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# Upper-air simulator to evaluate the radiation correction and measurement uncertainty of RS41

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ICM-13 online

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# Significance of radiosonde measurement

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- ❑ Accurate method to **monitor the long-term climate change** in stratosphere
  - ◆ Temperature is the direct index of global warming
- ❑ Practical tool to gather climate variables for the **weather forecasting** in troposphere
- ❑ Serve as a **Reference to other remote skills** such as satellite
- ❑ Sounding sites more than 1000 sites
  - ◆ National observatories
  - ◆ Military bases, etc
  - ◆ Institutes & universities for research



# Radiosonde meets ...

**High solar irradiance  $\sim 1360 \text{ W/m}^2$**

**Low pressure down to a few hPa**

**Upward air ventilation  $+5 \text{ m/s}$**

**Low temperature below  $-70 \text{ }^\circ\text{C}$**

**Requiring accurate test method based on international agreement**

# Conditions for test method

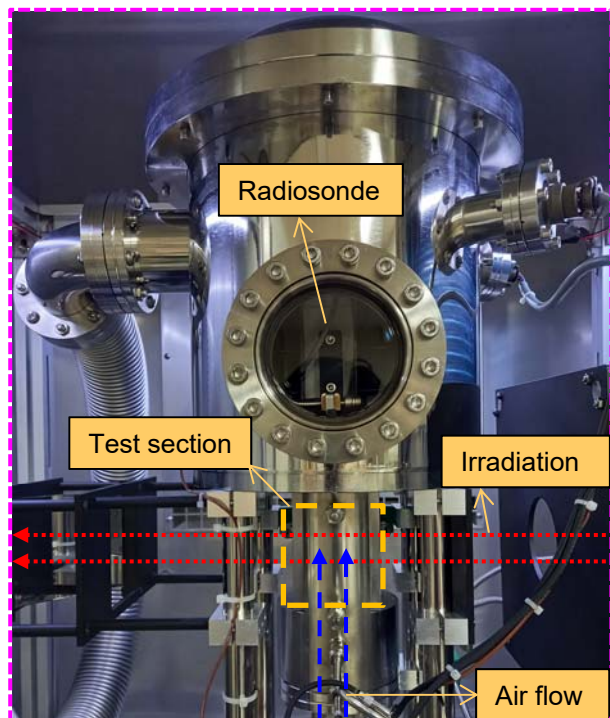
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- Guide to Meteorological Instruments and Methods of Observation (WMO-No.8)
  - ◆ Chapter 12, MEASUREMENT OF UPPER-AIR PRESSURE, TEMPERATURE AND HUMIDITY
    - “The calibration methods **used by manufacturers** should be identified before purchasing radiosondes.”
    - **Stability** condition of  $\pm 0.2$  hPa/min for pressure,  $\pm 0.25$  K/min for temperature and  $\pm 1$  relative humidity per minute
    - **Errors** less than  $\pm 0.2$  hPa for pressure,  $\pm 0.1$  K for temperature and  $\pm 1\%$  relative humidity

**There is no detailed descriptions on the implementation of calibration setups/methods**

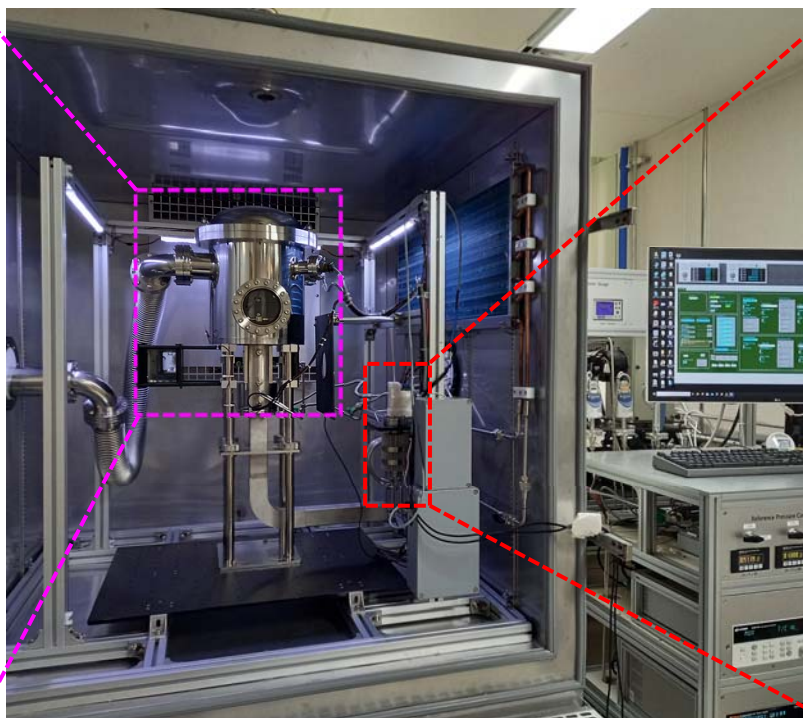
# Upper air simulator (UAS) at KRISS

- Radiation correction of temperature sensors
  - ◆ Control of temperature, pressure, ventilation, and irradiance
- Calibration of humidity sensors
  - ◆ Control of temperature and humidity

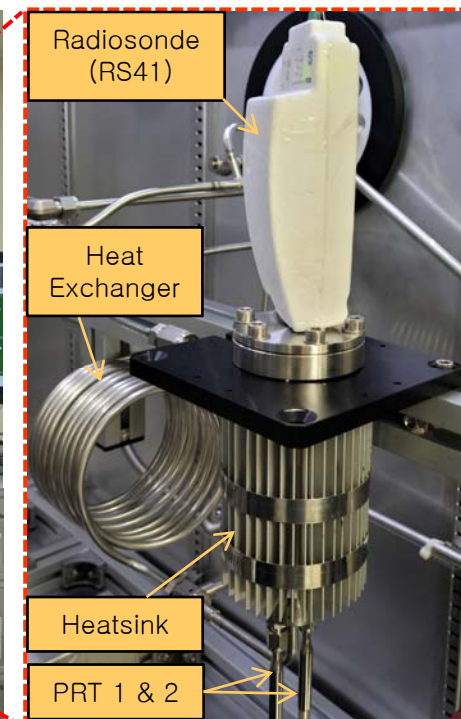


<Radiation correction setup>

Lee *et al.* Meteorol. Appl. **27**, e1855 (2020)



<Upper air simulator>



<Humidity calibration setup>

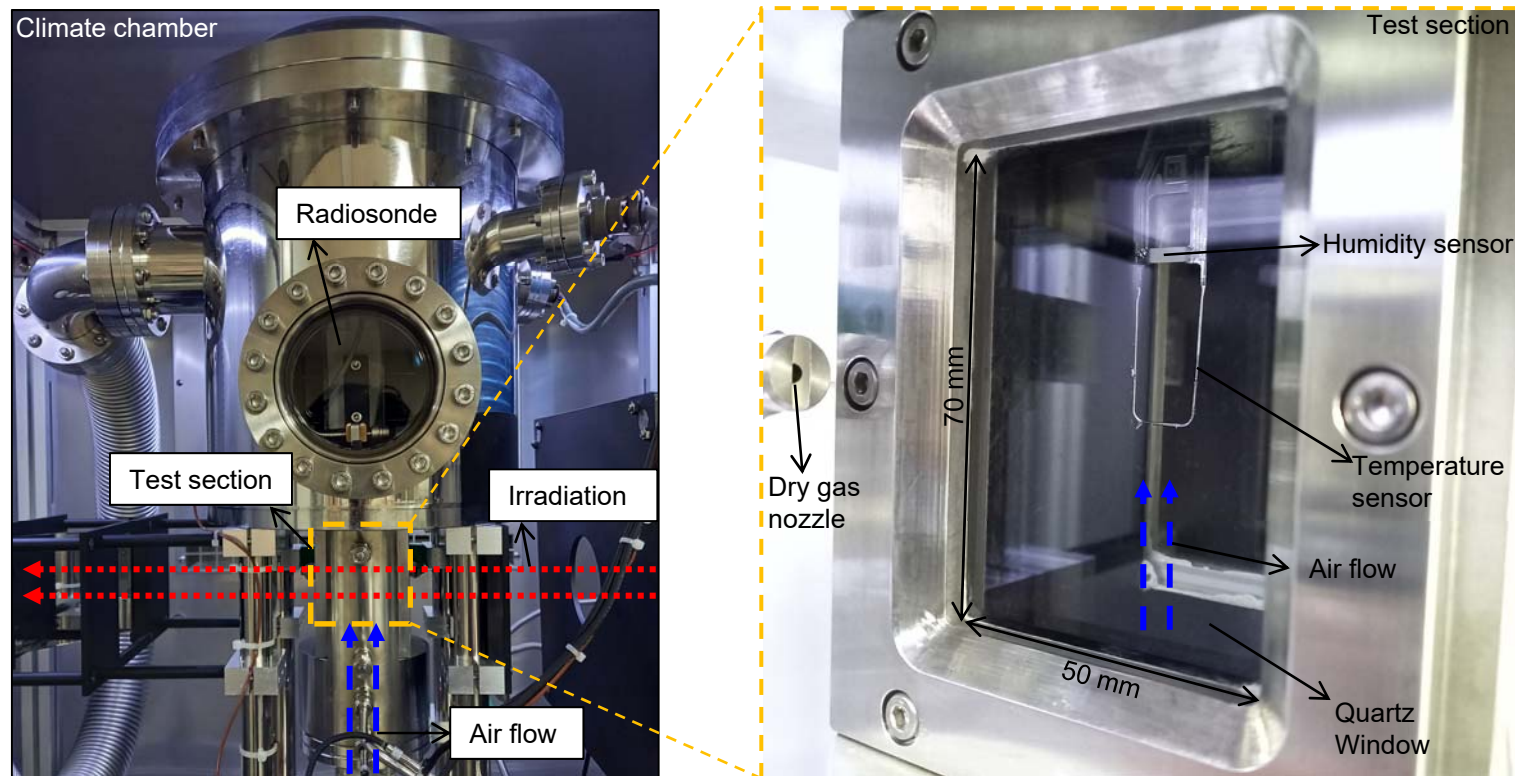
Lee *et al.* Meteorol. Appl. **28**, e2010 (2021)



# Radiation correction setup

## □ Environmental factors affecting radiation correction

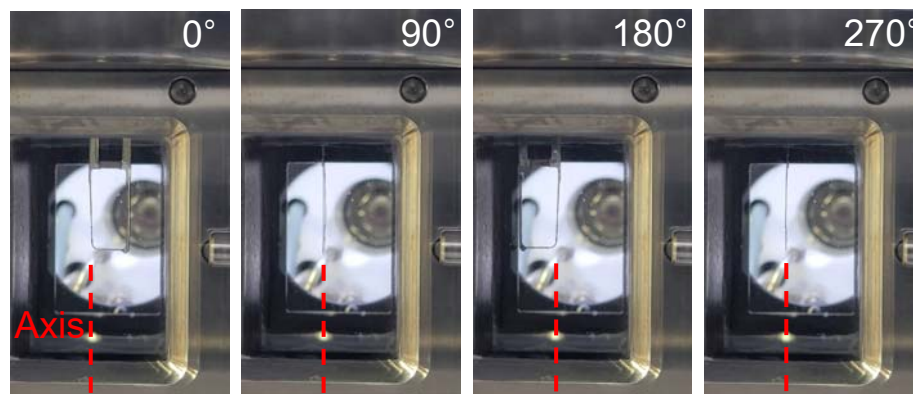
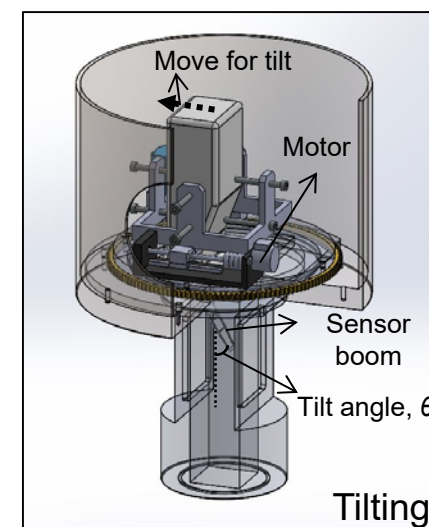
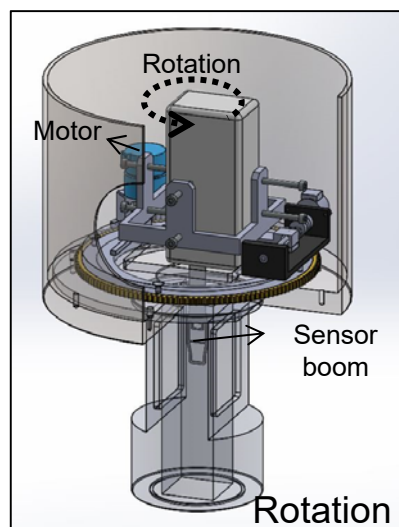
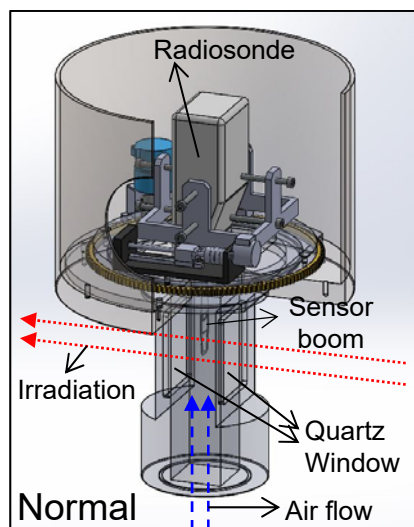
- ◆ Temperature ( $T = -70\text{--}20\text{ }^{\circ}\text{C}$ ) by climate chamber
- ◆ Air pressure ( $P = 5\text{--}500\text{ hPa}$ ) & Ventilation ( $v = 4\text{--}7\text{ m/s}$ ) by sonic nozzles
- ◆ Irradiance ( $S_0 = 1000\text{ W/m}^2$ ) by solar simulator



# Rotation & Tilting of radiosonde

## □ Simulation of movement of radiosonde in sounding

### ◆ Rotation (5, 10, 15 s) & Boom tilting (27 °)

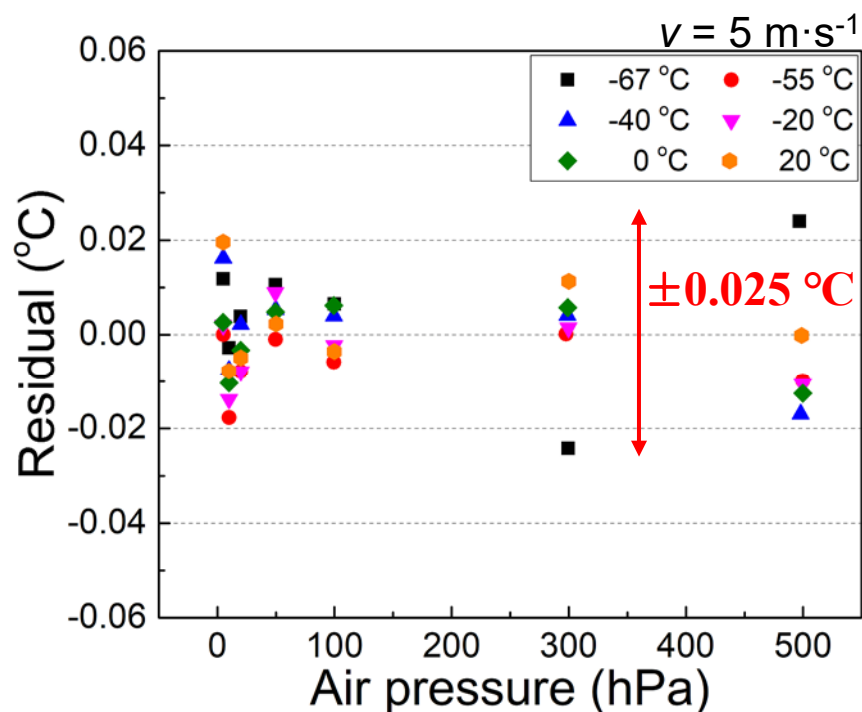
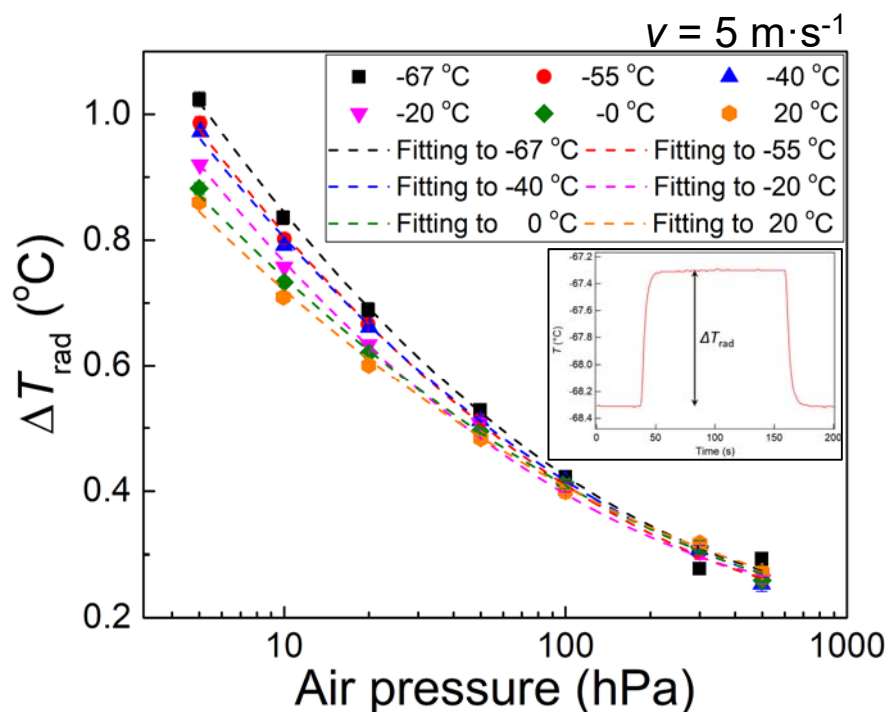


Rotation axis =  
Temperature sensor

# Pressure effect

## □ Convective cooling

- ◆ Radiation correction ( $\Delta T_{\text{rad}}$ ) decreases as air pressure ( $P$ ) increases
- ◆ Air density  $\uparrow$  at high  $P \rightarrow$  Convective cooling  $\uparrow$



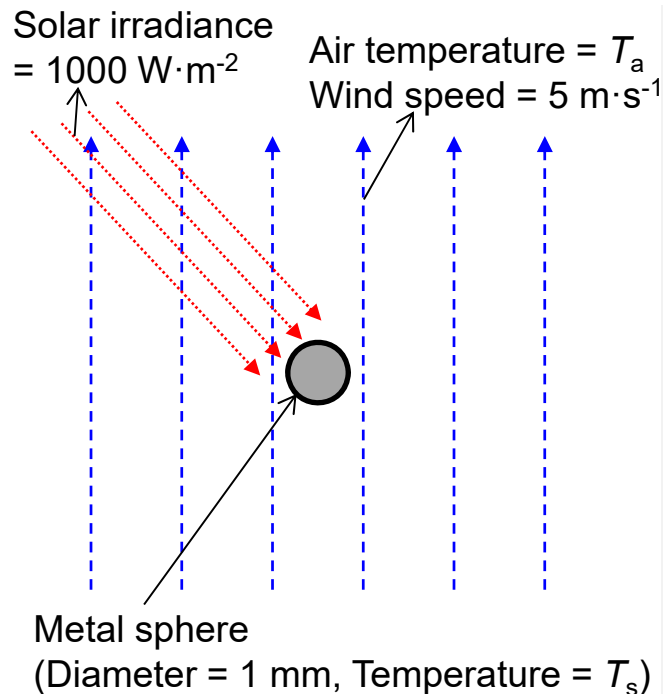
$$\Delta T_{\text{rad}} = A_0(T) + B_0(T) \cdot \log(P) + C_0(T) \cdot [\log(P)]^2 \text{ for } 5 \text{ hPa} \leq P \leq 500 \text{ hPa}, S_0 = 980 \text{ W} \cdot \text{m}^{-2}$$



# Theoretical understanding

## □ Heat transfer calculation

◆ Metal sphere is modelled as a temperature sensor



$$\alpha S = h(T_s - T_a), \quad h = \frac{k}{D} \left[ 2 + \left( 0.4Re^{\frac{1}{2}} + 0.06Re^{\frac{2}{3}} \right) \left( \frac{\mu C_p}{k} \right)^{\frac{2}{5}} \right]$$

$\alpha$  = absorptivity of the metal sphere

$S$  = solar irradiance

**$h$  = heat transfer coefficient**

$D$  = diameter of the sphere

$k$  = thermal conductivity of air

$\mu$  = viscosity of air

$C_p$  = heat capacity of air

$Re$  = Reynolds number ( $\rho v D / \mu$ )

$\rho$  = density of air

$v$  = wind speed

Properties of air &  
Sensor geometry

# Temperature effect

## □ Radiation from the sensor

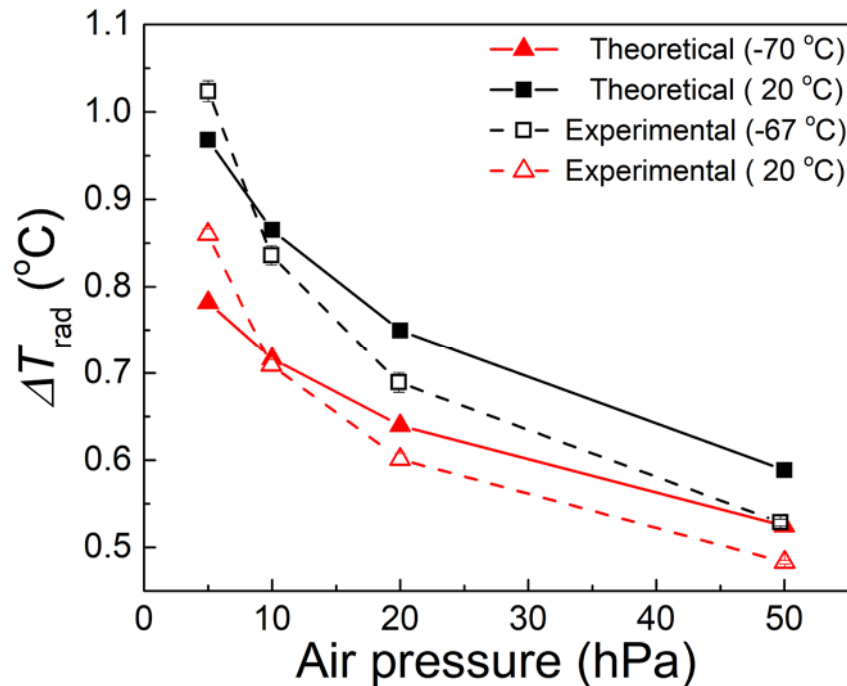
◆  $T \downarrow \rightarrow k \text{ (thermal conductivity)} \downarrow \rightarrow h \downarrow \rightarrow \Delta T_{\text{rad}}$

NIST National Institute of Standards and Technology  
NIST Chemistry WebBook, SRD 69

Thermophysical Properties of Fluid Systems

Accurate thermophysical properties are available for several fluids. These data include the following:

- Density
- $C_p$
- Enthalpy
- Internal energy
- Viscosity
- Joule-Thomson coefficient
- Specific volume
- $C_v$
- Entropy
- Speed of Sound
- Thermal conductivity
- Surface tension (saturation curve only)



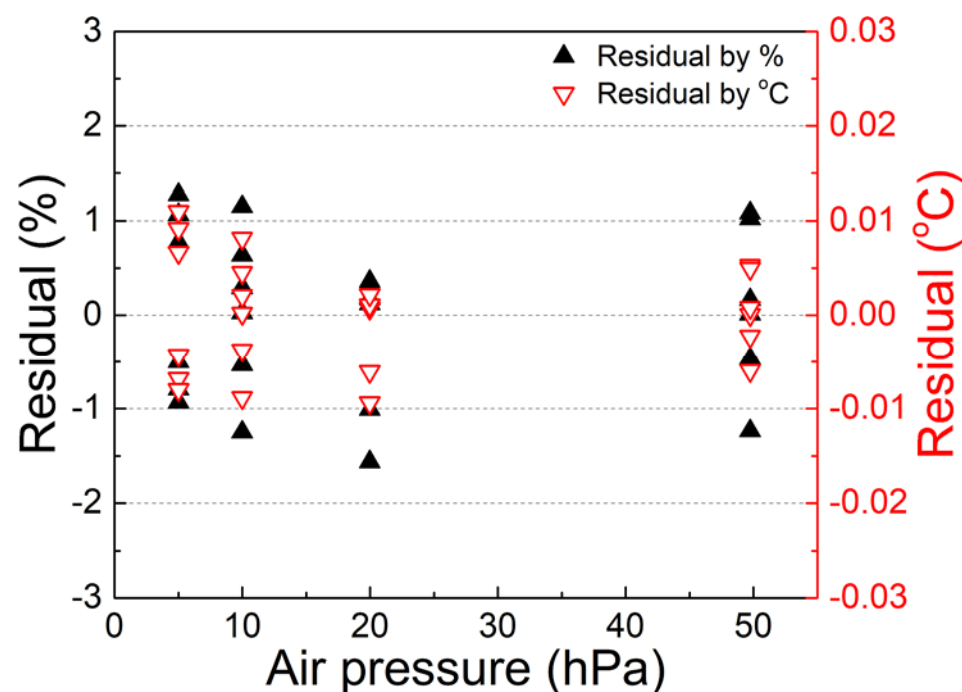
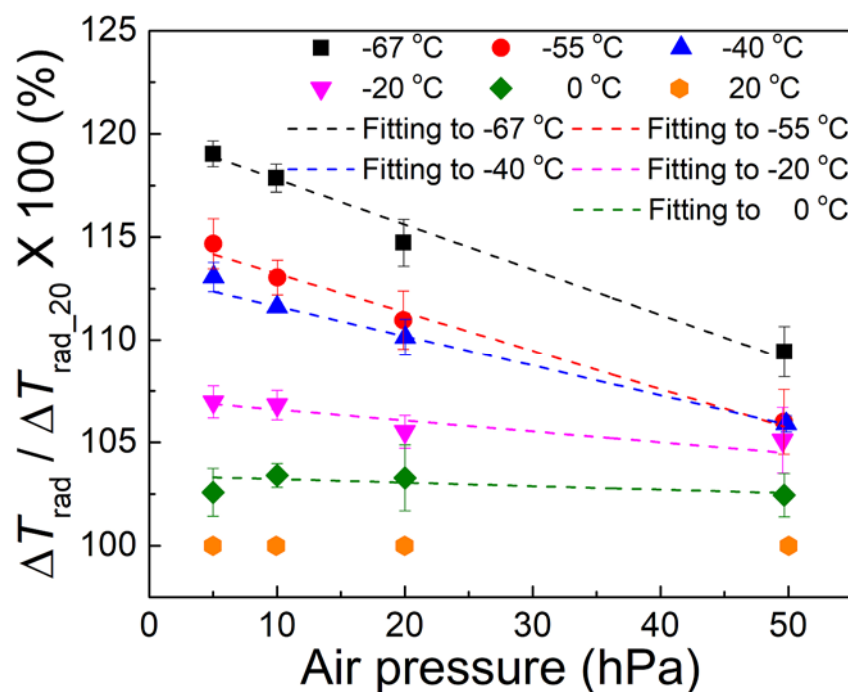
Parameter	Symbol (Unit)	Value ( $T_a = 20\text{ °C}$ )	Value ( $T_a = -70\text{ °C}$ )
Diameter	$D$ (m)	0.001	0.001
Air pressure	$P_a$ (hPa)	5	5
Wind speed	$v$ (ms <sup>-1</sup> )	5	5
Viscosity	$\mu$ (Pa·s)	0.00001754	0.00001307
Density	$\rho$ (kg·m <sup>-3</sup> )	0.0057466	0.0082925
Thermal conductivity	$k$ (W·m <sup>-1</sup> ·K <sup>-1</sup> )	0.025367	0.018869
Heat capacity	$C_p$ (J·kg <sup>-1</sup> ·K <sup>-1</sup> )	1039.6	1039.1
Reynolds number	$Re$	1.64	3.17
Heat transfer coefficient	$h$ (W·m <sup>-2</sup> ·K <sup>-1</sup> )	63.97	51.67
Solar irradiance	$S$ (W·m <sup>-2</sup> )	1000	1000
Absorptivity of metal	$\alpha$	0.2	0.2
Radiation correction	$T_s - T_a$ (K)	0.78	0.97

$$\alpha S = h(T_s - T_a), \quad h = \frac{k}{D} \left[ 2 + \left( 0.4Re^{\frac{1}{2}} + 0.06Re^{\frac{2}{3}} \right) \left( \frac{\mu C_p}{k} \right)^{\frac{2}{5}} \right]$$

# Estimation of low temperature effect

□ Empirical formula based on experiment

◆ Estimation of  $\Delta T_{\text{rad}}$  at cold temperatures using  $\Delta T_{\text{rad}}$  at 20 °C

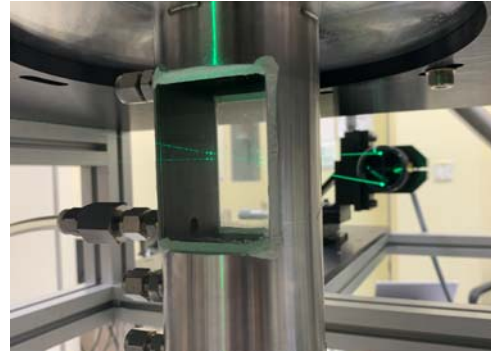


$$\Delta T_{\text{rad}} / \Delta T_{\text{rad}_20} \times 100 (\%) = D(T) \cdot P + E(T) , \quad D(T) = d_0 \cdot T + d_1 \text{ \& } E(T) = e_0 \cdot T + e_1$$

# Ventilation effect

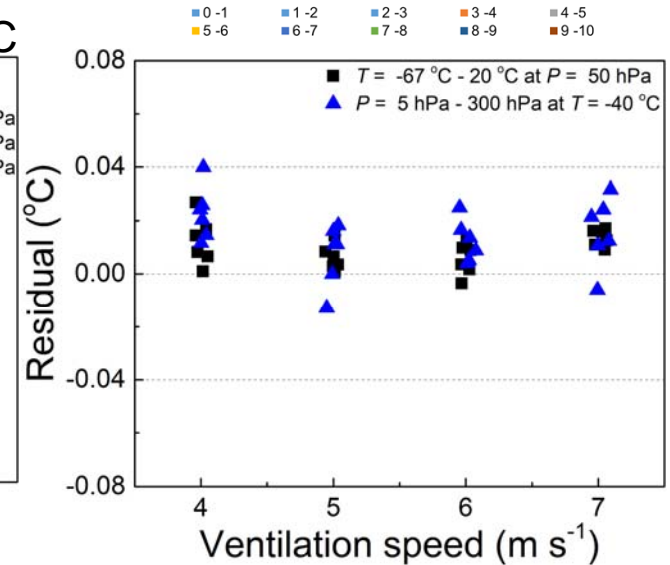
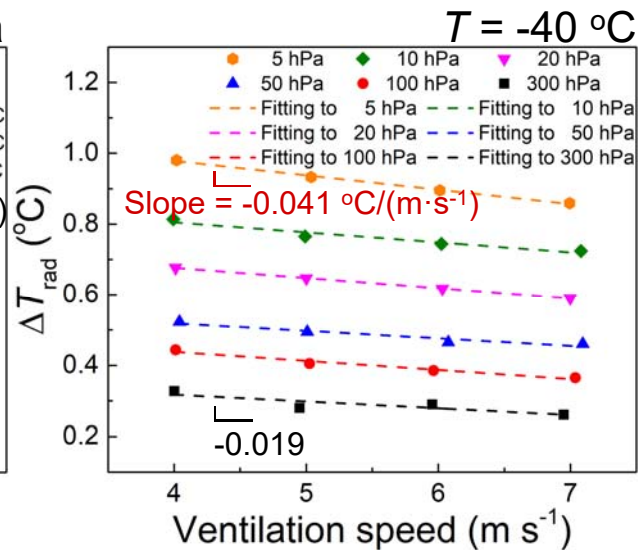
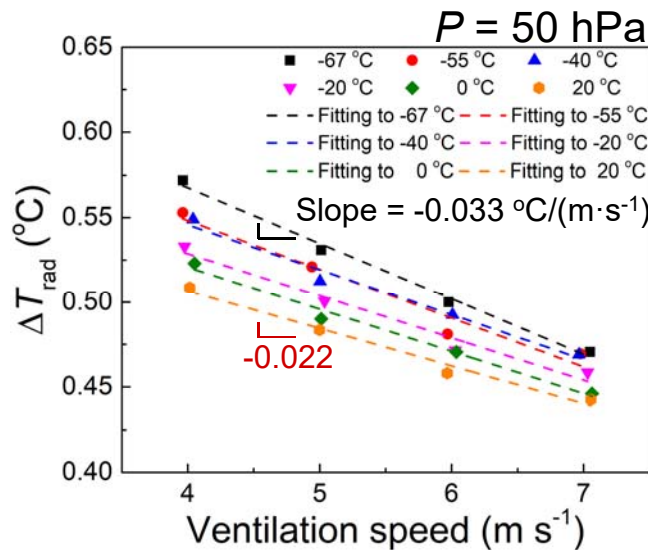
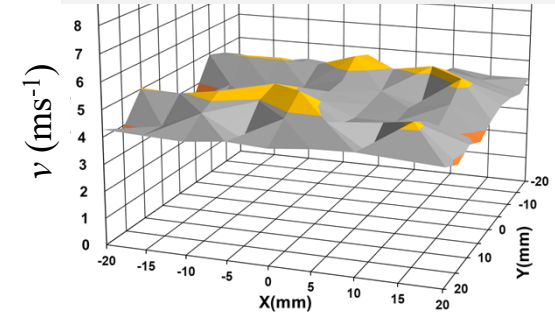
## □ Convective cooling

◆  $v \uparrow \rightarrow \Delta T_{\text{rad}} \downarrow$



Laser Doppler Velocimetry

Reference:  $4.67 \text{ ms}^{-1}$  (550 hPa)  
Measurement mean:  $4.63 \text{ ms}^{-1}$



$$\Delta T_{\text{rad}} = A_0(T) + B_0(T) \cdot \log(P) + C_0(T) \cdot [\log(P)]^2 - 0.027 \cdot (v-5)$$

for  $5 \text{ hPa} \leq P \leq 500 \text{ hPa}$ ,  $S_0 = 980 \text{ W} \cdot \text{m}^{-2}$

# Irradiance effect

## □ Heating by solar irradiance

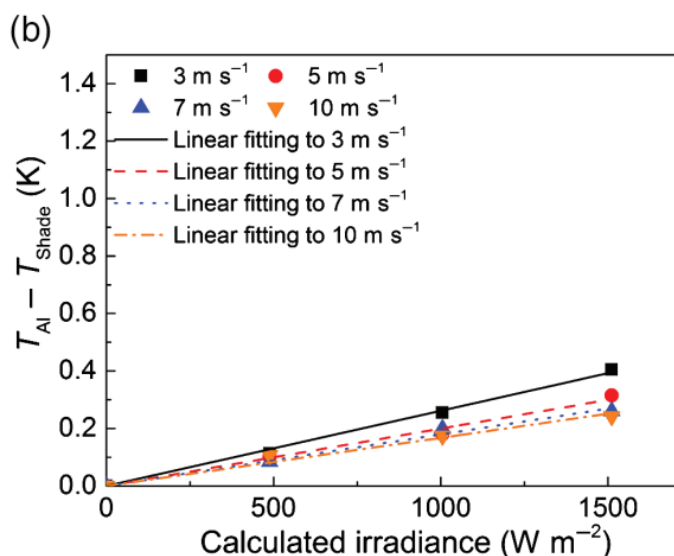
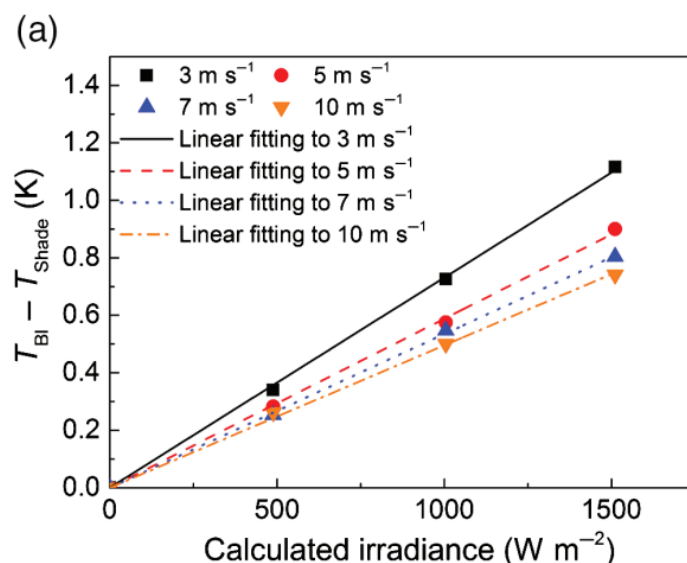
◆  $\Delta T_{\text{rad}}$  is proportional to  $S$

$$-h(T_s - T_a) - \sigma\varepsilon(T_s^4 - T_a^4) + \alpha S = 0$$

(convection)      (sensor radiation)      (solar radiation)



$$T_s - T_a = \frac{\alpha S}{h} \quad (\text{Proportional to } S)$$



Lee *et al.* Meteorol. Appl. **25**, 209 (2018)

$$\Delta T_{\text{rad}} = S/S_0 \times [A_0(T) + B_0(T) \cdot \log(P) + C_0(T) \cdot [\log(P)]^2 - 0.027 \cdot (v-5)]$$

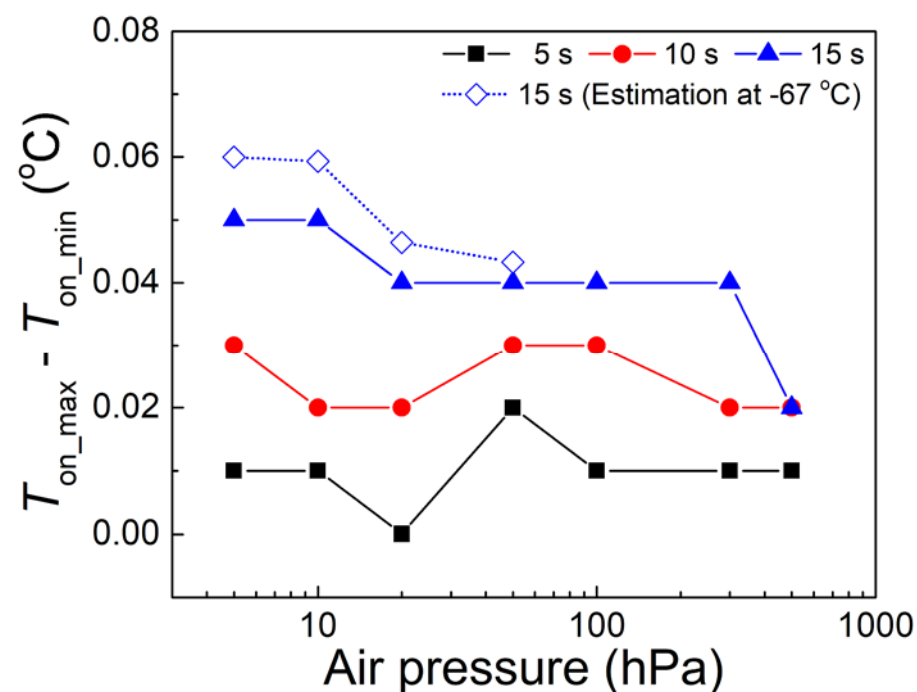
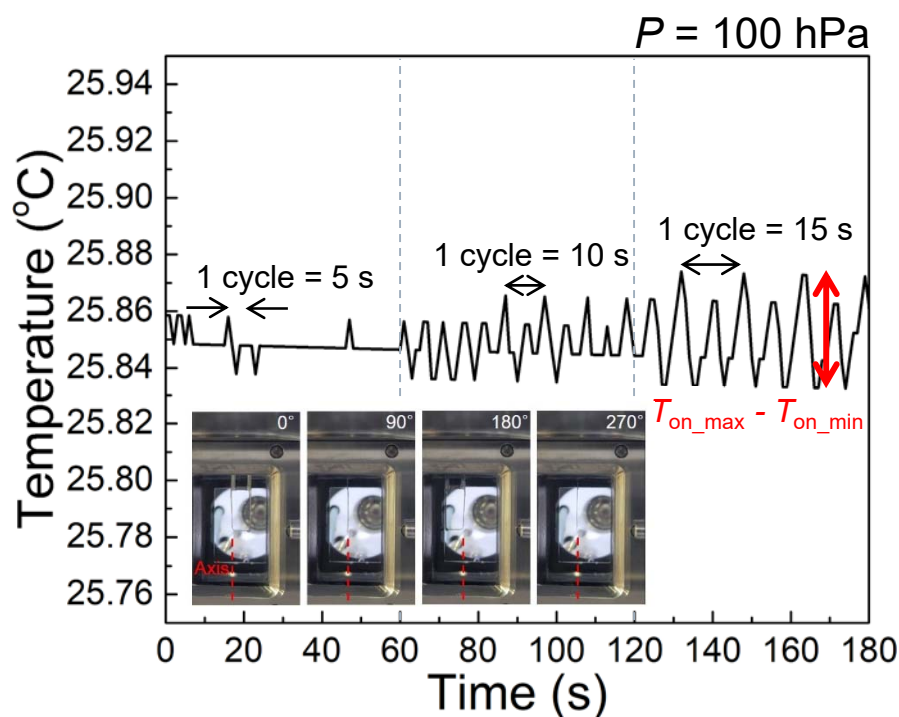
for  $5 \text{ hPa} \leq P \leq 500 \text{ hPa}$ ,  $S_0 = 980 \text{ W} \cdot \text{m}^{-2}$



# Rotation of radiosonde

□ Simulating rotation motion of radiosonde in sounding

◆ Oscillation of  $\Delta T_{\text{rad}}$

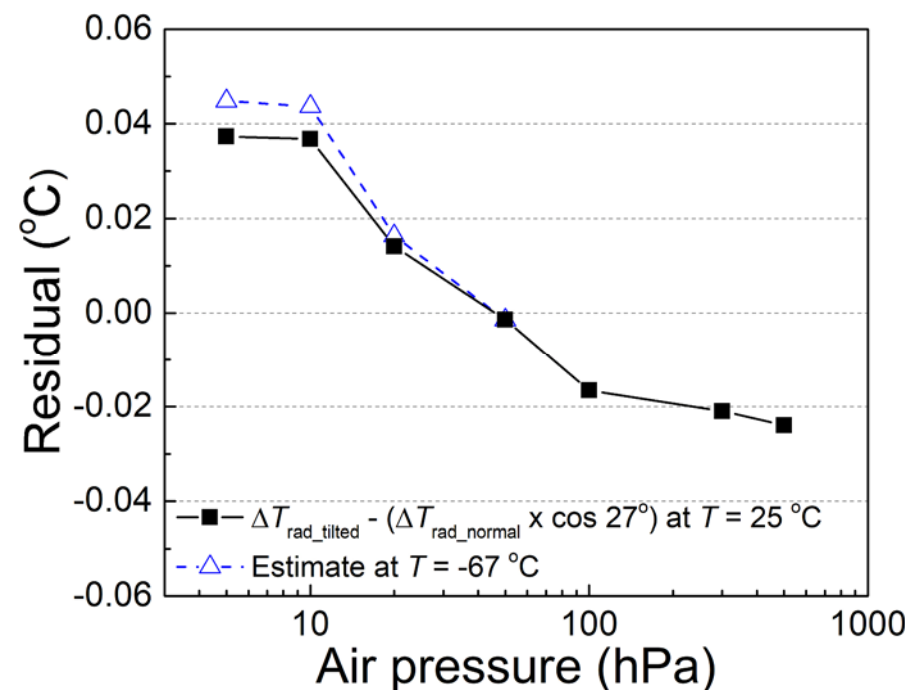
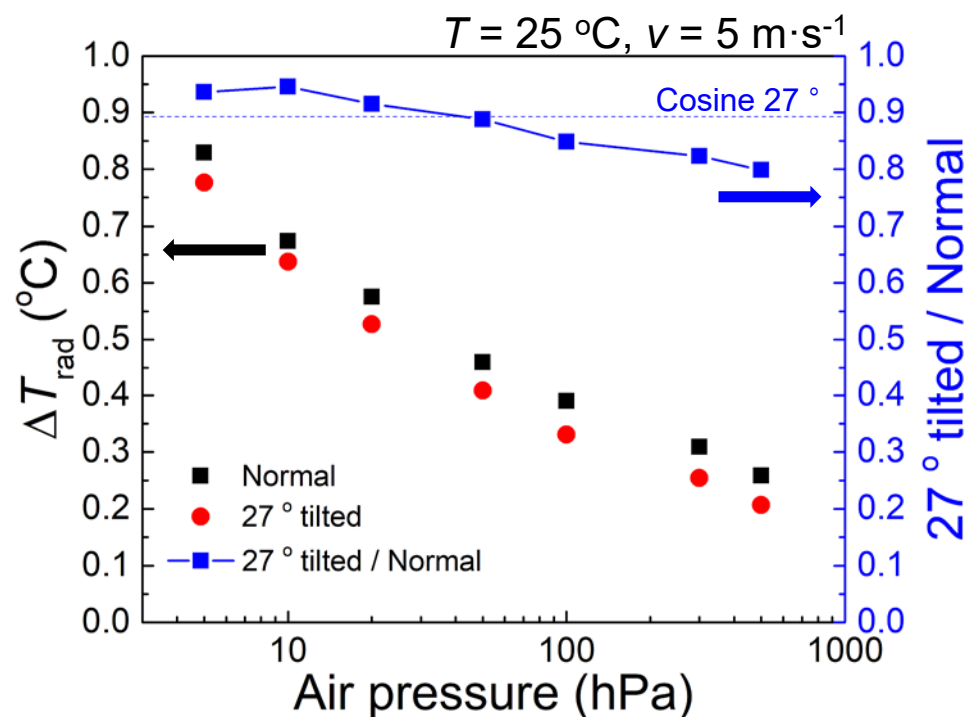


Oscillation of  $\Delta T_{\text{rad}}$  can be averaged out by fittings or treated as **uncertainty**

# Radiosonde tilting

□ Simulating solar elevation angle

◆ Calculation of  $\Delta T_{\text{rad}}$  in proportion to effective irradiance

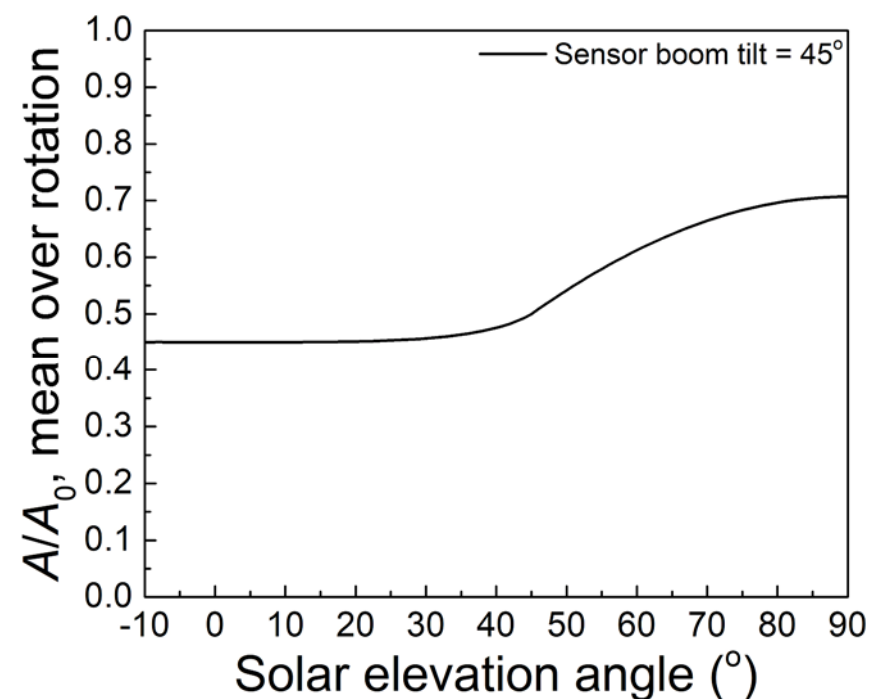
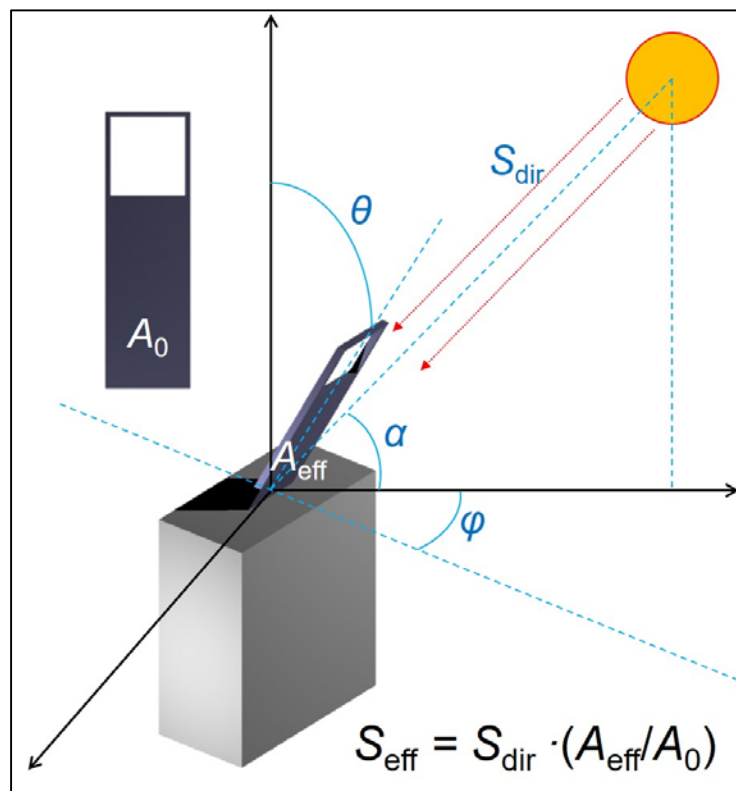


$$\Delta T_{\text{rad}} = (S_{\text{eff}}/S_0) \times [A_0(T) + B_0(T) \cdot \log(P) + C_0(T) \cdot [\log(P)]^2 - 0.027 \cdot (v-5)]$$

for  $5\text{ hPa} \leq P \leq 500\text{ hPa}$ ,  $S_0 = 980\text{ W}\cdot\text{m}^{-2}$

# Effective irradiance to sensor

- Solar angle  $\alpha$ , Azimuthal angle  $\varphi$ , & Boom tilt angle  $\theta$
- ◆ Effective irradiance (mean over rotation angle,  $\varphi$ )



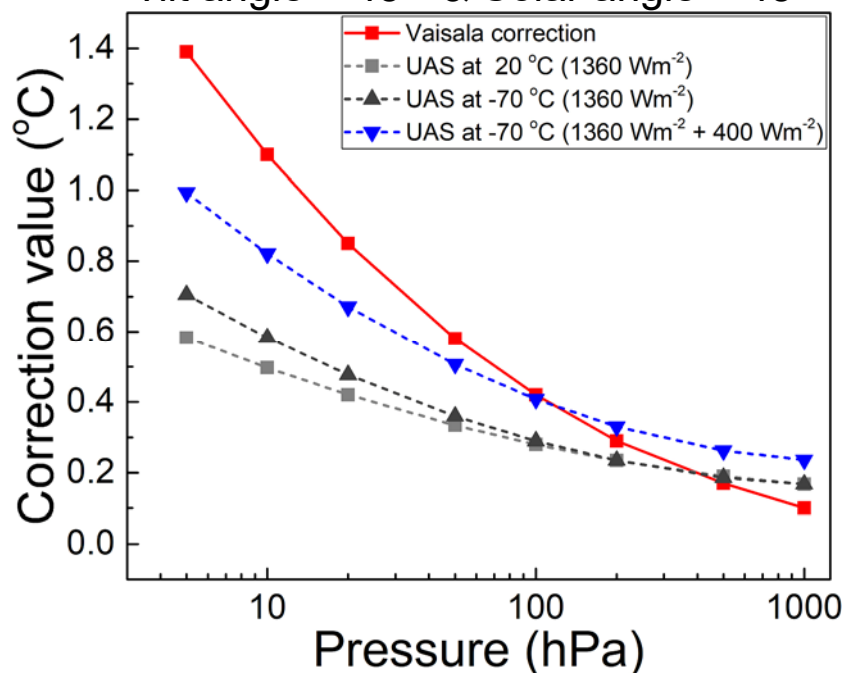
$$S_{\text{eff}} = S_{\text{dir}} \cdot | \cos \alpha \cos \theta \cos \varphi - \sin \theta \sin \alpha |$$

# Radiation correction

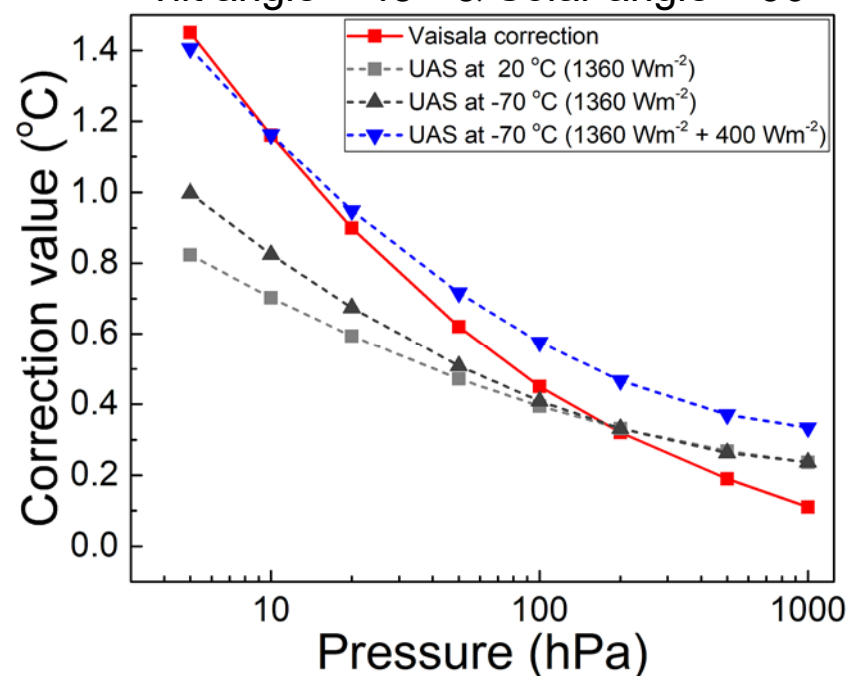
## □ UAS (KRISS) vs. Manufacturer (Vaisala)

◆  $\Delta T_{\text{rad\_UAS}} < \Delta T_{\text{rad\_Vaisala}}$

Tilt angle = 45 ° & Solar angle = 45 °



Tilt angle = 45 ° & Solar angle = 90 °



$\Delta T_{\text{rad\_UAS}} < \Delta T_{\text{rad\_Vaisala}}$  by 0.5–0.7 °C at -70 °C & 5 hPa with  $S = 1360 \text{ W} \cdot \text{m}^{-2}$  &  $\alpha = 45\text{--}90^\circ$

$\Delta T_{\text{rad\_UAS}} < \Delta T_{\text{rad\_Vaisala}}$  by 0.04–0.4 °C at -70 °C & 5 hPa with  $S = 1360+400 \text{ W} \cdot \text{m}^{-2}$  &  $\alpha = 45\text{--}90^\circ$

# Uncertainty

## □ Uncertainty of radiation correction, $U(\Delta T_{\text{rad}})$

Uncertainty factor	Condition	Unit	Standard uncertainty ( $k = 1$ )	Contribution to uncertainty of radiation correction ( $k = 2$ )
$T$	-67	°C	0.028	0.000 °C
$P$	5	hPa	0.01	0.000 °C
$v$	5	m·s <sup>-1</sup>	0.058	0.004 °C
$S$	980	W·m <sup>-2</sup>	30.5	0.062 °C
Rotation	24	°·s <sup>-1</sup>	-	0.035 °C
Tilting	27	°	-	0.052 °C
Fitting error	-0.024 – 0.04	°C	0.023	0.046 °C
Expanded uncertainty of radiation correction ( $k = 2$ ), $U(\Delta T_{\text{rad}})$				0.100 °C

## □ Uncertainty of corrected temperature, $U(T_{\text{cor}})$

$$U(T_{\text{cor}})^2 = U(T_{\text{raw}})^2 + U(\Delta T_{\text{rad}})^2$$

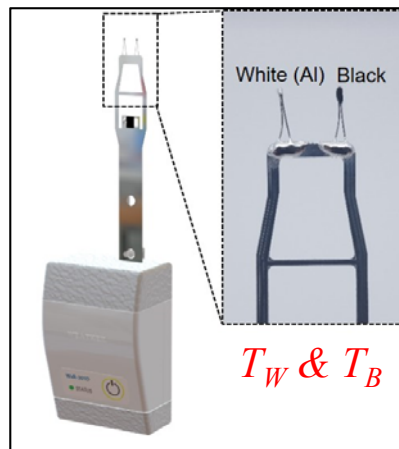
Uncertainty factor	Uncertainty ( $k = 2$ )
Expanded uncertainty for the radiation correction at 1360 W·m <sup>-2</sup> , $U(\Delta T_{\text{rad}})$	0.138 °C
Calibration of RS41 temperature sensor (Vaisala), $U(T_{\text{raw}})$	0.100 °C
Expanded uncertainty in the corrected temperature, $U(T_{\text{cor}})$	0.170 °C

Scaled to 1360 W·m<sup>-2</sup>

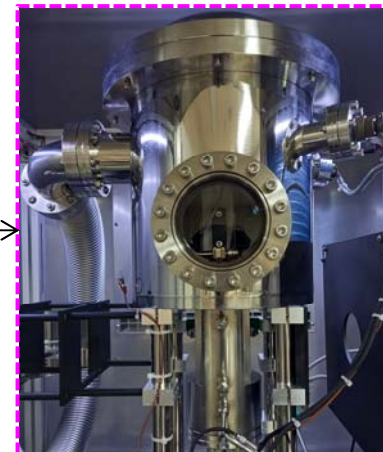


# Radiation correction with irradiance measurement

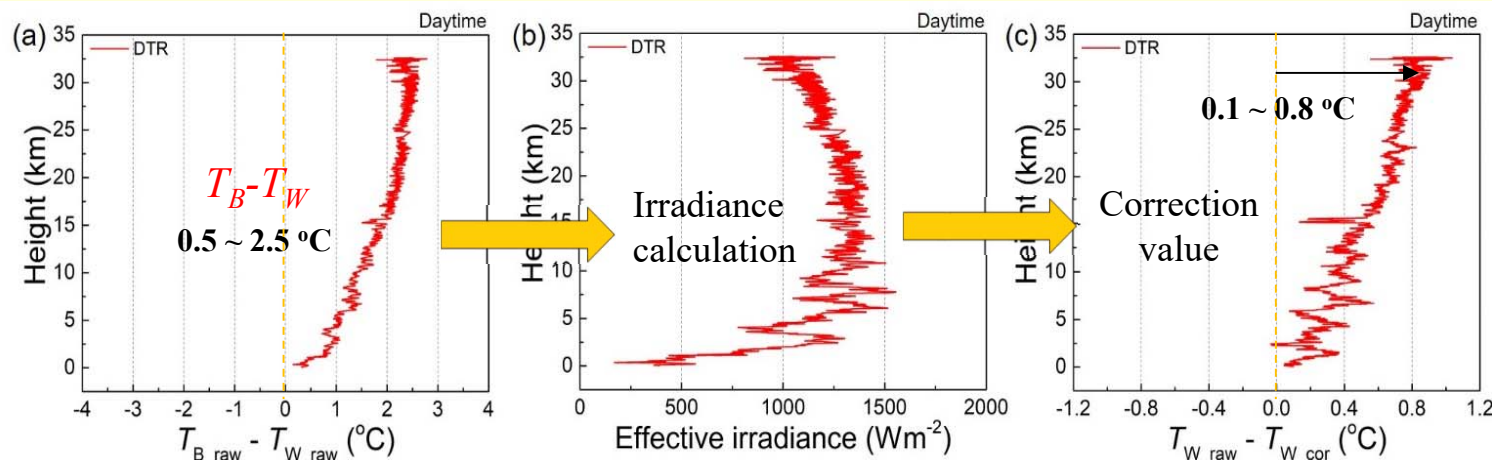
## □ Dual thermistor radiosonde (DTR)



Parameterization of  $S$  &  $\Delta T_{\text{rad}}$   
with  $T_B - T_W$ ,  $T$ ,  $P$ ,  $v$  in UAS



Daytime



Dual thermistor radiosonde will be presented by Dr. Yong-Gyoo Kim (KRISS)

# Summary

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## □ Upper air simulator for radiation correction of radiosonde

- ◆ Temperature (-70–20 °C), Pressure (5–500 hPa), Ventilation (4–7 m/s), & Irradiance (1000 W/m<sup>2</sup>)
- ◆ Radiosonde rotation (5, 10, 15 s) & Boom tilting (0–27 °)
- ◆ Radiation correction as a function of  $T$ ,  $P$ ,  $v$ ,  $S$  and solar angle
- ◆  $\Delta T_{\text{rad\_UAS}} < \Delta T_{\text{rad\_Vaisala}}$  by max. 0.04–0.4 °C with  $\alpha = 45\text{--}90^\circ$
- ◆ Uncertainty of radiation correction,  $U(\Delta T_{\text{rad}}) = 0.14^\circ\text{C}$
- ◆ Uncertainty of corrected temperature,  $U(T_{\text{cor}}) = 0.17^\circ\text{C}$
- ◆ Uncertainty of soundings should be added to  $U(T_{\text{cor}})$
- ◆ Any type of radiosonde can be tested using the UAS at KRISS

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# Thank you for your attention

More discussions to [sangwook@kriss.re.kr](mailto:sangwook@kriss.re.kr)