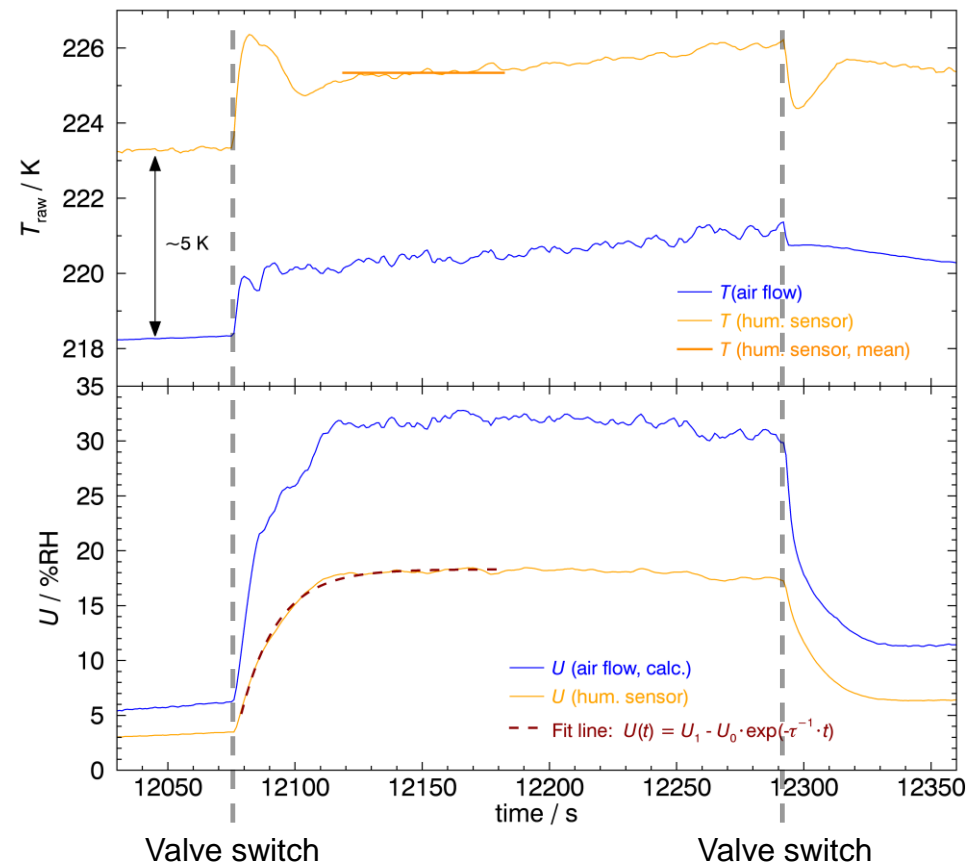
- Slow Response time of humidity sensor at low  $T$  causes systematic error (smoothing + time lag)
- Approach:
  - Design of laboratory experiment for direct time-lag quantification:
    - Measure response to step-like change in rel. humidity at various  $T$ -levels,
    - Read time constant  $\lambda$  (or 63%-time  $\tau = 1/\lambda$ ) from response curves by fitting  $U(t) = U_1 - \Delta U \cdot \exp(-\frac{t}{\tau})$
  - Parameterise response time  $\tau(T)$
  - Apply correction of time lag in processing

# (I) Time-lag: Setup (2015)



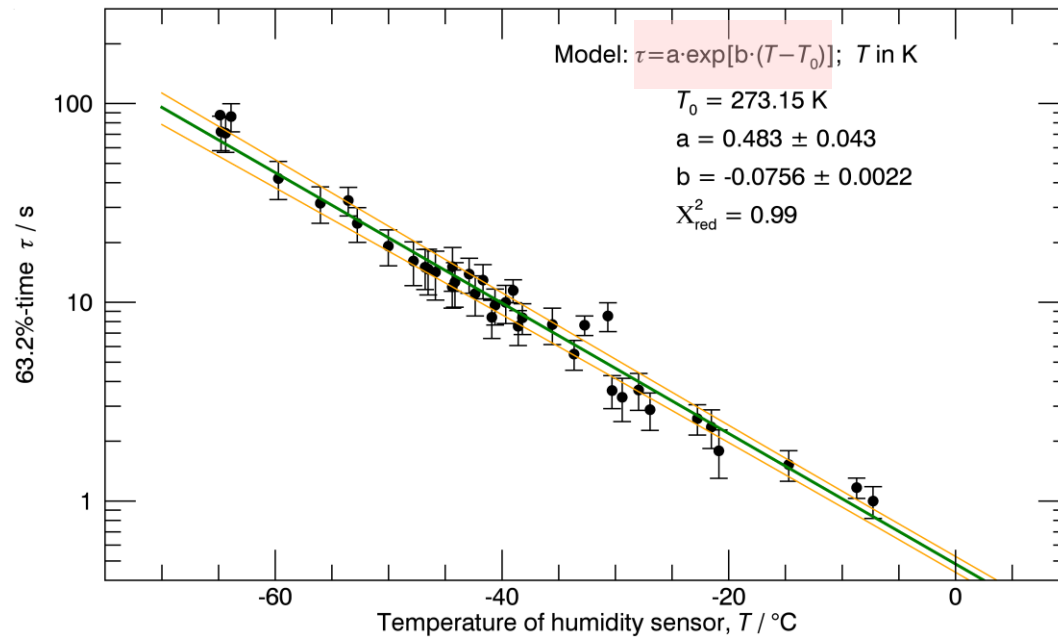
- RS41  $U$ -sensor heated  $\sim 5$  K

$\tau$  derived for 'internal'  $U$   
and related to 'internal'  $T$  of  $U$ -sensor



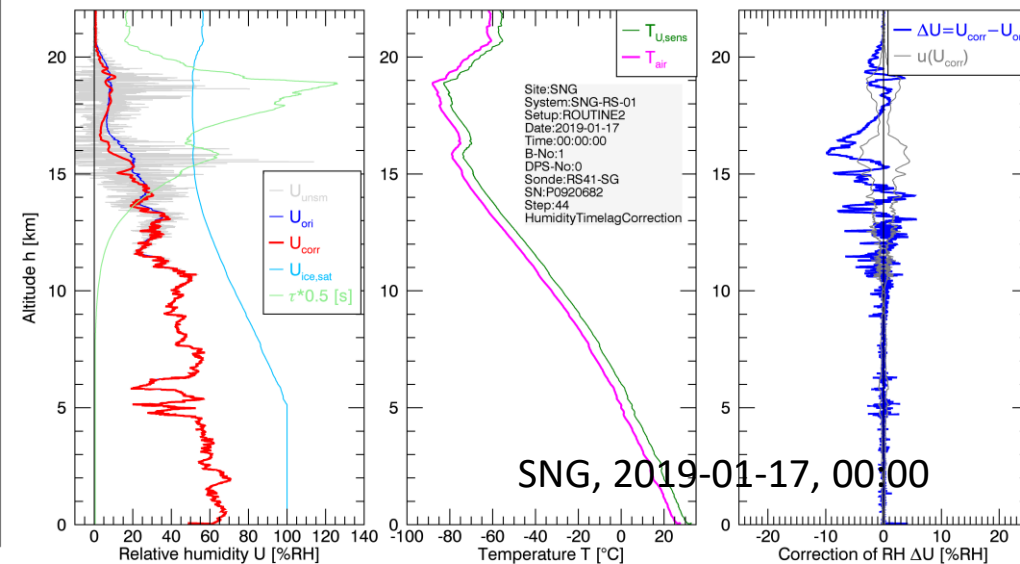
# (I) Time-lag: Results (2015)

- Parameterization  $\tau(T)$ , based on re-evaluated measurements of 2015



- Correction, implemented in RS41-GDP.1

$$\Delta U_i = U_{i,c} - U_{i,m} = \sum_{j=0}^{i-1} (U_{i,m} - U_{j,c}) \exp\left(\frac{t_j - t_i}{\tau_i}\right)$$



Reliable results, but still some issues to be resolved:

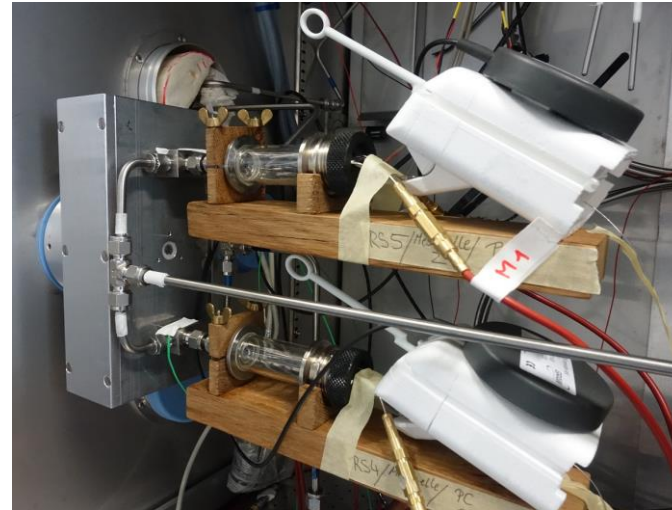
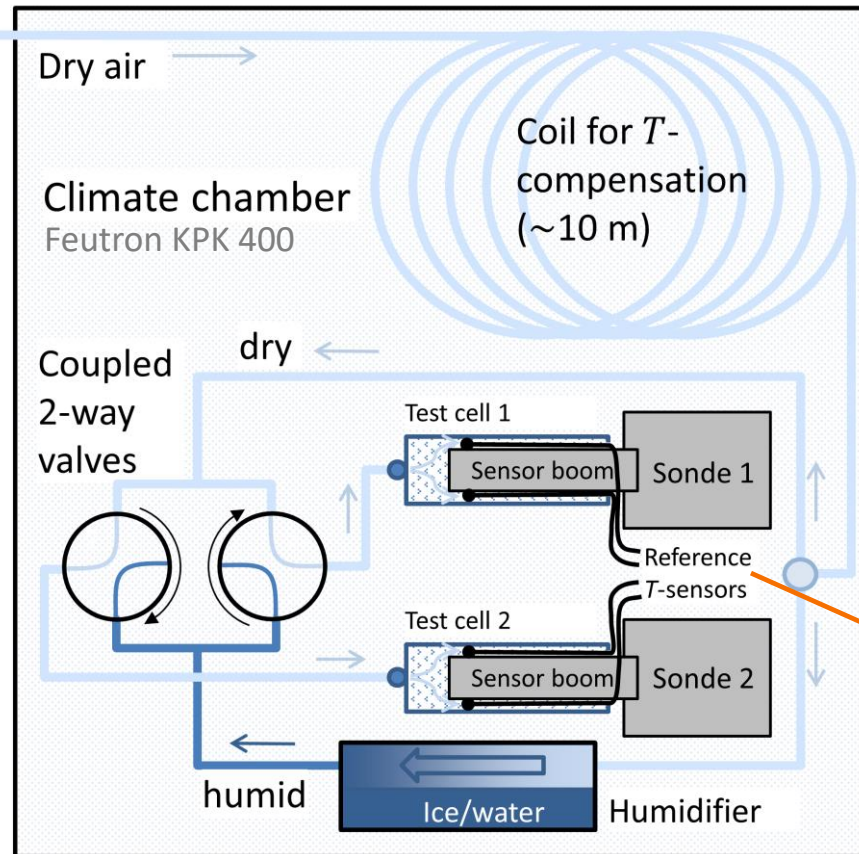
- $T$ -stability
- Small step size (efficiency of humidifier)
- Only dry-to-humid steps evaluated
- Scatter

# (I) Time-lag: Improved setup (2021)

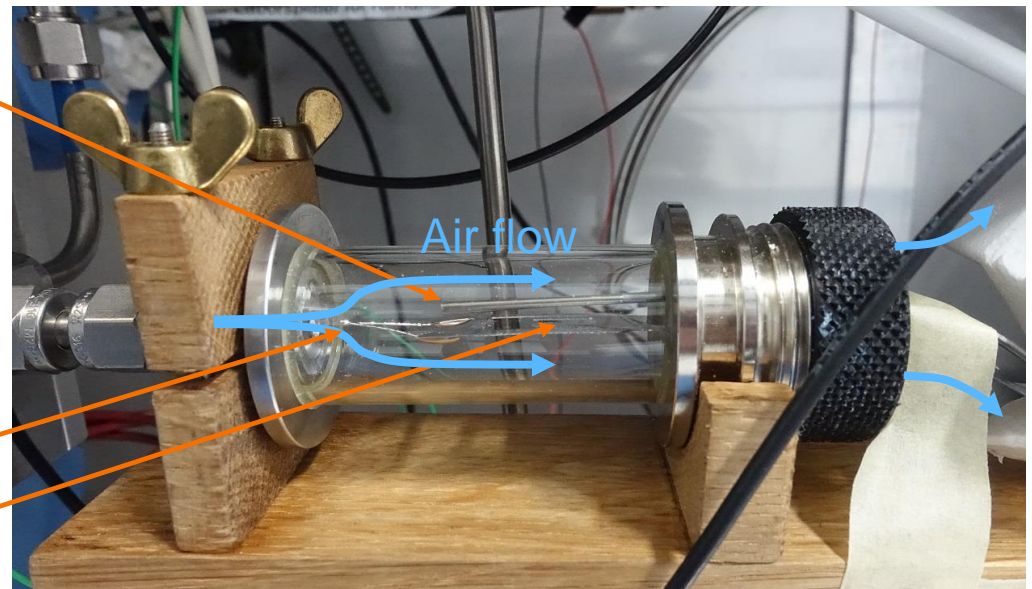
- New cell design (optimised size, visual control)
- Arrangement of all components including switch valve inside the chamber
- Automated  $T$ -programme: discrete  $T$  levels ( $-74\text{ °C} \dots +20\text{ °C}$ )
- Simultaneous tests in two cells with parallel switching in the same direction
- High  $T$ -stability during steps ( $\sim 0.2\text{ K}$ )
- Larger  $U$ -steps (more efficient humidifier)
- Evaluation of both up and down humidity steps



# (I) Time-lag: Improved setup (2021)



(Example foto  
Graw DFM-17)

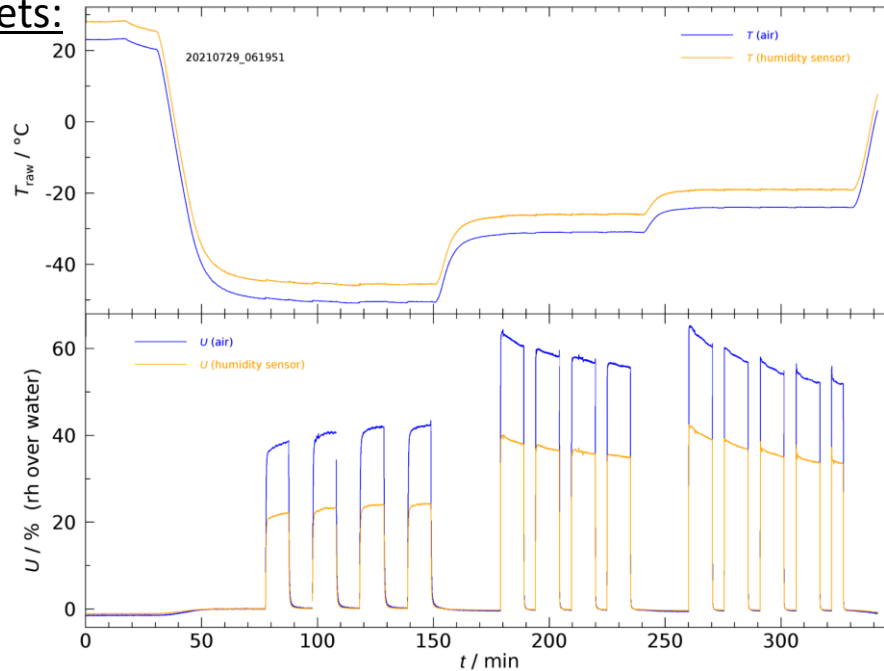


$T$ -sensor sonde

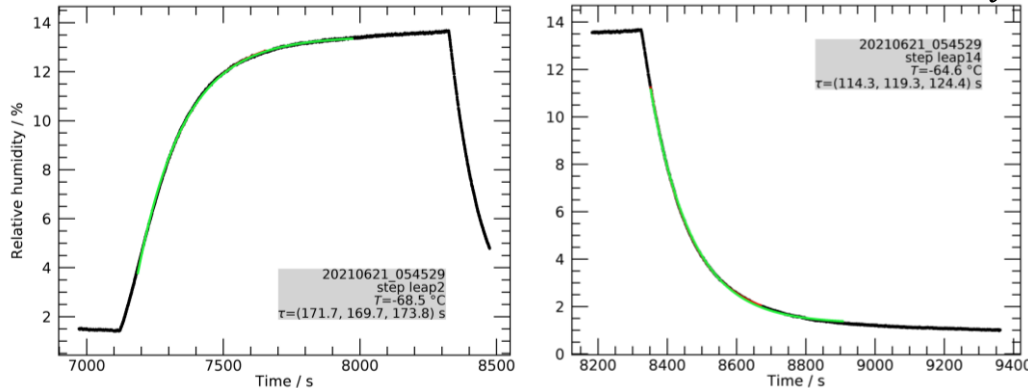
$U$ -sensor sonde

# (I) Time-lag: Improved setup (2021)

## Data sets:

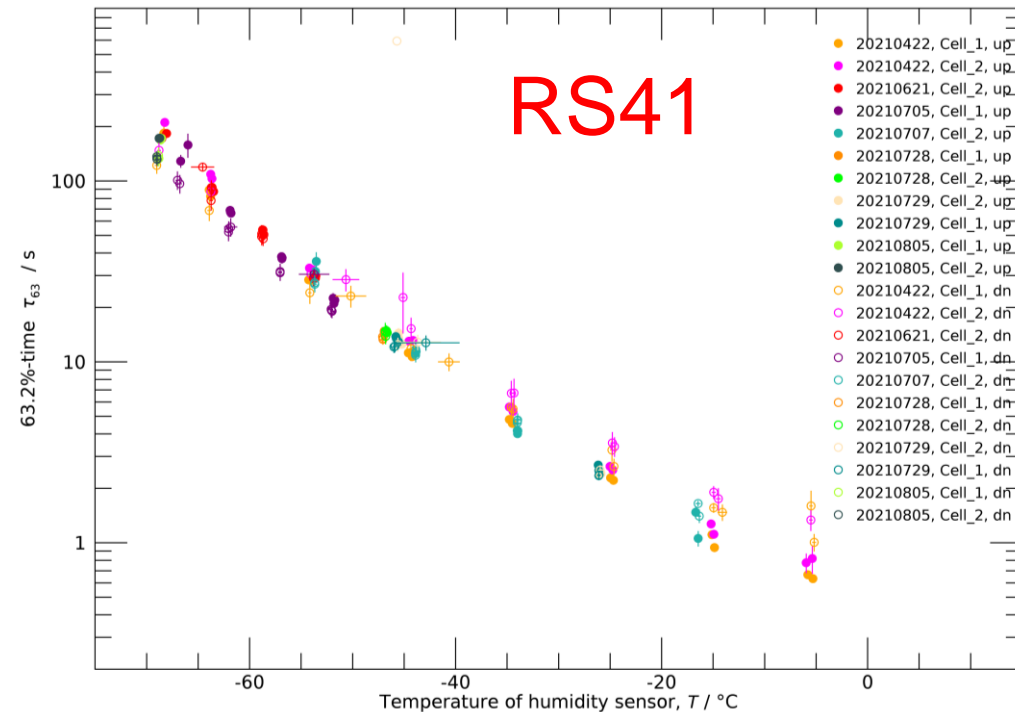


T-determination: fitting of  $U(t) = U_1 - \Delta U \cdot \exp(-\frac{t}{\tau})$



## Results (Preliminary):

- Good reproducibility, consistent overall picture, 2015-measurements essentially confirmed
- Further evaluation ongoing:
  - Small systematic differences up/down steps,
  - $\tau(T)$  not purely exponential with low  $T$  (?)
  - uncertainty estimates



# (I) Time-lag: Conclusions

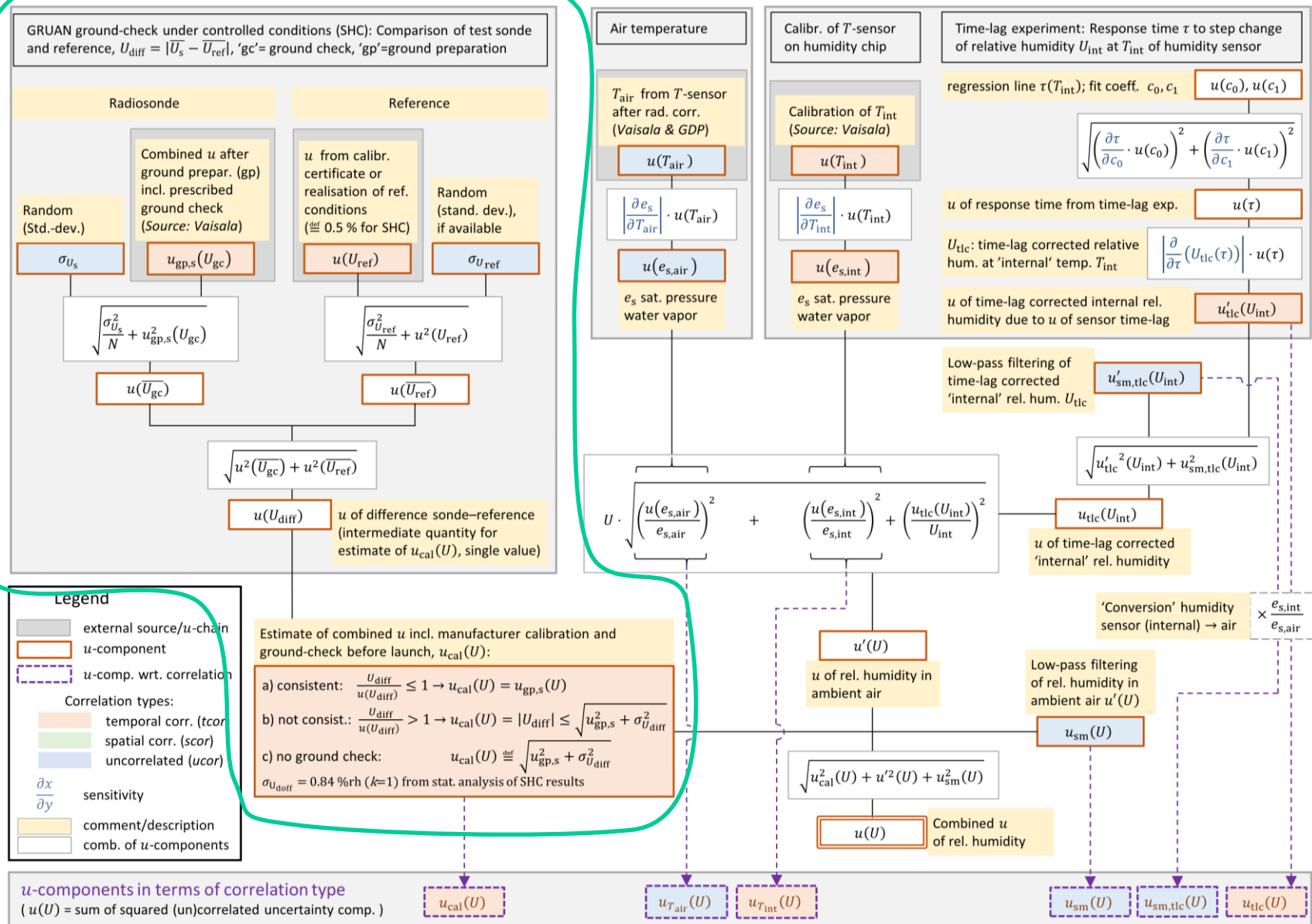
- Current status:  
RH time-lag correction in actual RS41-GDP.1 based on re-analysis of existing data (2015) measured with 'old' setup
- 2021: substantial technical improvements, new measurements
- Evaluation of new RS41 results ongoing, implementation of updated time-lag correction in next version (RS41-GDP.2)
- Setup 'ready' for measurements with other radiosonde models;  
First data for Graw DFM17 and Vaisala RS92 available;  
Use in laboratory part of WMO intercomparison campaign (UAI-2022)



## (II) GRUAN ground check: Objective

- GRUAN recommends routine manufacturer-independent ground check (GC) of physical sensors ( $U$ ,  $T$ ,  $p$ )
- GC should be performed after the manufacturer-prescribed GC as part of ground preparation procedure
- Motivation: check of manufacturer calibration, estimate of GC-related uncertainty
- Procedures explained here for the actual RS41 processing, but applicable to any radiosonde model

# (II) Ground check Relative humidity



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1. **Manufacturer-GC (RI41):**  
Reconditioning, check against 0 % by sensor heating,  
→ Pre-launch  $u$ :  $u_{gp,s}(U)$  (Vaisala), see Figure
2. **GRUAN-GC, in SHC:**  
Measure  $\Delta U_{SHC} = |\overline{U}_s - U_{ref,100}|$  in 100 % RH  
environment for  $\sim 3$  min, assign uncertainty  $u(\Delta U_{SHC})$

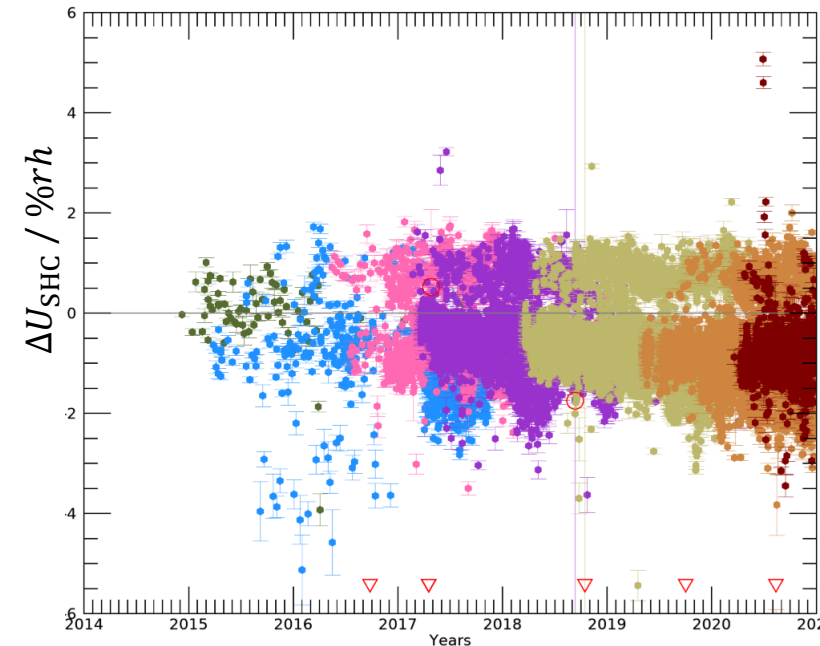
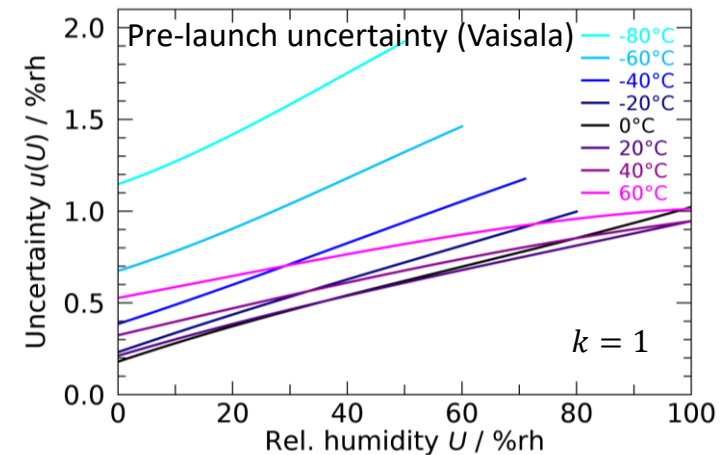
No correction applied, use GRUAN GC-result to assign **overall pre-launch-uncertainty**  $u_{cal}(U)$ :

- $\frac{|\Delta U_{SHC}|}{u(\Delta U_{SHC})} \leq 1$ : **consistency**,  $u_{cal}(U) = u_{gp,s}(U)$
- $\frac{|\Delta U_{SHC}|}{u(\Delta U_{SHC})} > 1$ :  $u_{cal}(U) = |\Delta U_{SHC}|$ ,

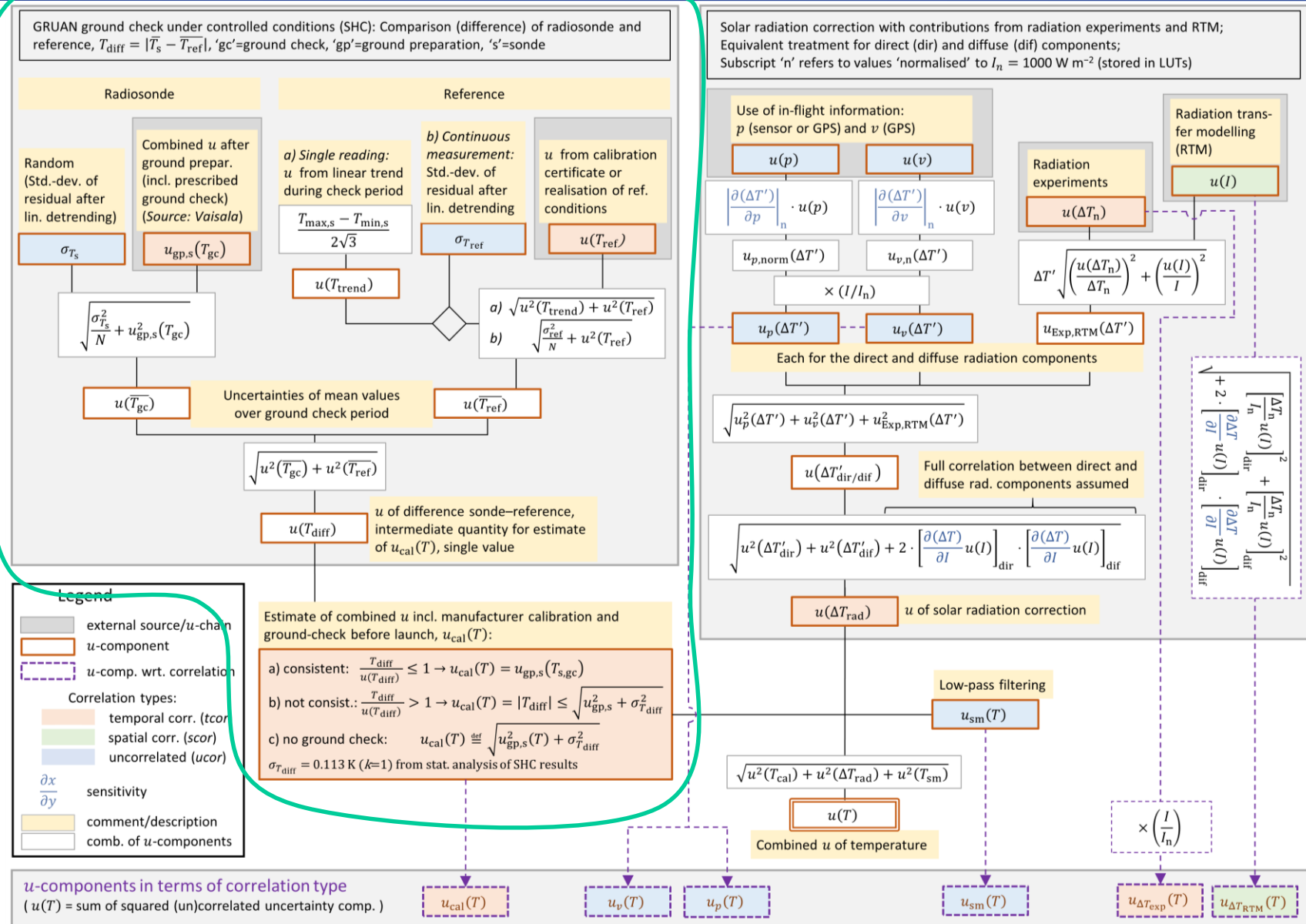
with upper limit  $u_{cal}(U) \leq \sqrt{u_{gp,s}^2(U) + \sigma_{\Delta U}^2}$ , and

$\sigma_{\Delta U}^2 = 0.84$  %rh the standard deviation of the mean of existing GRUAN-GC results ( $N=23271$ )

If no SHC-GC available: Set  $u_{cal}(U) = \sqrt{u_{gp,s}^2(U) + \sigma_{\Delta U}^2}$



# (II) Ground check Temperature



# (II) Ground check Temperature

1. **Manufacturer-GC (RI41):**  
Functionality check  
(no comparison to reference, no correction applied)  
→ Pre-launch  $u$ :  $u_{gp,s}(T)$  (Vaisala), see Figure
2. **GRUAN-GC in SHC (in parallel with  $U$ -check):**  
Measure  $\Delta T_{SHC} = |\bar{T}_s - T_{ref}|$  with uncertainty  $u(\Delta T_{SHC})$

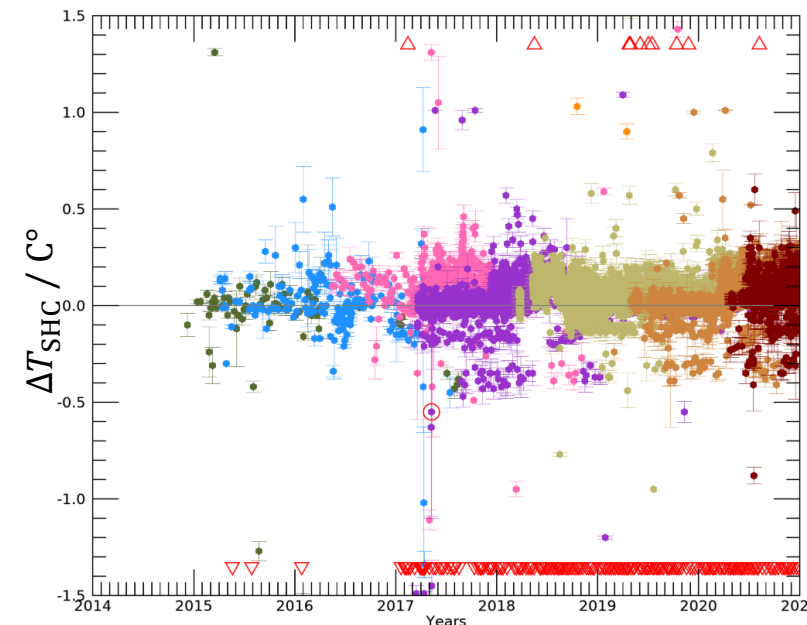
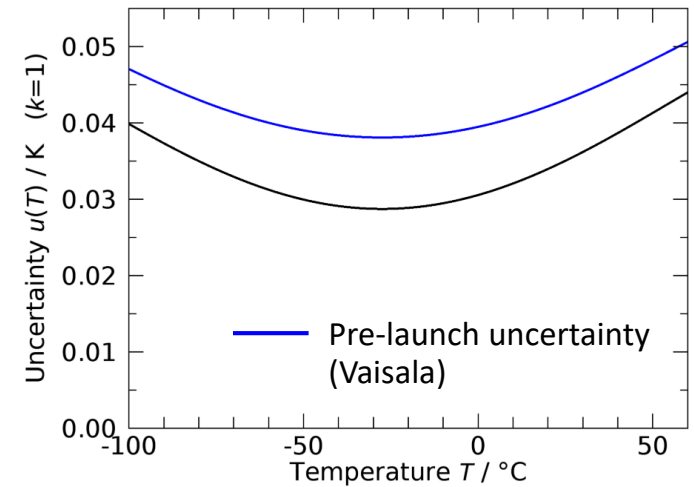
No correction applied, use GRUAN GC-result to assign **overall pre-launch-uncertainty**  $u_{cal}(T)$ :

- $\frac{|\Delta T_{SHC}|}{u(\Delta T_{SHC})} \leq 1$ : **consistency**,  $u_{cal}(T) = u_{gp,s}(T)$

- $\frac{|\Delta T_{SHC}|}{u(\Delta T_{SHC})} > 1$ :  $u_{cal}(T) = |\Delta T_{SHC}|$ ,

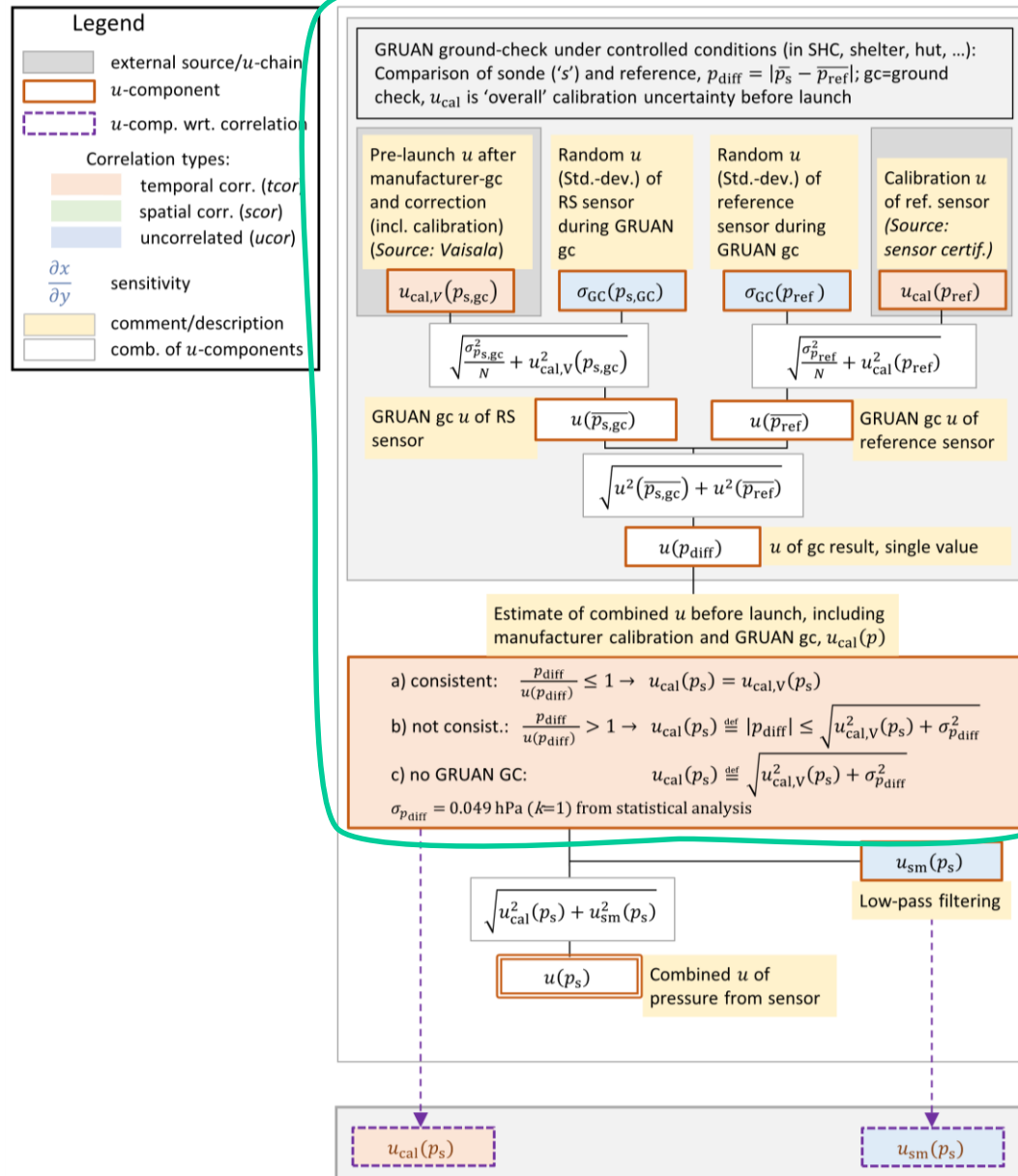
with upper limit  $u_{cal}(T) \leq \sqrt{u_{gp,s}^2(T) + \sigma_{\Delta T}^2}$ , and  
 $\sigma_{\Delta T}^2 = 0.113^2$  K the standard deviation of the mean of  
existing GRUAN-GC results ( $N=9269$ )

If no SHC-GC available:  $u_{cal}(T) = \sqrt{u_{gp,s}^2(T) + \sigma_{\Delta T}^2}$





# (II) Ground check Pressure (RS41-SGP)



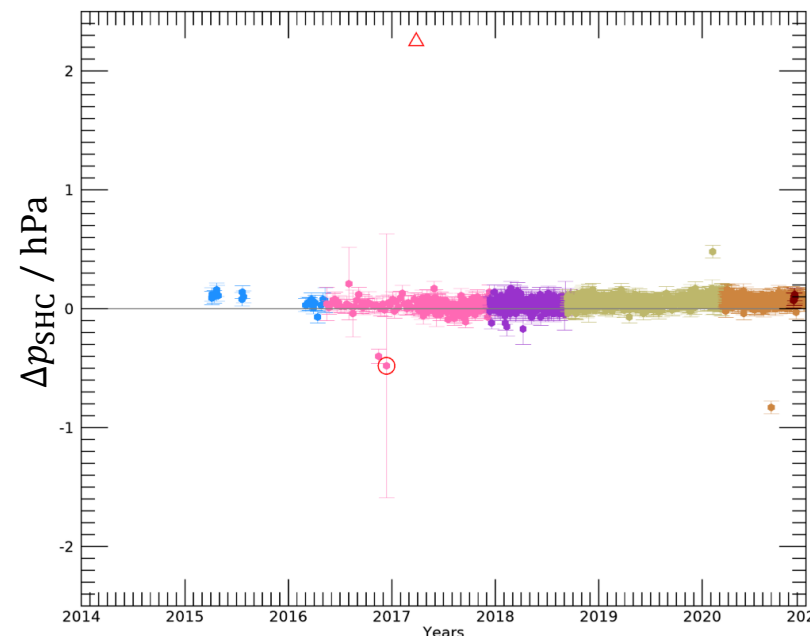
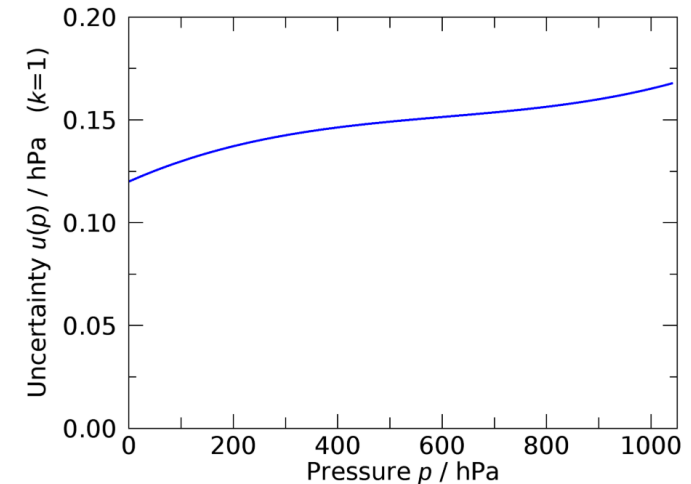
# (II) Ground check Pressure (RS41-SGP)

1. **Manufacturer-GC (RI41):**  
Comparison with ref. barometer (RI41-B or station barometer), correction factor applied,  
→ Pre-launch uncertainty  $u_{\text{cal},V}$  (Vaisala), see Figure
2. **GRUAN-GC under controlled conditions**  
(e.g. in SHC in parallel with  $U$ -check):  
Measure  $\Delta p = |\bar{p}_s - p_{\text{ref}}^{\text{GRUAN}}|$  with uncertainty  $u(\Delta p)$

Assign **overall pre-launch-uncertainty**  $u_{\text{cal}}(p)$ :

- $\frac{|\Delta p|}{u(\Delta p)} \leq 1$ : **consistency**,  $u_{\text{cal}}(p) = u_{\text{cal},V}(p)$
- $\frac{|\Delta p|}{u(\Delta p)} > 1$ :  $u_{\text{cal}}(p) = |\Delta p|$ ,  
with upper limit  $u_{\text{cal}}(p) \leq \sqrt{u_{\text{cal},V}^2(p) + \sigma_{\Delta p}^2}$ ,  
and  $\sigma_{\Delta T}^2 = 0.049 \text{ hPa}$  ( $N=23271$ )

If no GRUAN-GC available:  $u_{\text{cal}}(T) = \sqrt{u_{\text{cal},V}^2(p) + \sigma_{\Delta p}^2}$



## (II) Ground check: Conclusions

- GRUAN recommends independent ground check of  $U$ ,  $T$ ,  $p$  as part of pre-launch procedures
- Currently only practicable at manually operated stations
- Presented approach for use of ground check results accounts for missing checks (lack of information) by adding an uncertainty component
- Approach is transferrable to any other ground check environment