
Upper-air simulator to evaluate the radiation correction and measurement uncertainty of RS41

ICM-13 online

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Significance of radiosonde measurement

- Accurate method to **monitor the long-term climate change** in stratosphere
 - ◆ Temperature is the direct index of global warming
- Practical tool to gather climate variables for the **weather forecasting** in troposphere
- Serve as a **Reference to other remote skills** such as satellite
- Sounding sites more than 1000 sites
 - ◆ National observatories
 - ◆ Military bases, etc
 - ◆ Institutes & universities for research



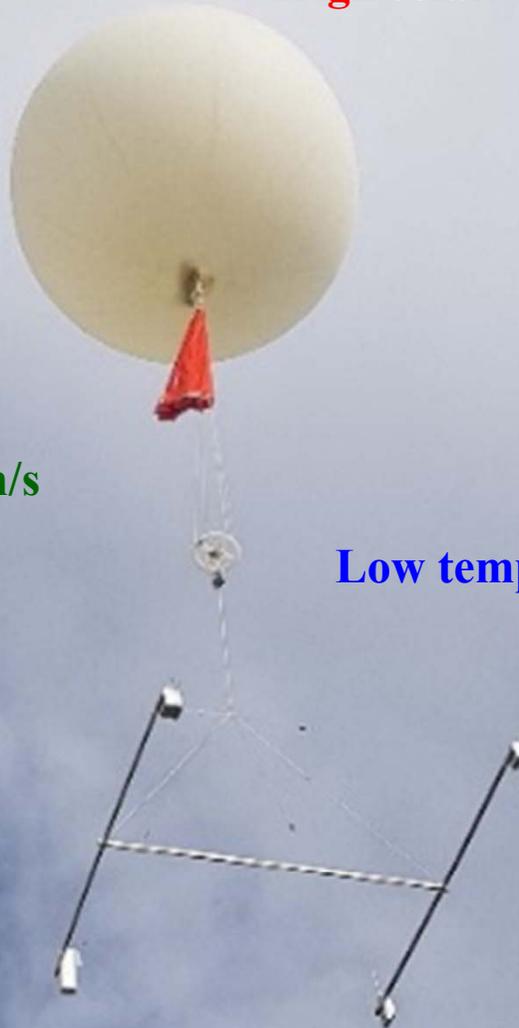
Radiosonde meets ...

High solar irradiance ~ 1360 W/m²

Low pressure down to a few hPa

Upward air ventilation +5 m/s

Low temperature below -70 °C



Requiring accurate test method based on international agreement

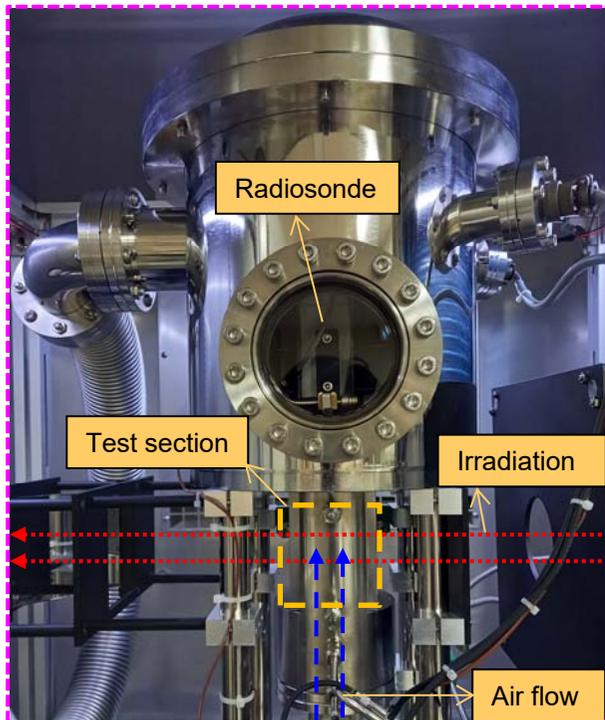
Conditions for test method

- Guide to Meteorological Instruments and Methods of Observation (WMO-No.8)
 - ◆ Chapter 12, MEASUREMENT OF UPPER-AIR PRESSURE, TEMPERATURE AND HUMIDITY
 - “The calibration methods **used by manufacturers** should be identified before purchasing radiosondes.”
 - **Stability** condition of ± 0.2 hPa/min for pressure, ± 0.25 K/min for temperature and ± 1 relative humidity per minute
 - **Errors** less than ± 0.2 hPa for pressure, ± 0.1 K for temperature and $\pm 1\%$ relative humidity

There is no detailed descriptions on the implementation of calibration setups/methods

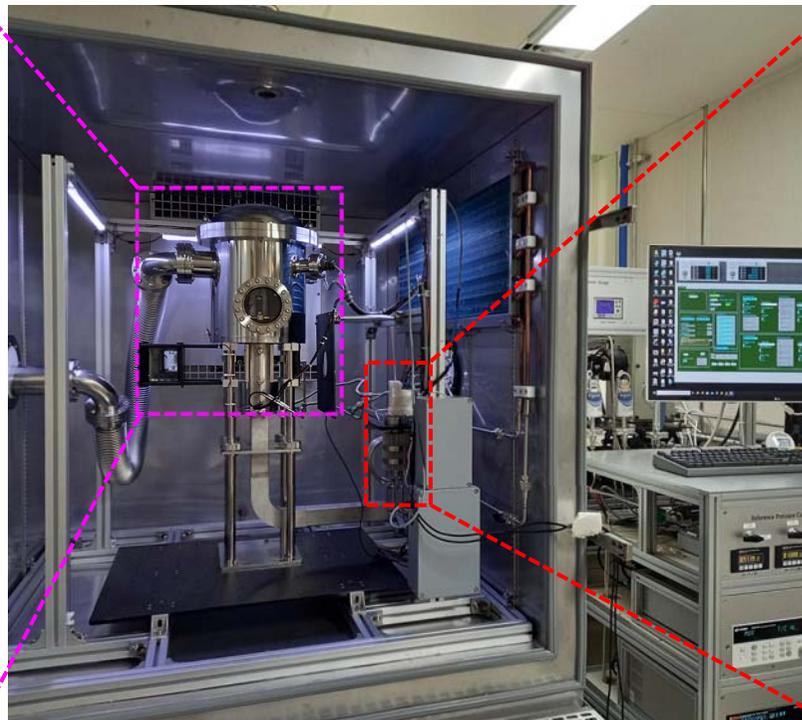
Upper air simulator (UAS) at KRISS

- Radiation correction of temperature sensors
 - ◆ Control of temperature, pressure, ventilation, and irradiance
- Calibration of humidity sensors
 - ◆ Control of temperature and humidity

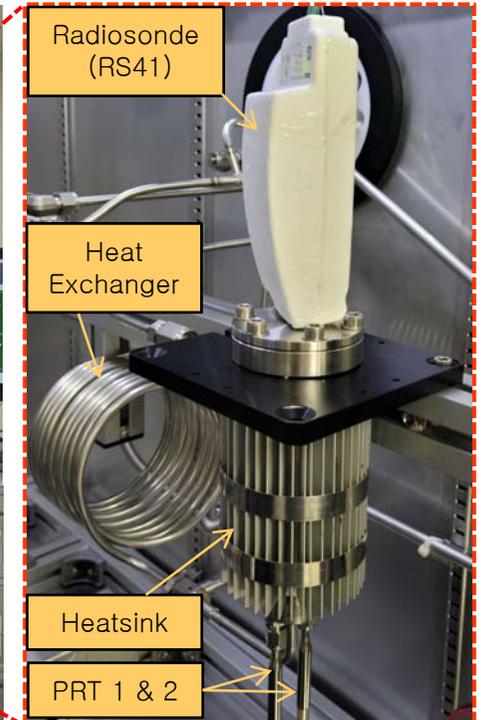


<Radiation correction setup>

Lee *et al.* Meteorol. Appl. **27**, e1855 (2020)



<Upper air simulator>

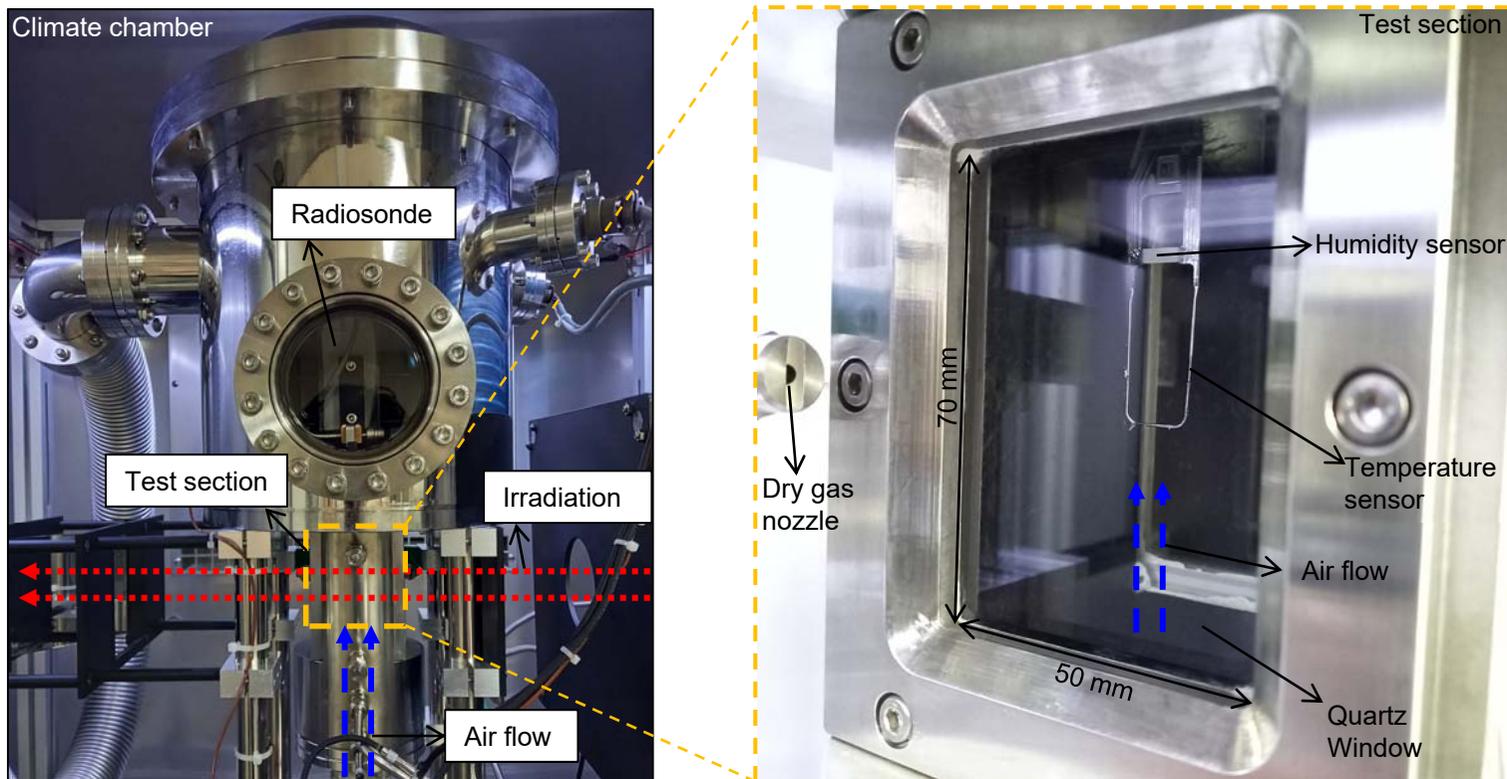


<Humidity calibration setup>

Lee *et al.* Meteorol. Appl. **28**, e2010 (2021)

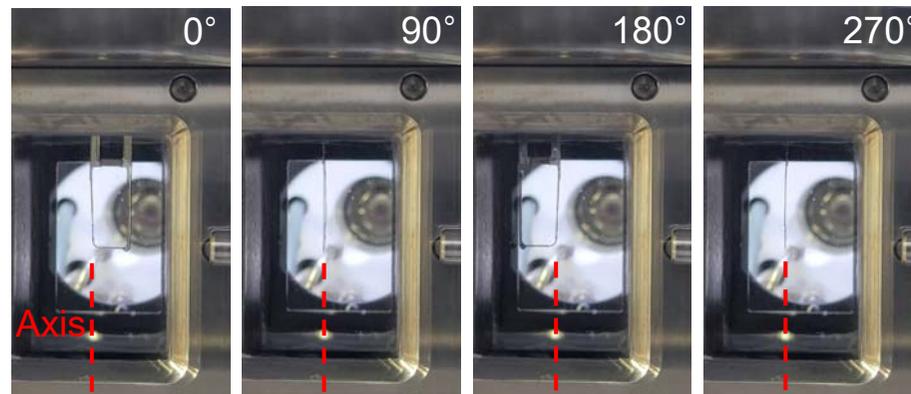
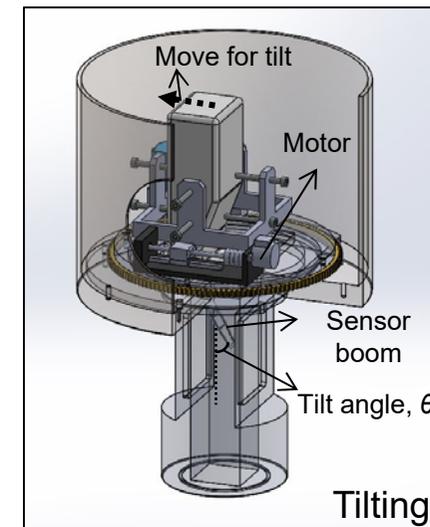
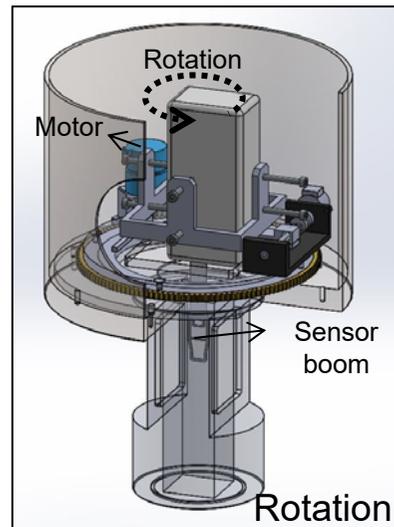
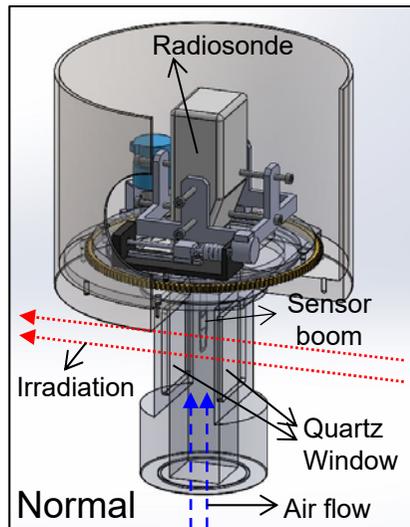
Radiation correction setup

- Environmental factors affecting radiation correction
 - ◆ Temperature ($T = -70\text{--}20\text{ }^{\circ}\text{C}$) by climate chamber
 - ◆ Air pressure ($P = 5\text{--}500\text{ hPa}$) & Ventilation ($v = 4\text{--}7\text{ m/s}$) by sonic nozzles
 - ◆ Irradiance ($S_0 = 1000\text{ W/m}^2$) by solar simulator



Rotation & Tilting of radiosonde

- Simulation of movement of radiosonde in sounding
 - ◆ Rotation (5, 10, 15 s) & Boom tilting (27 °)

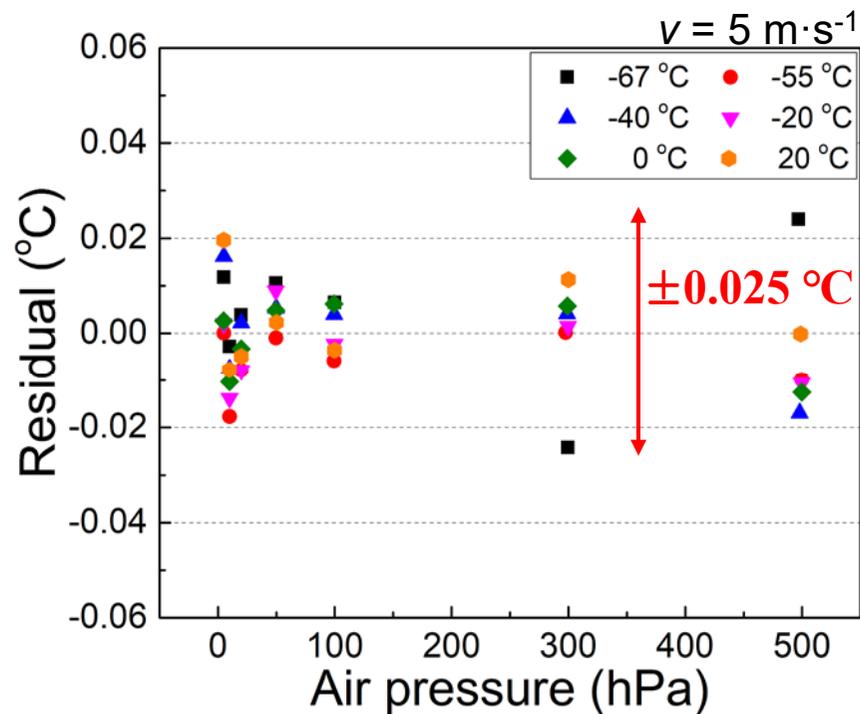
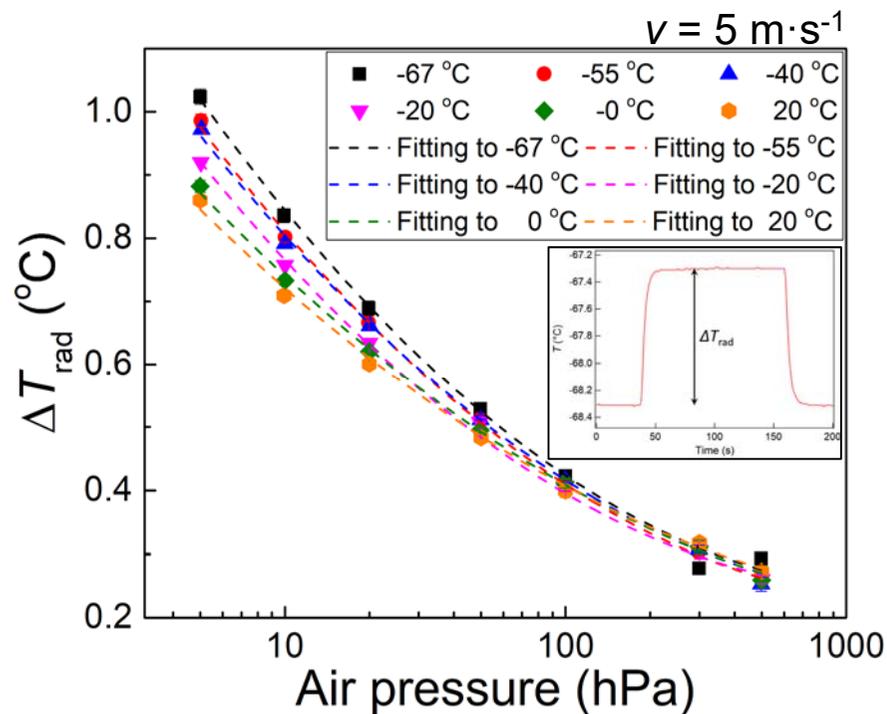


Rotation axis =
Temperature sensor

Pressure effect

□ Convective cooling

- ◆ Radiation correction (ΔT_{rad}) decreases as air pressure (P) increases
- ◆ Air density \uparrow at high $P \rightarrow$ Convective cooling \uparrow

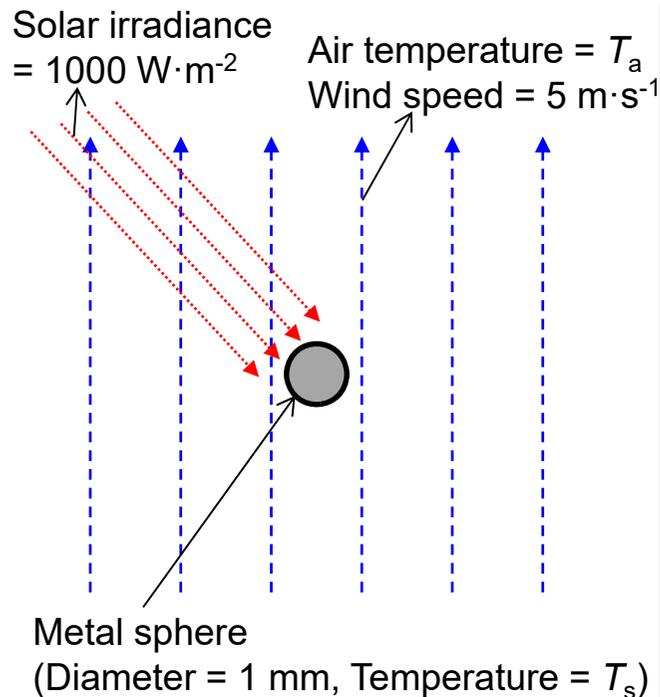


$$\Delta T_{\text{rad}} = A_0(T) + B_0(T) \cdot \log(P) + C_0(T) \cdot [\log(P)]^2 \quad \text{for } 5 \text{ hPa} \leq P \leq 500 \text{ hPa}, S_0 = 980 \text{ W}\cdot\text{m}^{-2}$$

Theoretical understanding

□ Heat transfer calculation

- ◆ Metal sphere is modelled as a temperature sensor



$$\alpha S = h(T_s - T_a), \quad h = \frac{k}{D} \left[2 + \left(0.4Re^{\frac{1}{2}} + 0.06Re^{\frac{2}{3}} \right) \left(\frac{\mu C_p}{k} \right)^{\frac{2}{5}} \right]$$

α = absorptivity of the metal sphere

S = solar irradiance

h = heat transfer coefficient

D = diameter of the sphere

k = thermal conductivity of air

μ = viscosity of air

C_p = heat capacity of air

Re = Reynolds number ($\rho v D / \mu$)

ρ = density of air

v = wind speed

Properties of air &
Sensor geometry

Temperature effect

□ Radiation from the sensor

◆ $T \downarrow \rightarrow k$ (thermal conductivity) $\downarrow \rightarrow h \downarrow \rightarrow \Delta T_{\text{rad}}$

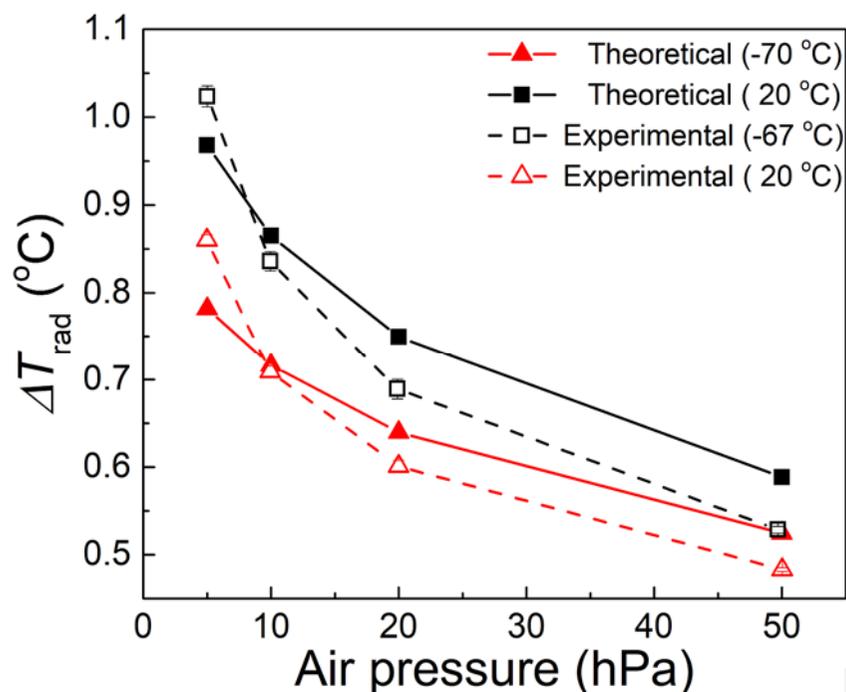
NIST National Institute of Standards and Technology NIST Chemistry WebBook, SRD 69

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Thermophysical Properties of Fluid Systems

Accurate thermophysical properties are available for several fluids. These data include the following:

- Density
- C_p
- Enthalpy
- Internal energy
- Viscosity
- Joule-Thomson coefficient
- Specific volume
- C_v
- Entropy
- Speed of Sound
- Thermal conductivity
- Surface tension (saturation curve only)



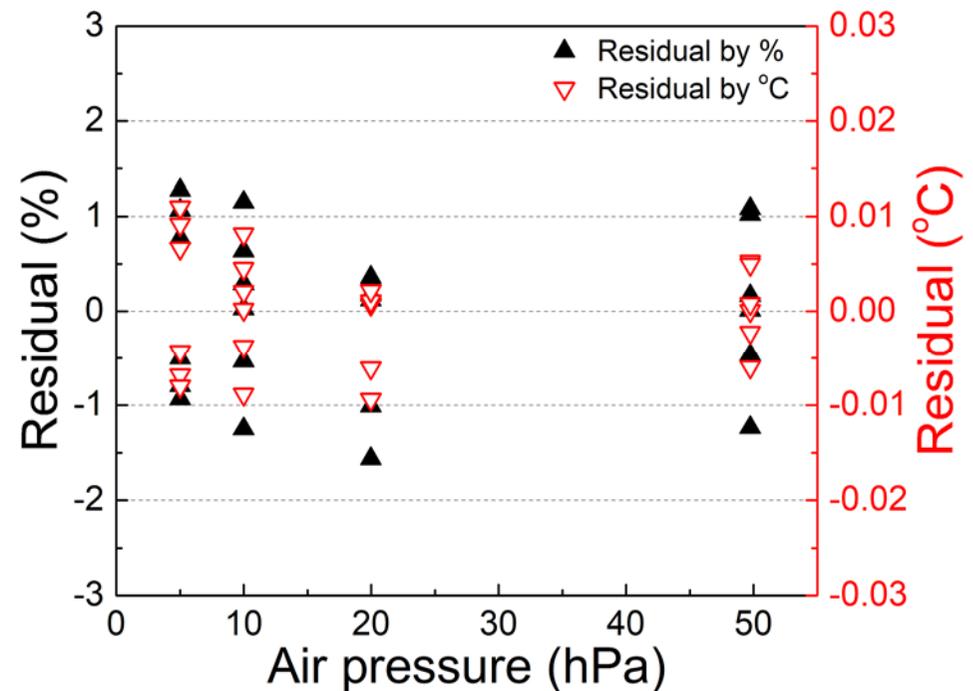
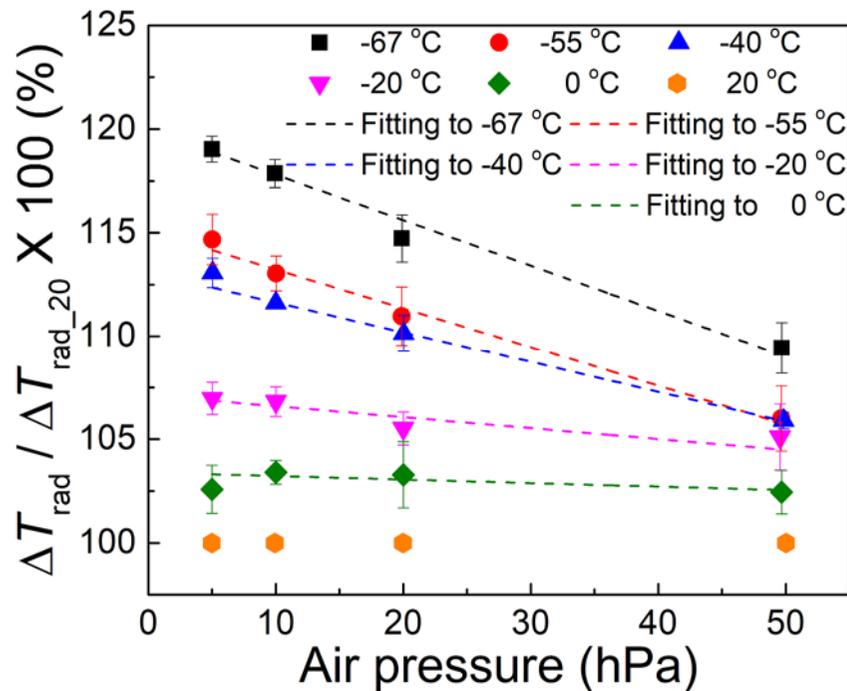
Parameter	Symbol (Unit)	Value ($T_a = 20\text{ °C}$)	Value ($T_a = -70\text{ °C}$)
Diameter	D (m)	0.001	0.001
Air pressure	P_a (hPa)	5	5
Wind speed	v (ms^{-1})	5	5
Viscosity	μ (Pa·s)	0.00001754	0.00001307
Density	ρ ($\text{kg}\cdot\text{m}^{-3}$)	0.0057466	0.0082925
Thermal conductivity	k ($\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$)	0.025367	0.018869
Heat capacity	C_p ($\text{J}\cdot\text{kg}^{-1}\cdot\text{K}^{-1}$)	1039.6	1039.1
Reynolds number	Re	1.64	3.17
Heat transfer coefficient	h ($\text{W}\cdot\text{m}^{-2}\cdot\text{K}^{-1}$)	63.97	51.67
Solar irradiance	S ($\text{W}\cdot\text{m}^{-2}$)	1000	1000
Absorptivity of metal	α	0.2	0.2
Radiation correction	$T_s - T_a$ (K)	0.78	0.97

$$\alpha S = h(T_s - T_a), \quad h = \frac{k}{D} \left[2 + \left(0.4Re^{\frac{1}{2}} + 0.06Re^{\frac{2}{3}} \right) \left(\frac{\mu C_p}{k} \right)^{\frac{2}{5}} \right]$$

Estimation of low temperature effect

□ Empirical formula based on experiment

◆ Estimation of ΔT_{rad} at cold temperatures using ΔT_{rad} at 20 °C

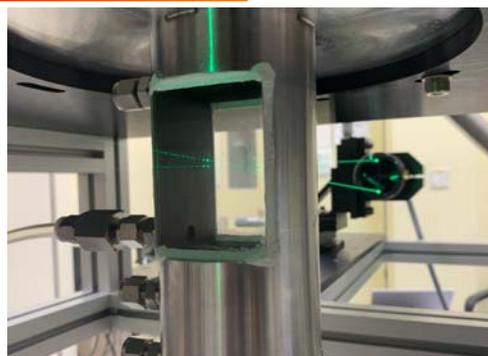


$$\Delta T_{\text{rad}} / \Delta T_{\text{rad}_20} \times 100 (\%) = D(T) \cdot P + E(T) , \quad D(T) = d_0 \cdot T + d_1 \ \& \ E(T) = e_0 \cdot T + e_1$$

Ventilation effect

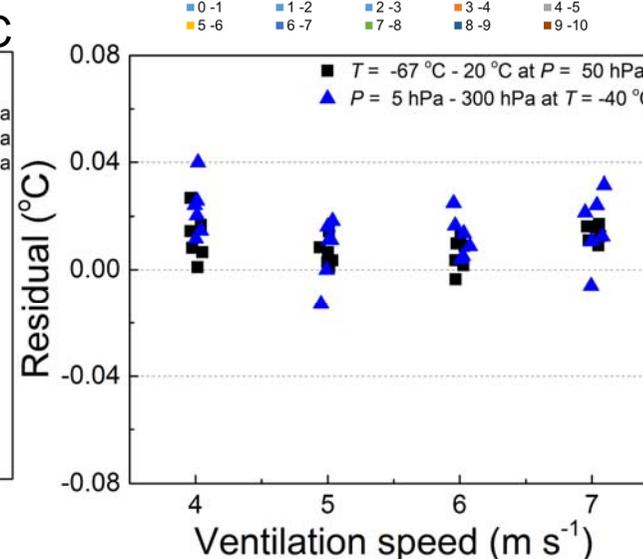
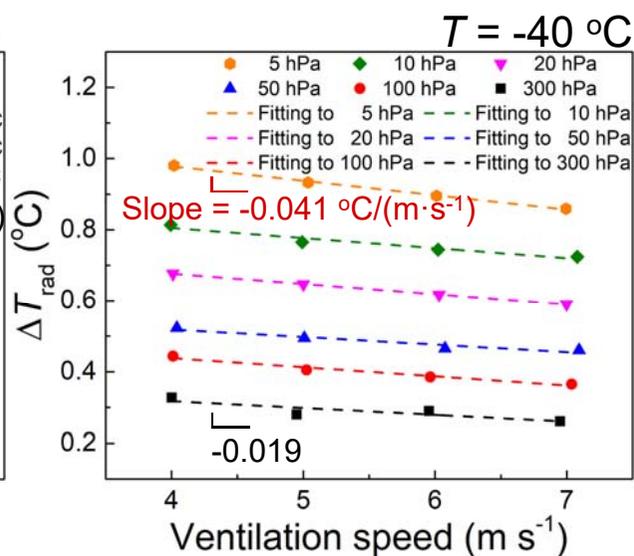
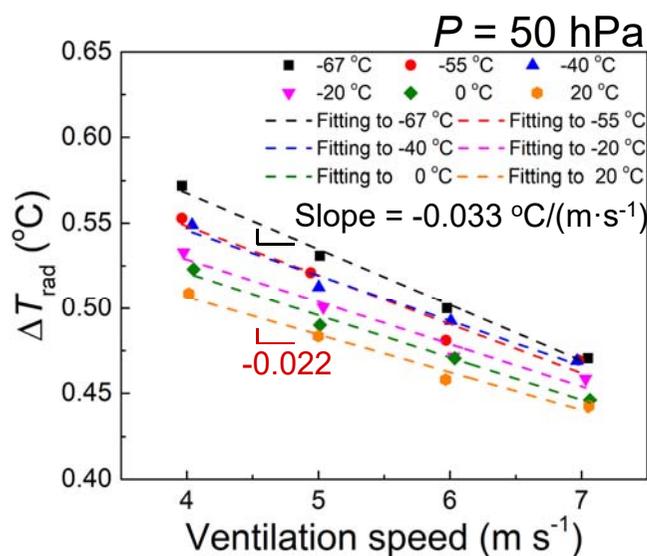
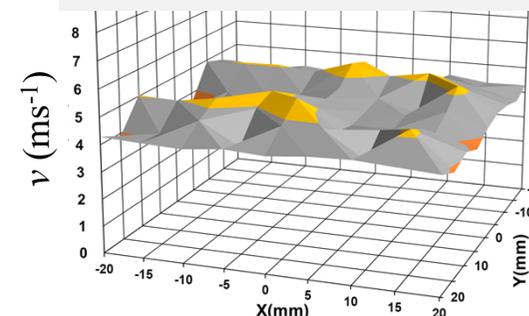
□ Convective cooling

◆ $v \uparrow \rightarrow \Delta T_{\text{rad}} \downarrow$



Laser Doppler Velocimetry

Reference: 4.67 ms^{-1} (550 hPa)
Measurement mean: 4.63 ms^{-1}



$$\Delta T_{\text{rad}} = A_0(T) + B_0(T) \cdot \log(P) + C_0(T) \cdot [\log(P)]^2 - 0.027 \cdot (v-5)$$

for $5 \text{ hPa} \leq P \leq 500 \text{ hPa}$, $S_0 = 980 \text{ W} \cdot \text{m}^{-2}$

Irradiance effect

□ Heating by solar irradiance

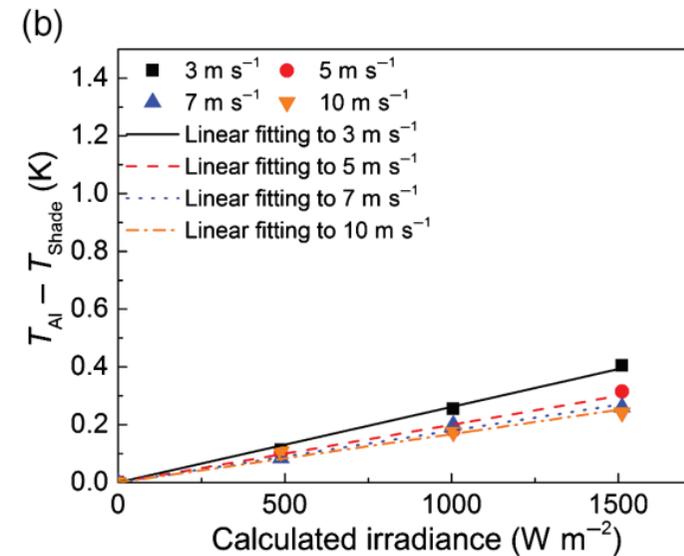
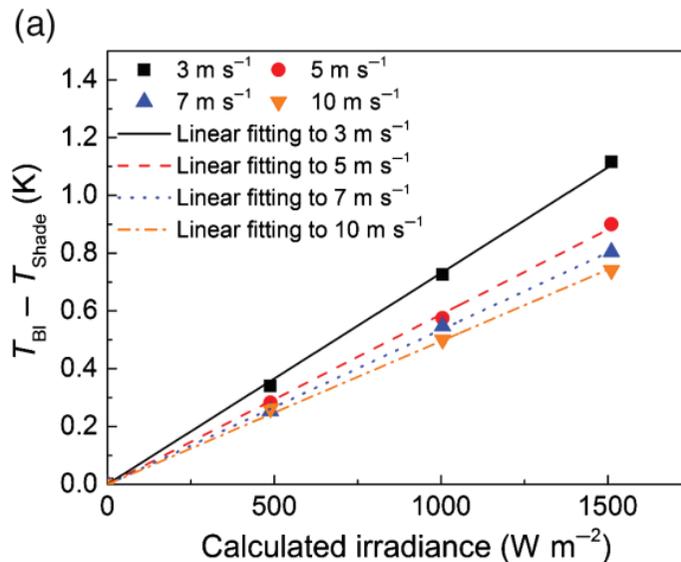
◆ ΔT_{rad} is proportional to S

$$-h(T_s - T_a) - \sigma\varepsilon(T_s^4 - T_a^4) + \alpha S = 0$$

(convection) (sensor radiation) (solar radiation)



$$T_s - T_a = \frac{\alpha S}{h} \quad (\text{Proportional to } S)$$



Lee *et al.* Meteorol. Appl. **25**, 209 (2018)

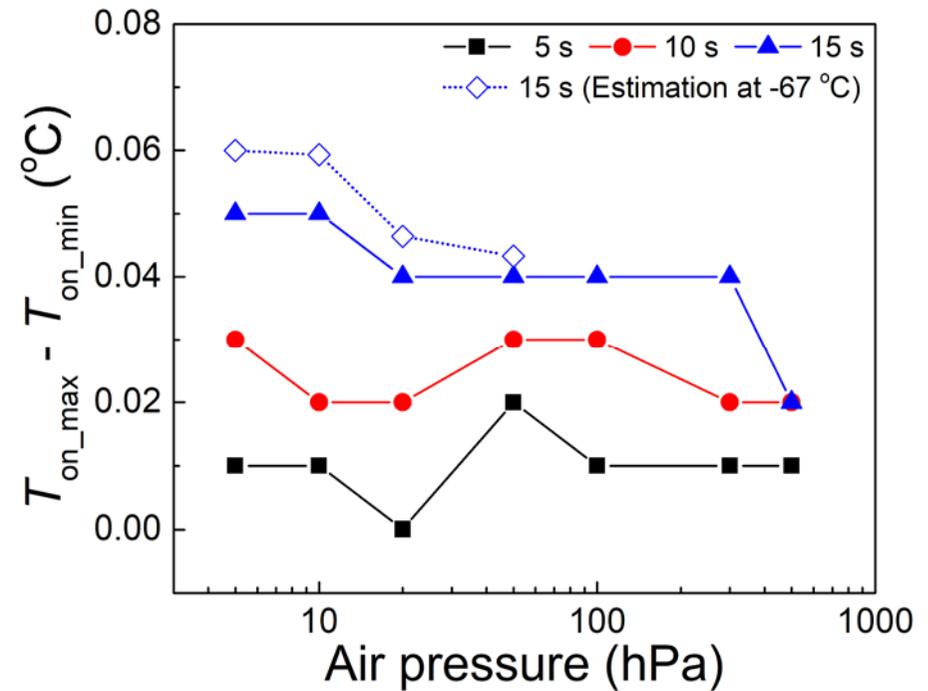
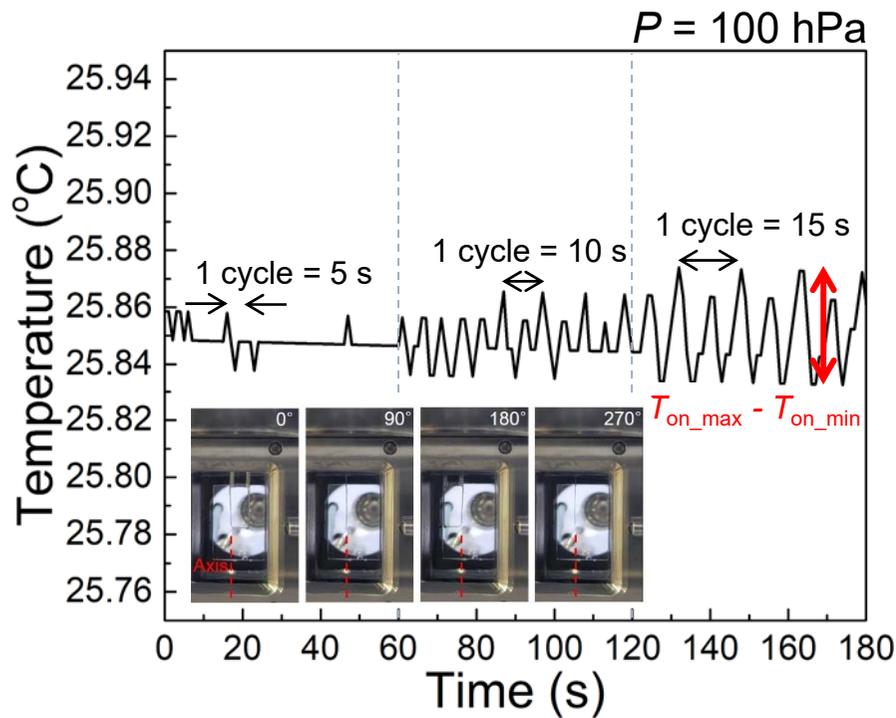
$$\Delta T_{\text{rad}} = S/S_0 \times [A_0(T) + B_0(T) \cdot \log(P) + C_0(T) \cdot [\log(P)]^2 - 0.027 \cdot (v-5)]$$

for $5 \text{ hPa} \leq P \leq 500 \text{ hPa}$, $S_0 = 980 \text{ W} \cdot \text{m}^{-2}$

Rotation of radiosonde

□ Simulating rotation motion of radiosonde in sounding

◆ Oscillation of ΔT_{rad}

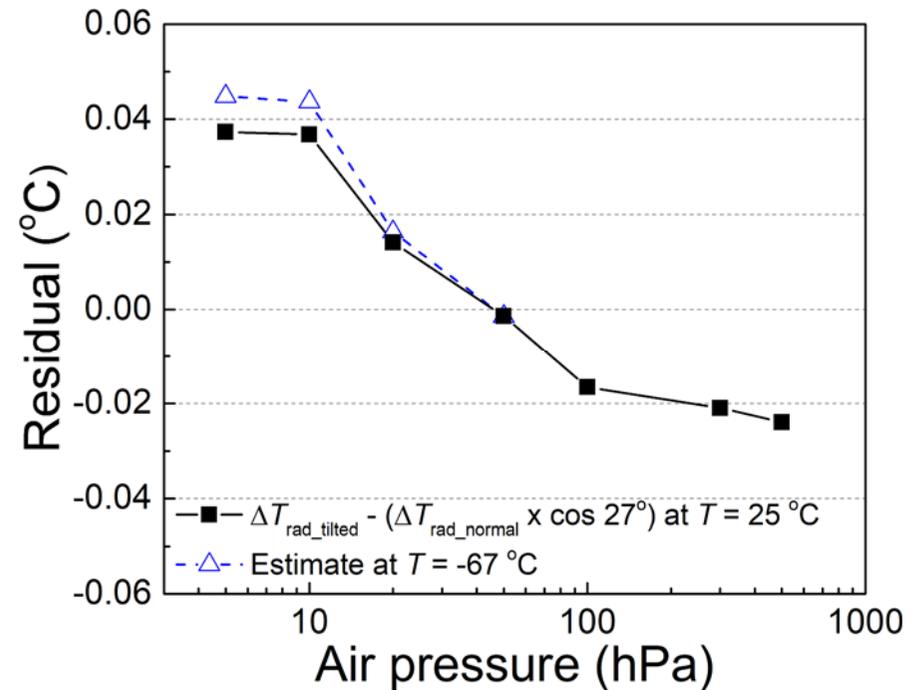
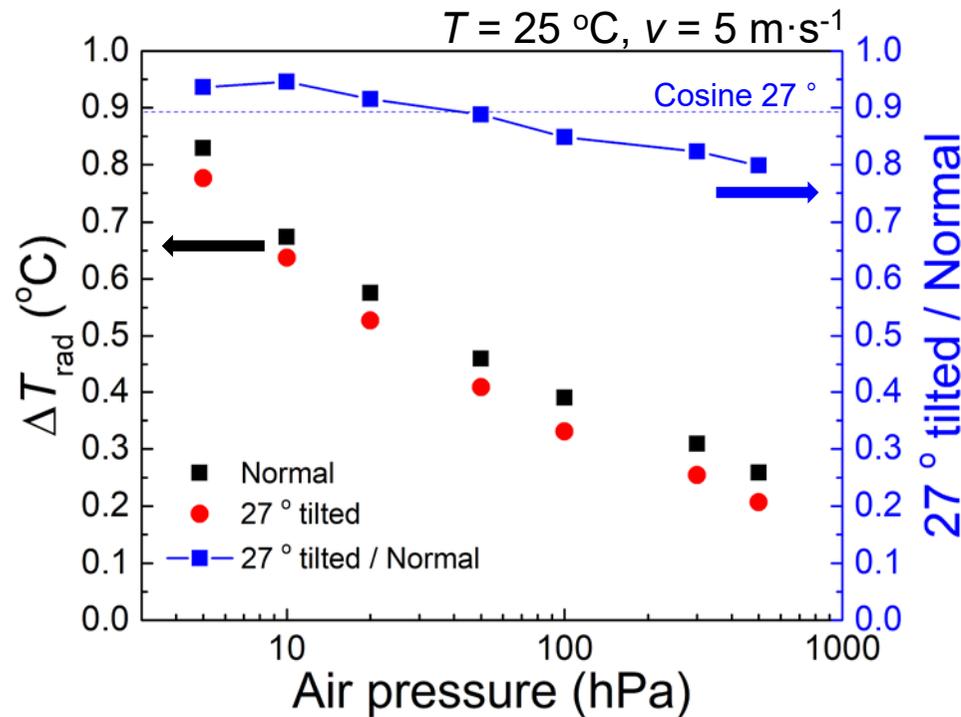


Oscillation of ΔT_{rad} can be averaged out by fittings or treated as **uncertainty**

Radiosonde tilting

□ Simulating solar elevation angle

◆ Calculation of ΔT_{rad} in proportion to effective irradiance

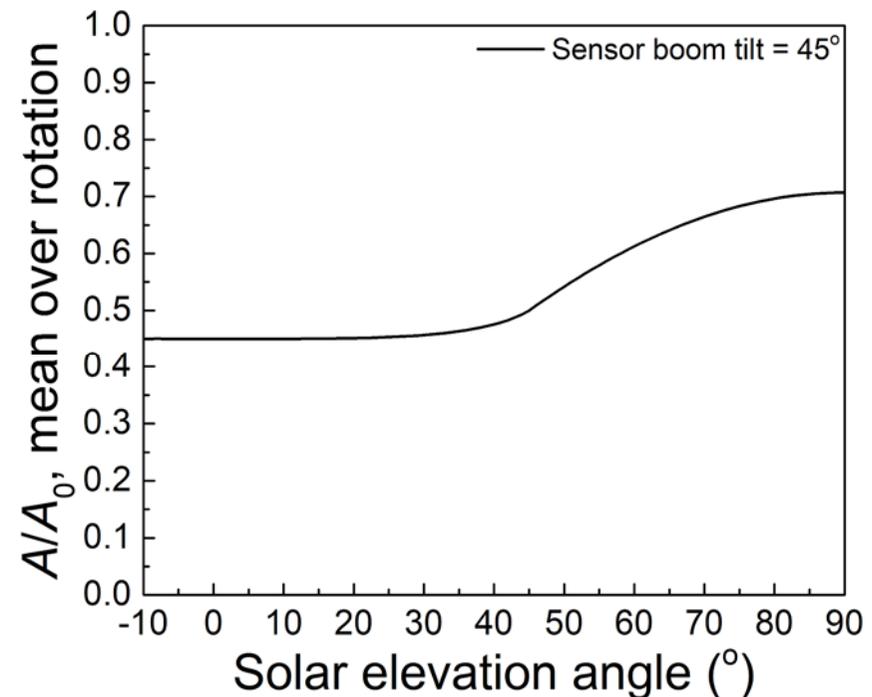
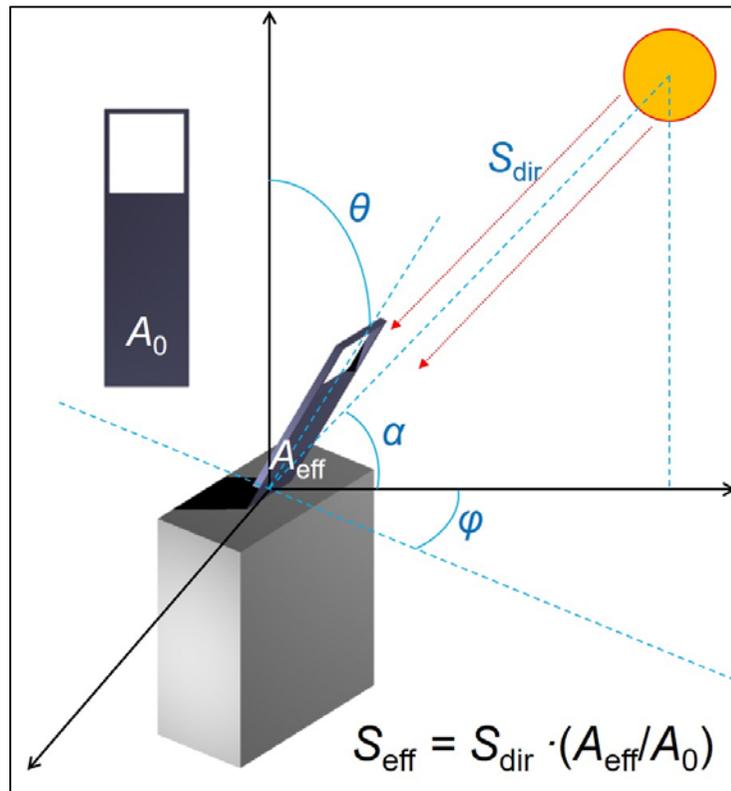


$$\Delta T_{\text{rad}} = (S_{\text{eff}}/S_0) \times [A_0(T) + B_0(T) \cdot \log(P) + C_0(T) \cdot [\log(P)]^2 - 0.027 \cdot (v-5)]$$

for $5 \text{ hPa} \leq P \leq 500 \text{ hPa}, S_0 = 980 \text{ W}\cdot\text{m}^{-2}$

Effective irradiance to sensor

- Solar angle α , Azimuthal angle φ , & Boom tilt angle θ
- ◆ Effective irradiance (mean over rotation angle, φ)



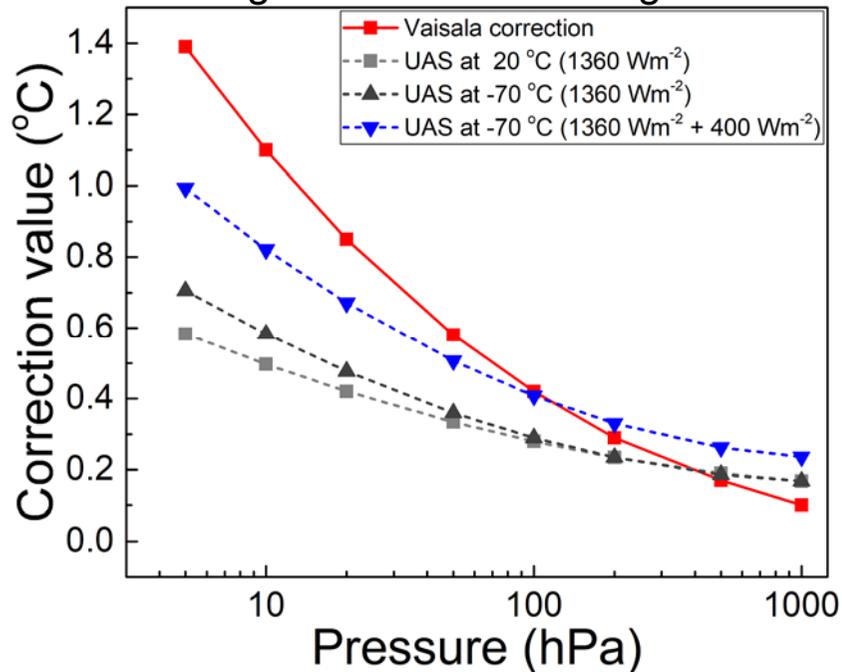
$$S_{\text{eff}} = S_{\text{dir}} \cdot | \cos\alpha \cos\theta \cos\varphi - \sin\theta \sin\alpha |$$

Radiation correction

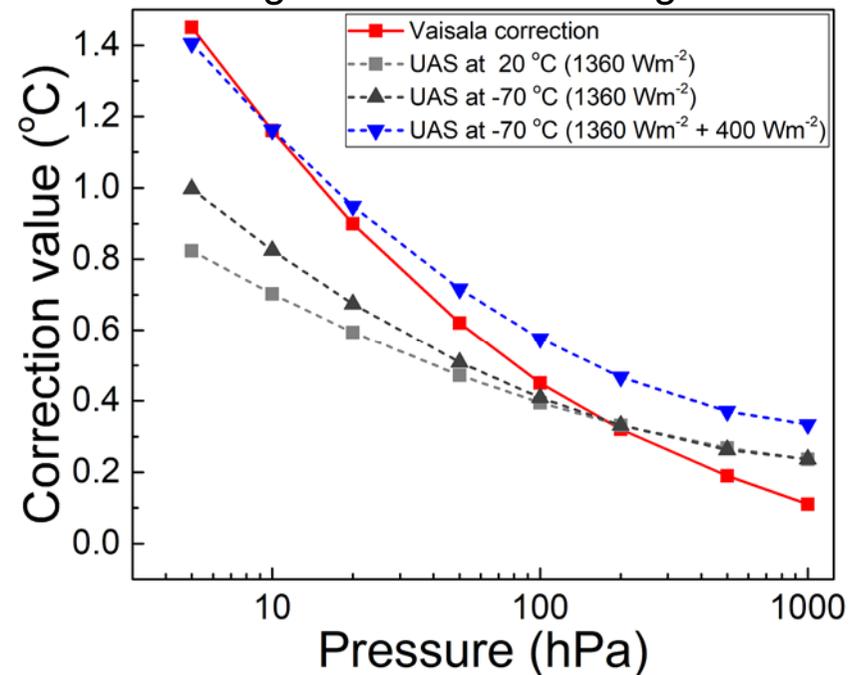
UAS (KRISS) vs. Manufacturer (Vaisala)

◆ $\Delta T_{\text{rad_UAS}} < \Delta T_{\text{rad_Vaisala}}$

Tilt angle = 45 ° & Solar angle = 45 °



Tilt angle = 45 ° & Solar angle = 90 °



$\Delta T_{\text{rad_UAS}} < \Delta T_{\text{rad_Vaisala}}$ by 0.5–0.7 °C at -70 °C & 5 hPa with $S = 1360 \text{ W} \cdot \text{m}^{-2}$ & $\alpha = 45\text{--}90^\circ$

$\Delta T_{\text{rad_UAS}} < \Delta T_{\text{rad_Vaisala}}$ by 0.04–0.4 °C at -70 °C & 5 hPa with $S = 1360+400 \text{ W} \cdot \text{m}^{-2}$ & $\alpha = 45\text{--}90^\circ$

Uncertainty

□ Uncertainty of radiation correction, $U(\Delta T_{\text{rad}})$

Uncertainty factor	Condition	Unit	Standard uncertainty ($k = 1$)	Contribution to uncertainty of radiation correction ($k = 2$)
T	-67	°C	0.028	0.000 °C
P	5	hPa	0.01	0.000 °C
v	5	m·s ⁻¹	0.058	0.004 °C
S	980	W·m ⁻²	30.5	0.062 °C
Rotation	24	°·s ⁻¹	-	0.035 °C
Tilting	27	°	-	0.052 °C
Fitting error	-0.024 – 0.04	°C	0.023	0.046 °C
Expanded uncertainty of radiation correction ($k = 2$), $U(\Delta T_{\text{rad}})$				0.100 °C

□ Uncertainty of corrected temperature, $U(T_{\text{cor}})$

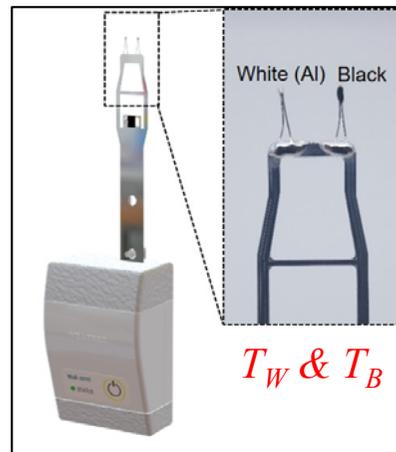
$$U(T_{\text{cor}})^2 = U(T_{\text{raw}})^2 + U(\Delta T_{\text{rad}})^2$$

Uncertainty factor	Uncertainty ($k = 2$)
Expanded uncertainty for the radiation correction at 1360 W·m ⁻² , $U(\Delta T_{\text{rad}})$	0.138 °C
Calibration of RS41 temperature sensor (Vaisala), $U(T_{\text{raw}})$	0.100 °C
Expanded uncertainty in the corrected temperature, $U(T_{\text{cor}})$	0.170 °C

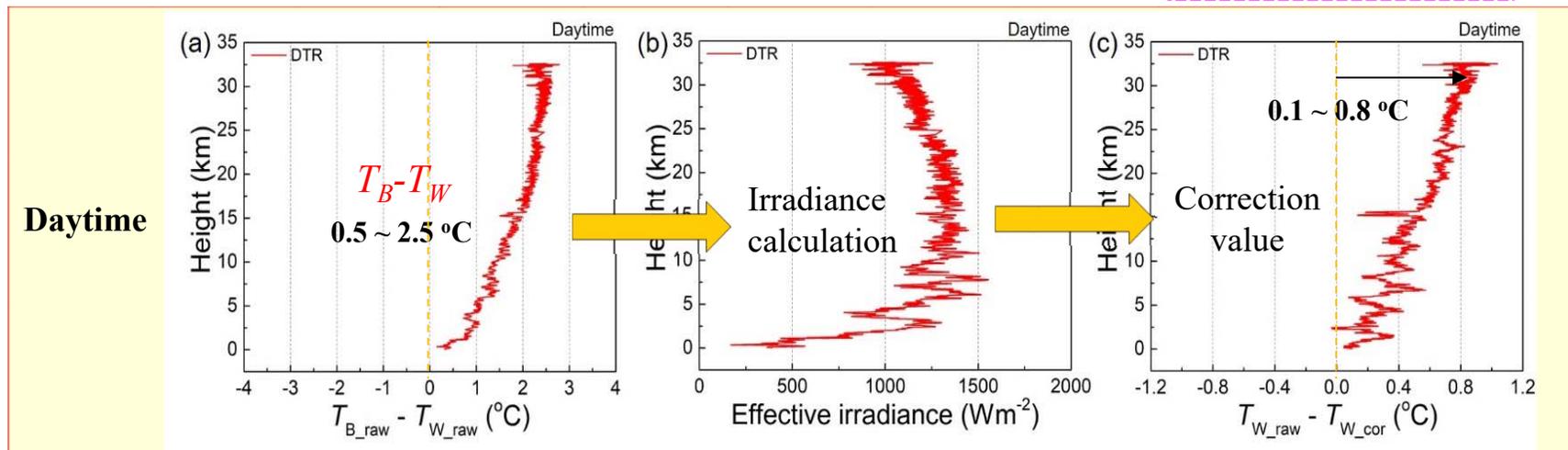
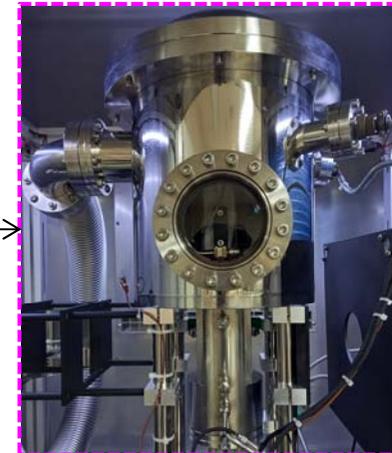
Scaled to 1360 W·m⁻²

Radiation correction with irradiance measurement

□ Dual thermistor radiosonde (DTR)



Parameterization of S & ΔT_{rad}
with $T_B - T_W$, T , P , v in UAS



Dual thermistor radiosonde will be presented by Dr. Yong-Gyoo Kim (KRISS)

Summary

□ Upper air simulator for radiation correction of radiosonde

- ◆ Temperature (-70–20 °C), Pressure (5–500 hPa), Ventilation (4–7 m/s), & Irradiance (1000 W/m²)
- ◆ Radiosonde rotation (5, 10, 15 s) & Boom tilting (0–27 °)
- ◆ Radiation correction as a function of T , P , v , S and solar angle
- ◆ $\Delta T_{\text{rad_UAS}} < \Delta T_{\text{rad_Vaisala}}$ by max. 0.04–0.4 °C with $\alpha = 45\text{--}90^\circ$
- ◆ Uncertainty of radiation correction, $U(\Delta T_{\text{rad}}) = 0.14^\circ\text{C}$
- ◆ Uncertainty of corrected temperature, $U(T_{\text{cor}}) = 0.17^\circ\text{C}$
- ◆ Uncertainty of soundings should be added to $U(T_{\text{cor}})$
- ◆ Any type of radiosonde can be tested using the UAS at KRISS

Thank you for your attention

More discussions to sangwook@kriss.re.kr