



(I) Radiation experiments:

First results for RS41 from MOL wind channel setup

(II) Relative humidity time lag for RS41

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(I): Radiation tests (RS41)

- Motivation: Restrictions of earlier results from 'old' chamber (current RS41-GDP-ALPHA.2)
- MOL wind channel:
 - Description of new setup
 - First results: T -response depending on irradiance, pressure, ventilation, 'sun elevation angle'
 - Intended procedure for deriving a new radiation correction
- Conclusions

(II): Time lag for rel. humidity (RS41)

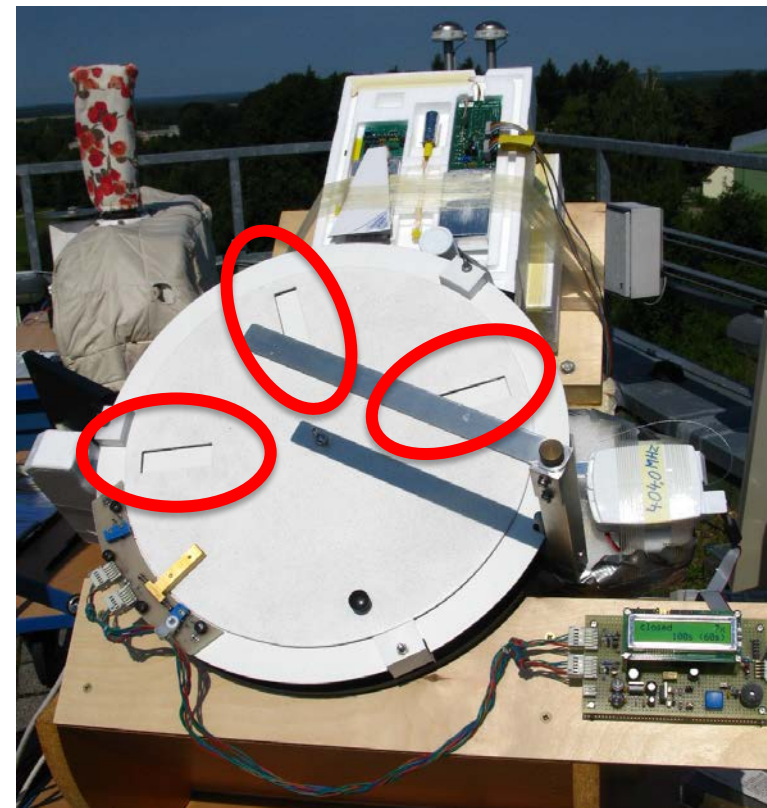
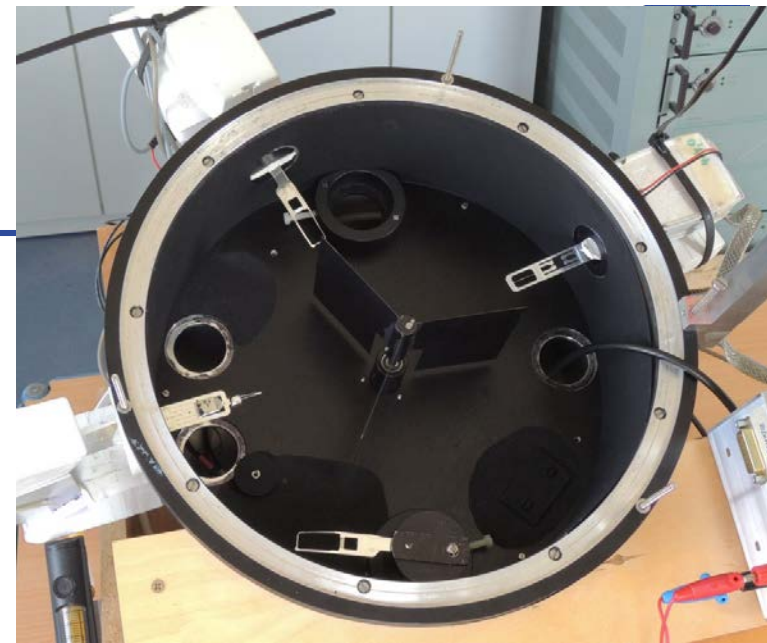
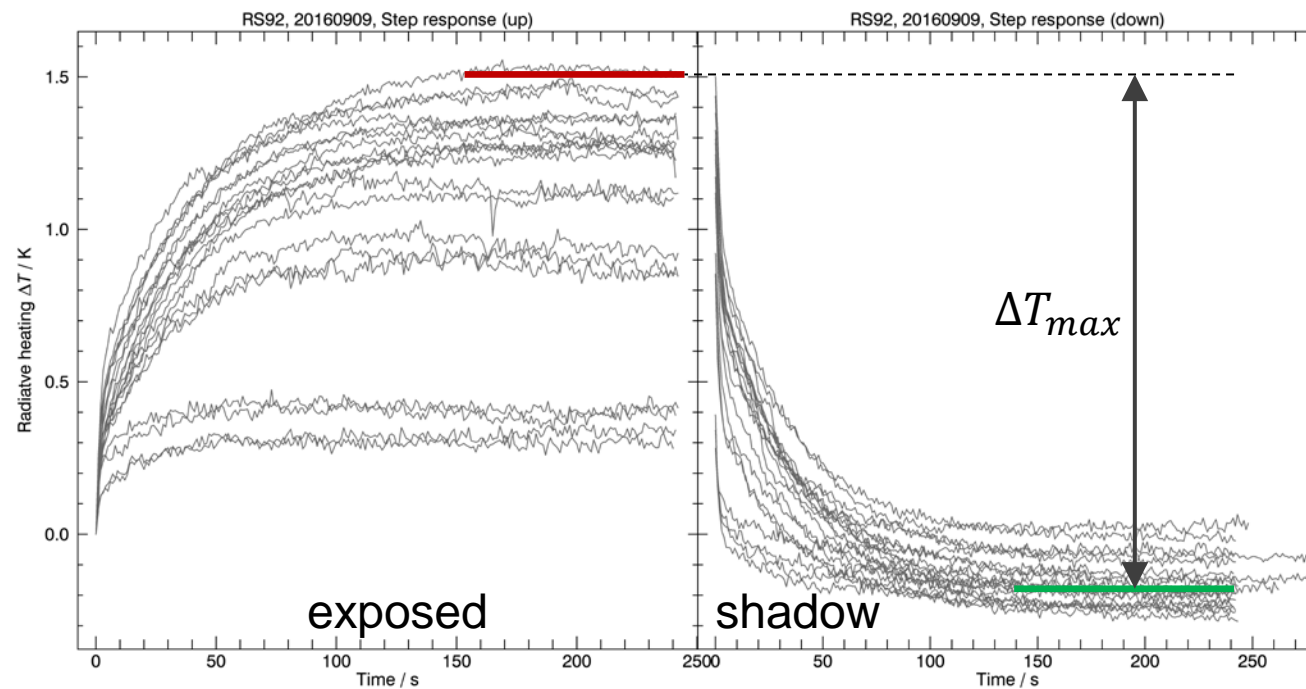
- Experimental setup
- Results
- Conclusions

(I) Radiation correction

Current approach

(RS41-GDP-ALPHA.2)

- Experimental basis:
Perpendicular irradiation of one side of **sensor boom** → maximum ΔT (thermal equilibrium)



(I) Radiation correction

Current approach

(RS41-GDP-ALPHA.2)

- Experimental data: $\Delta T_{\max}(I, p, v)$
- Model to transfer experimental results to operational correction:
→ Include orientation changes (sonde rotation)

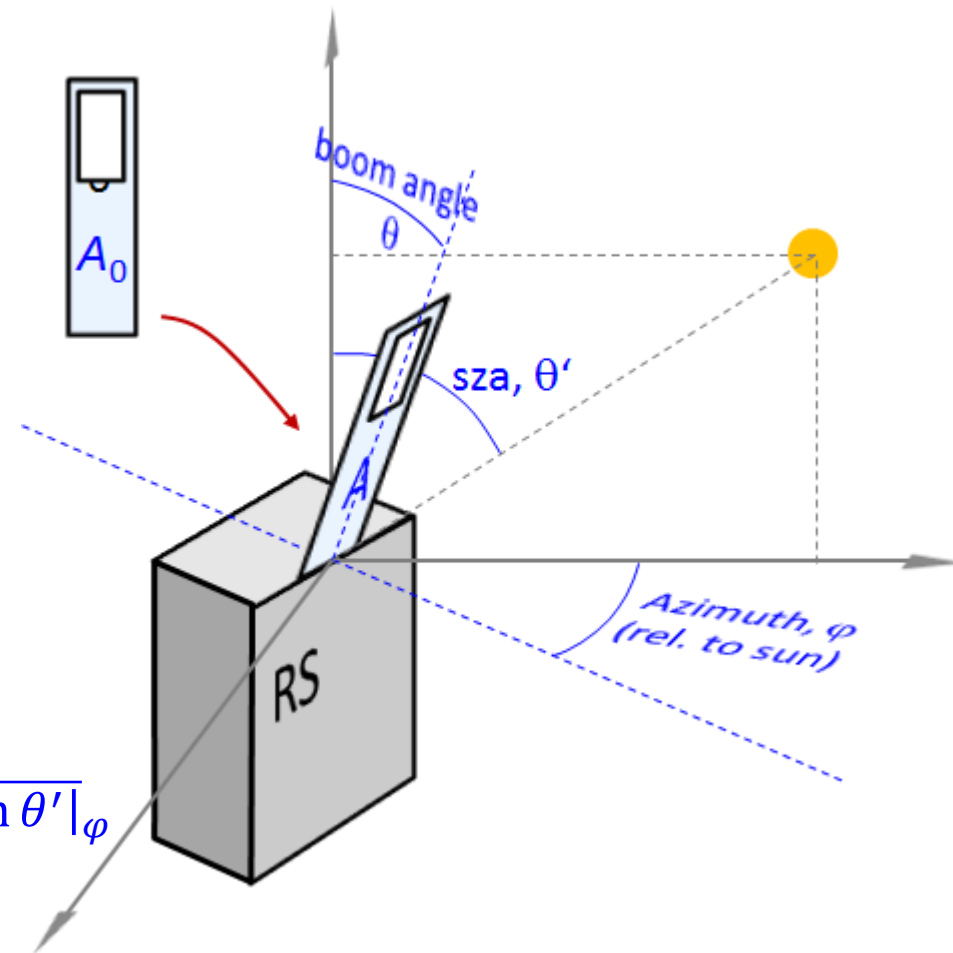
Scale direct comp. of actinic flux with *effective* area of sensor boom as seen from sun *after averaging over a full φ -rotation* (I_{dir} and I_{diff} from RT-simulation):

$$I_a = I_{\text{diff}} + f_{\text{geo}} \cdot I_{\text{dir}}$$

$$f_{\text{geo}} = \overline{A/A_0} \Big|_{\varphi} = \overline{|\cos \theta \cos \theta' - \sin \theta \cos \varphi \sin \theta'|} \Big|_{\varphi}$$

- T -bias (correction): $\Delta T = a \cdot \left(\frac{I_a}{p^j \cdot v^k} \right)^b$

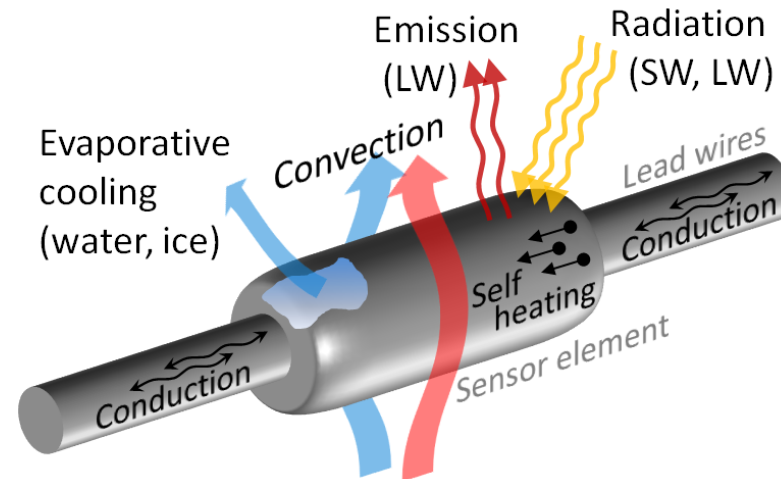
a, b, j, k from fits to experimental data



(I) Radiation correction

Current approach

(RS41-GDP-ALPHA.2)



- Problem: T -response result of numerous T -compensation processes:
 - Different parts of sensor boom heated to different extents
 - Overlay of different time constants for heat flow components
- Ascent: Irregular changes of rel. orientation to sun (rotation, pendulum)
 - Variance in effective irradiation and ventilation
 - Variable forcing and smoothing of T -signal; *probably never in equilibrium*

Simple model using f_{geo} does not include temporal behavior
(assumes *instantaneous* and *uniform* warming of boom and sensor element)

(I) Radiation correction MOL wind channel: Setup

- New experimental approach:

Better reproduce real sounding conditions.

1) Arrange direction of ventilation and radiation relative to the orientation of sensor boom similar to real soundings

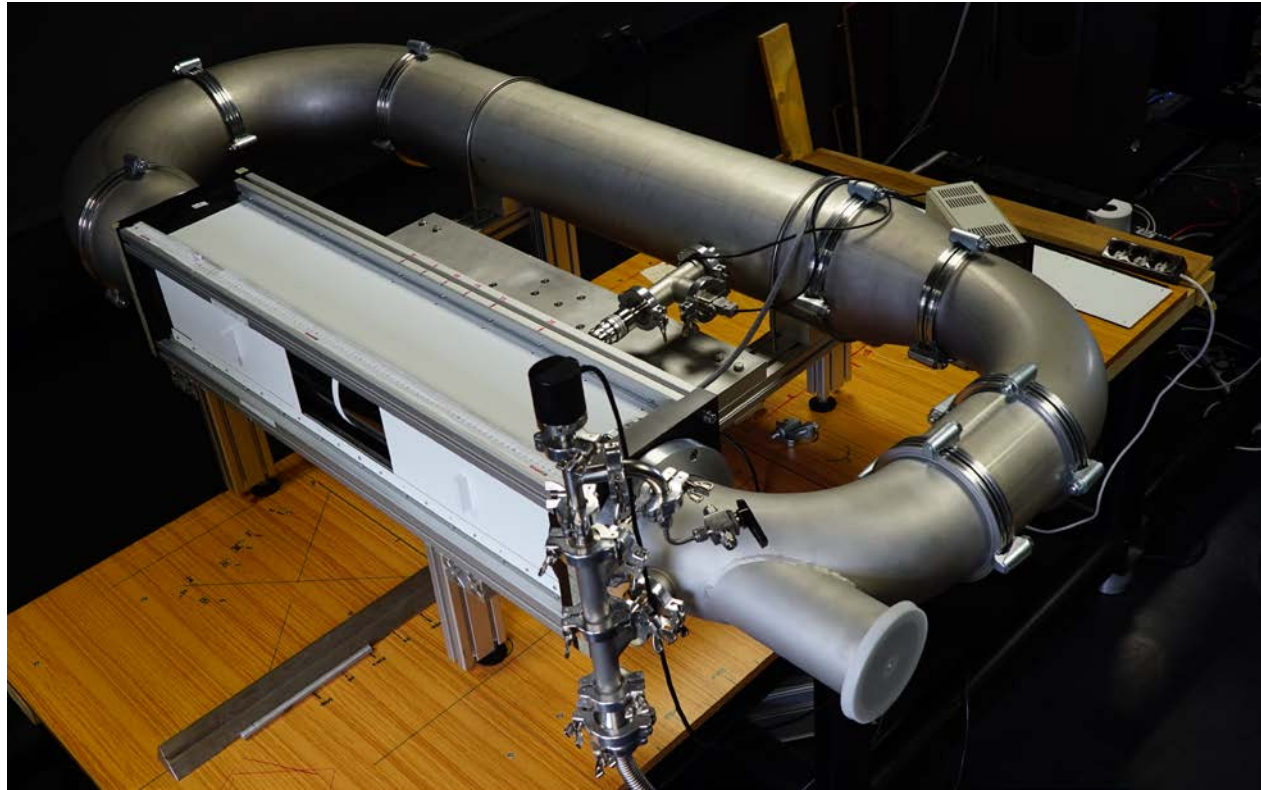
2) ‚Dynamical‘ measurements:

Continuous rotation of test sonde during irradiation;

Evaluate T -response as mean value over several (azimuthal) rotations

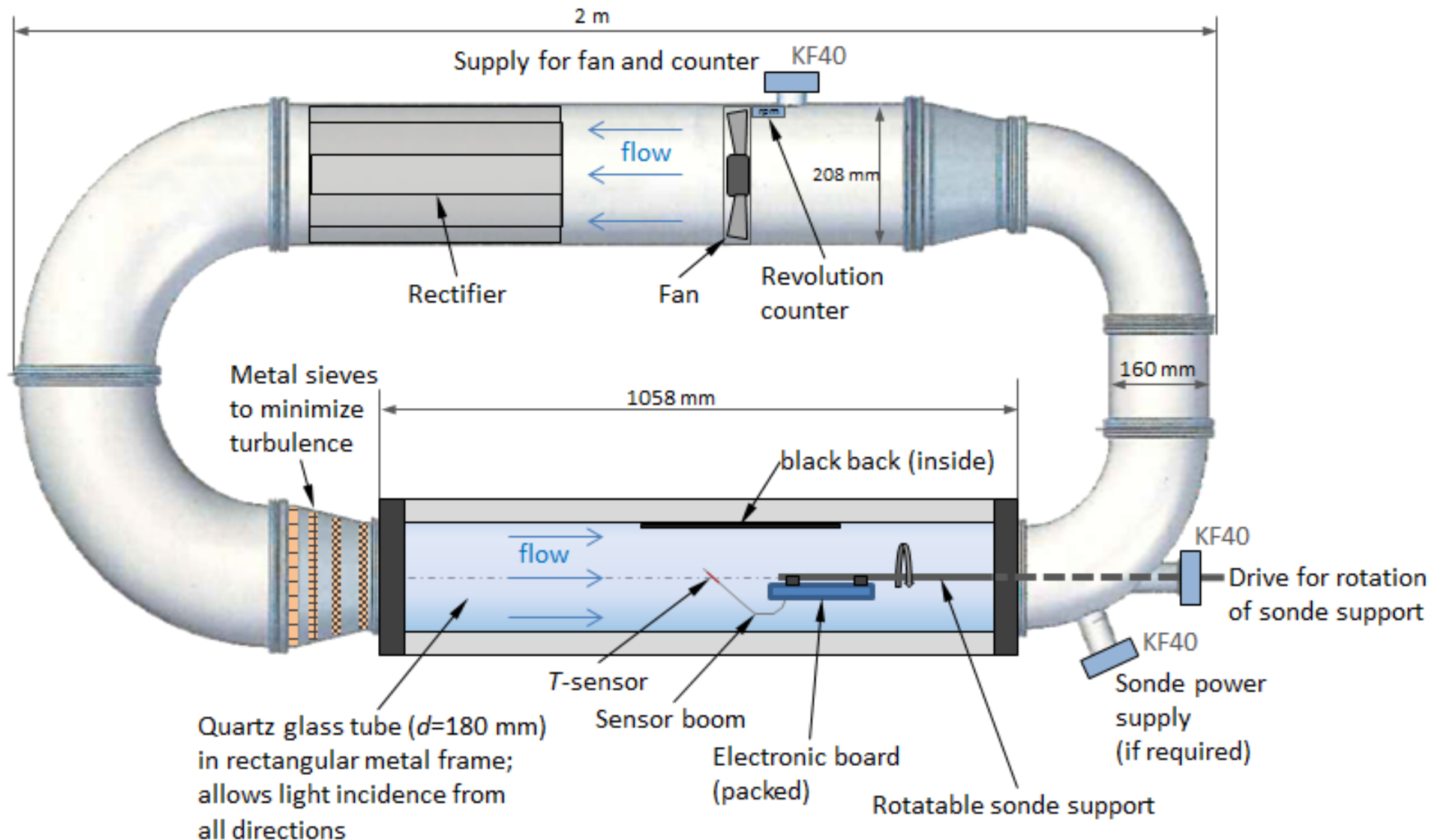
Empirical approach to measure the effective ΔT
(= average over some 10 s) directly

(I) Radiation correction MOL wind channel: Setup



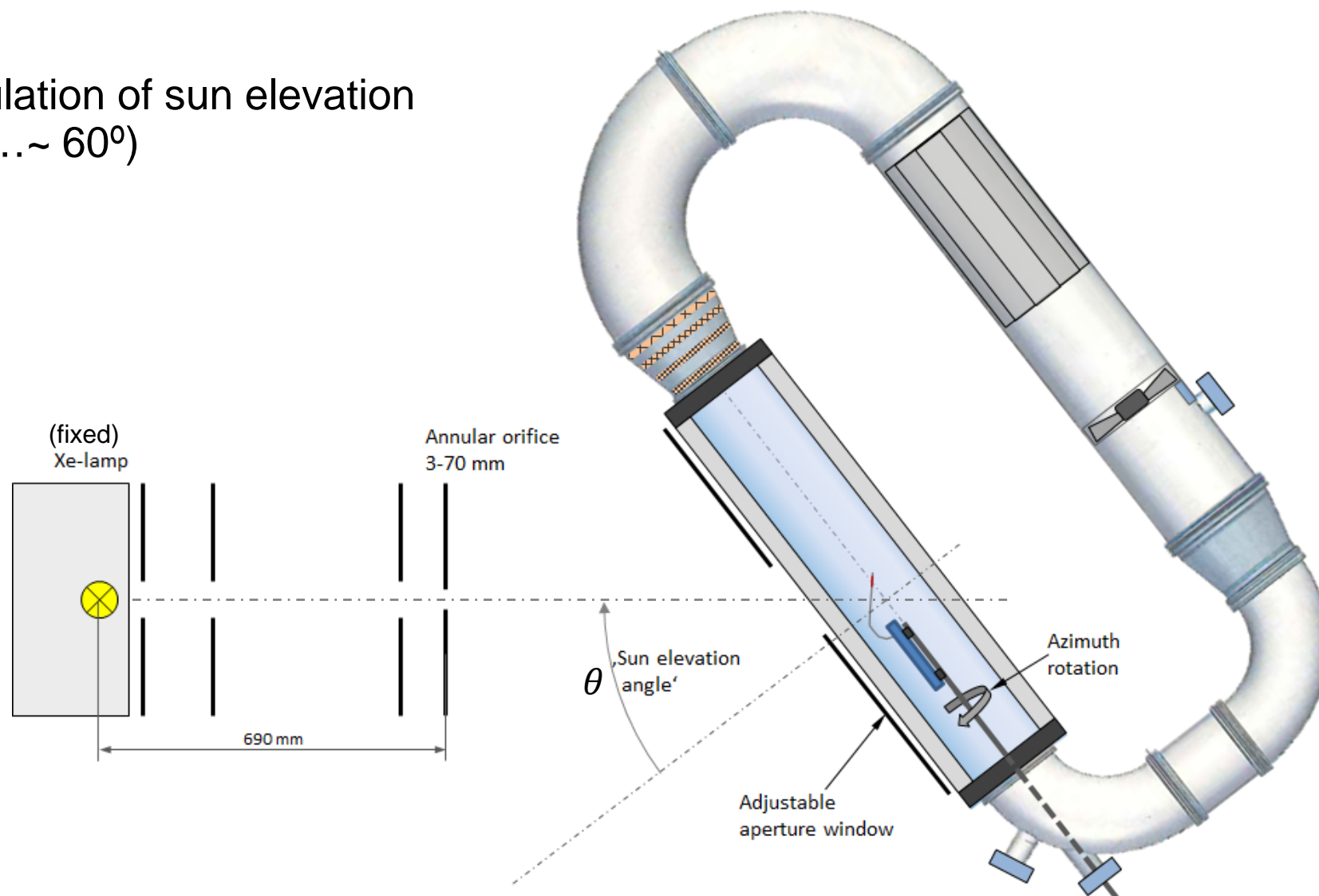
- Evacuatable wind tunnel, $p = (3 \text{ to } 1000) \text{ hPa}$
- Quartz glass tube ($l=1 \text{ m}$, $\varnothing 180 \text{ mm}$) as test volume: sonde installation (w/o housing)
- Air flow: circulating, control by fan revolution
- Variable angles of incident radiation: free rotation of sonde (azimuth) + simulation of SEA

(I) Radiation correction MOL wind channel: Setup



(I) Radiation correction MOL wind channel: Setup

Simulation of sun elevation
($0^\circ \dots \sim 60^\circ$)



(I) Radiation correction

New experimental setup:

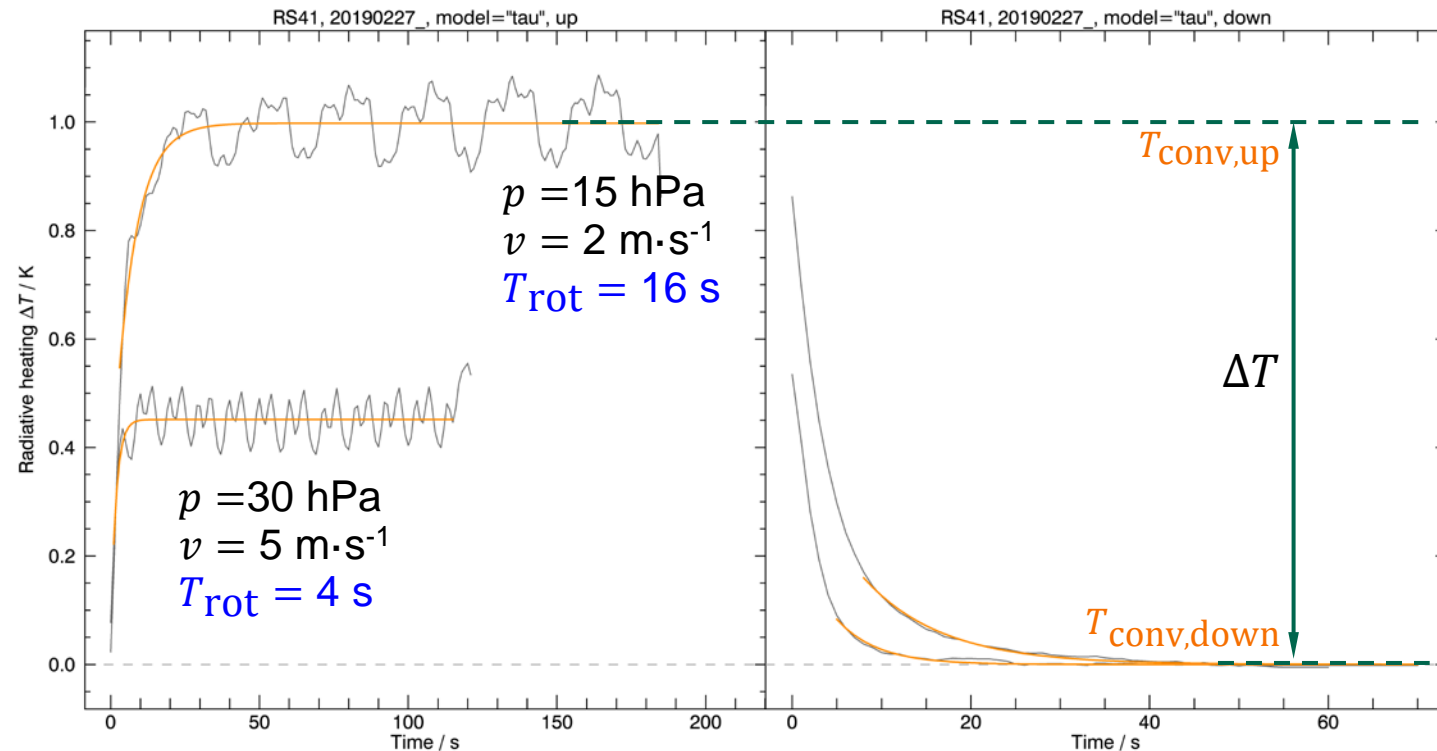
First results

- Continuous rotation:

- Uniform turning of sonde during periods of light incident
- Irradiation period until quasi-equilibrium (‘constant’ oscillation)
- ΔT determined by **average** value over oscillation

Fit function (‘up’ an ‘down’):

$$\Delta T = T_{\text{conv}} + c \cdot \exp\left(-\frac{t}{\tau}\right)$$



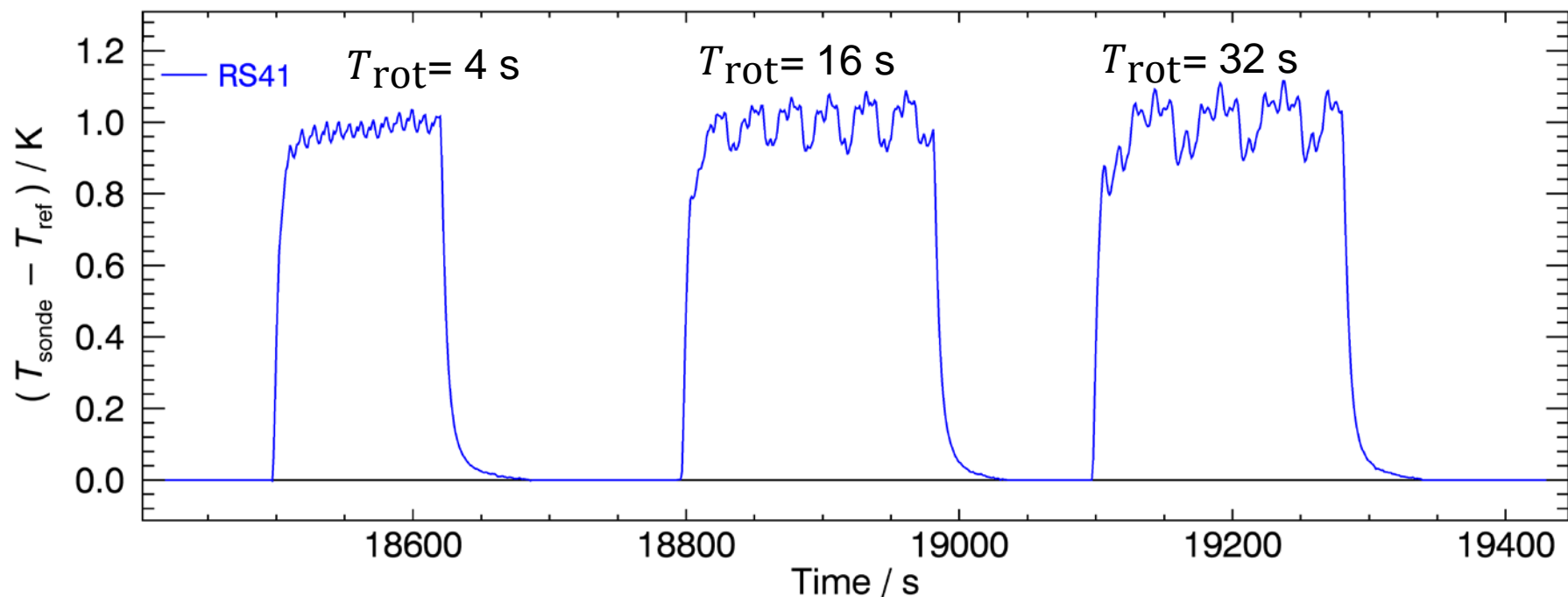
(I) Radiation correction

New experimental setup:

First results

- Continuous rotation:
 - Test of different frequencies for φ -rotation: $T_{\text{rot}} = 4, 16, 32 \text{ s}$
→ ΔT sensitive to T_{rot} ?

$v = 2 \text{ m}\cdot\text{s}^{-1}$, $p = 15 \text{ hPa}$, $I_a = 1156 \text{ W}\cdot\text{m}^2$, $\text{SEA} = 0^\circ$

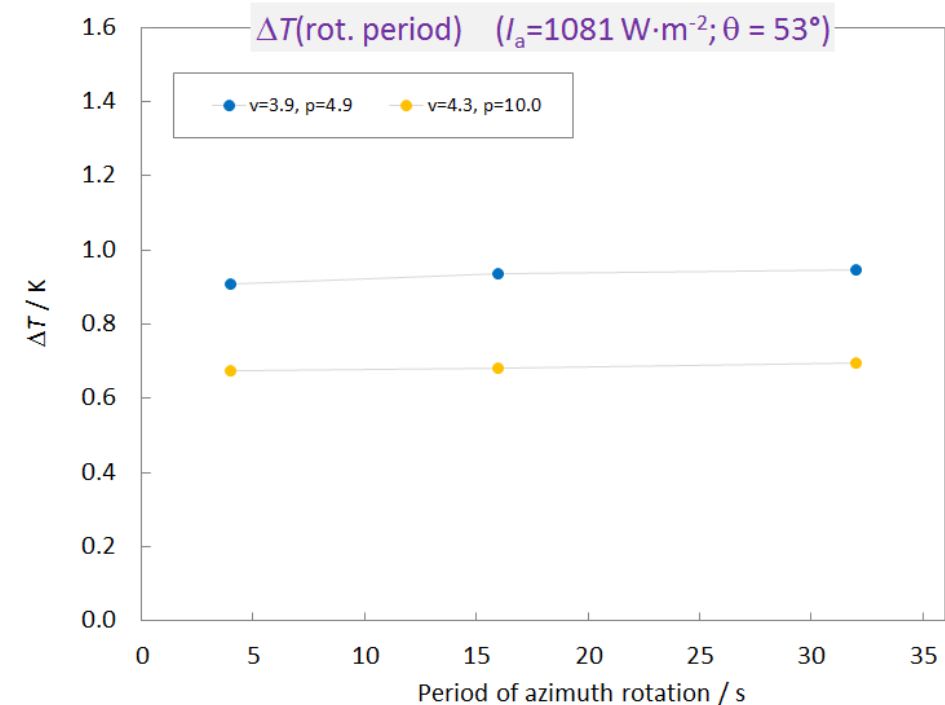
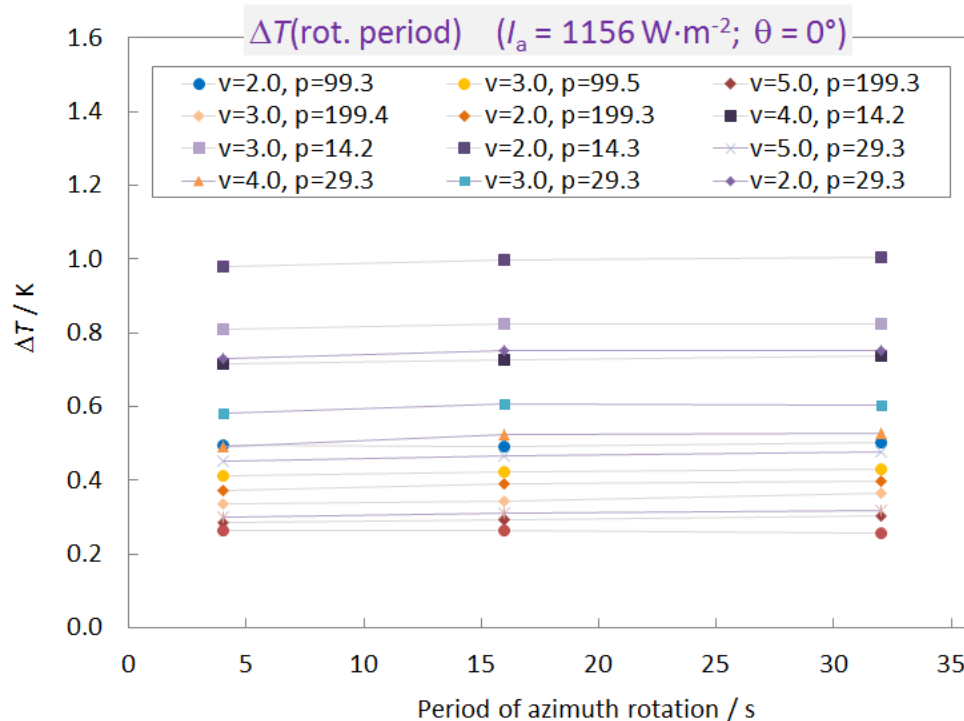


(I) Radiation correction

New experimental setup:

First results

- Continuous rotation:
 - Test of different frequencies for φ -rotation: $T_{\text{rot}} = 4, 16, 32$ s
→ ΔT sensitive to T_{rot} ? → No.

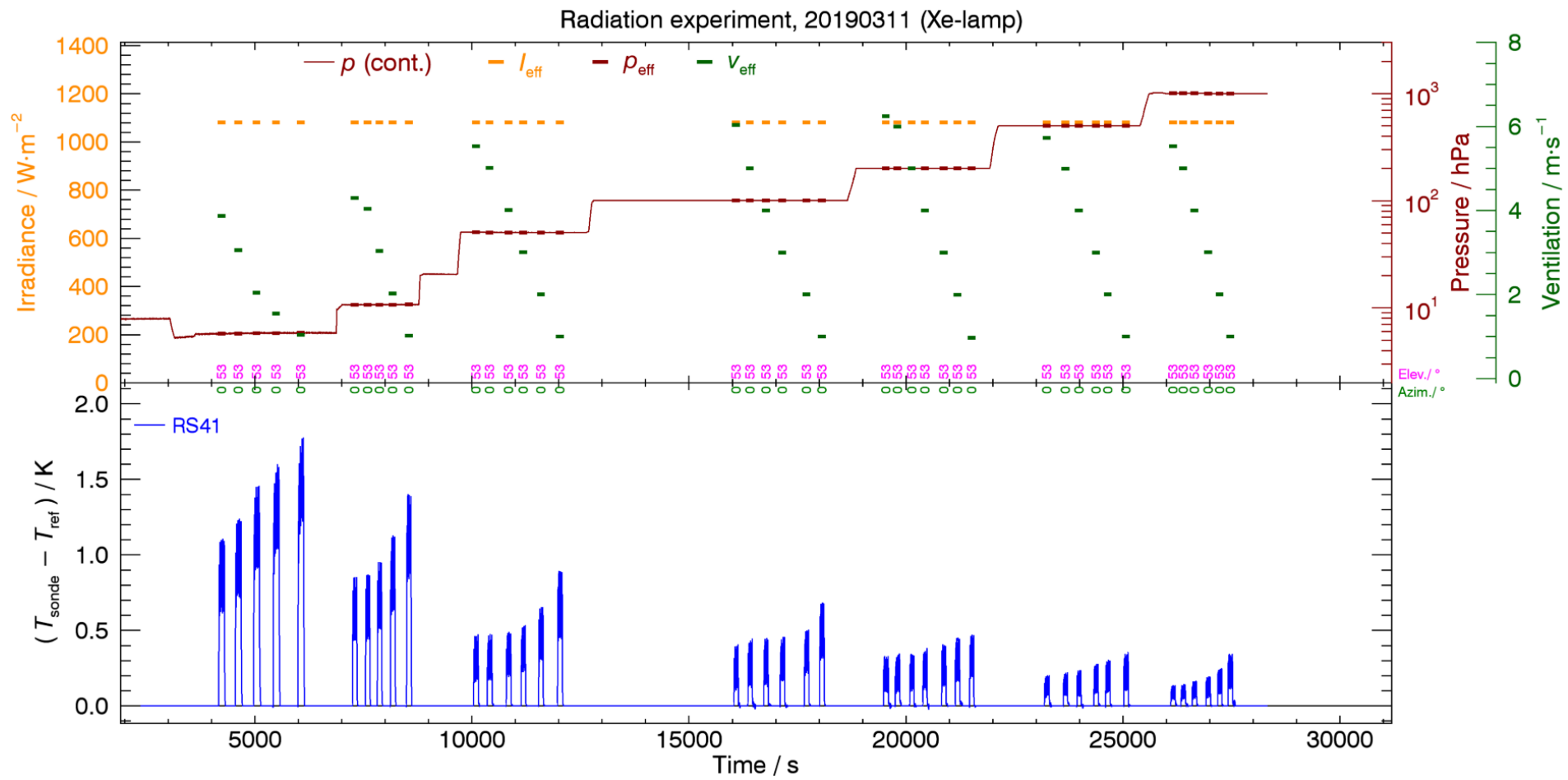


(I) Radiation correction

New experimental setup:

First results

- Example for $I_a = 1081 \text{ W}\cdot\text{m}^2$, $\theta(=\text{SEA}) = 53^\circ$, p and v variable

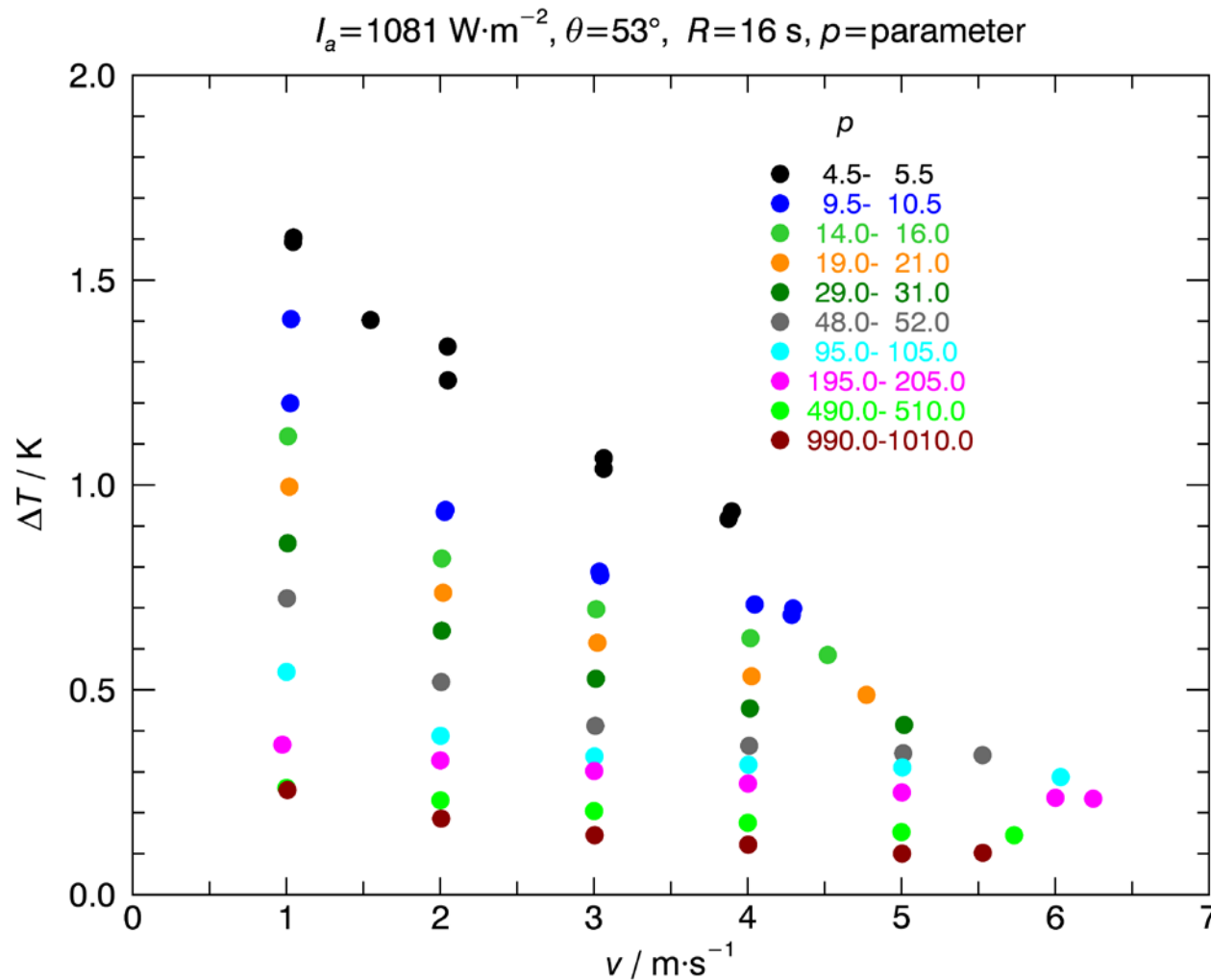


(I) Radiation correction

New experimental setup:

First results

- Ventilation

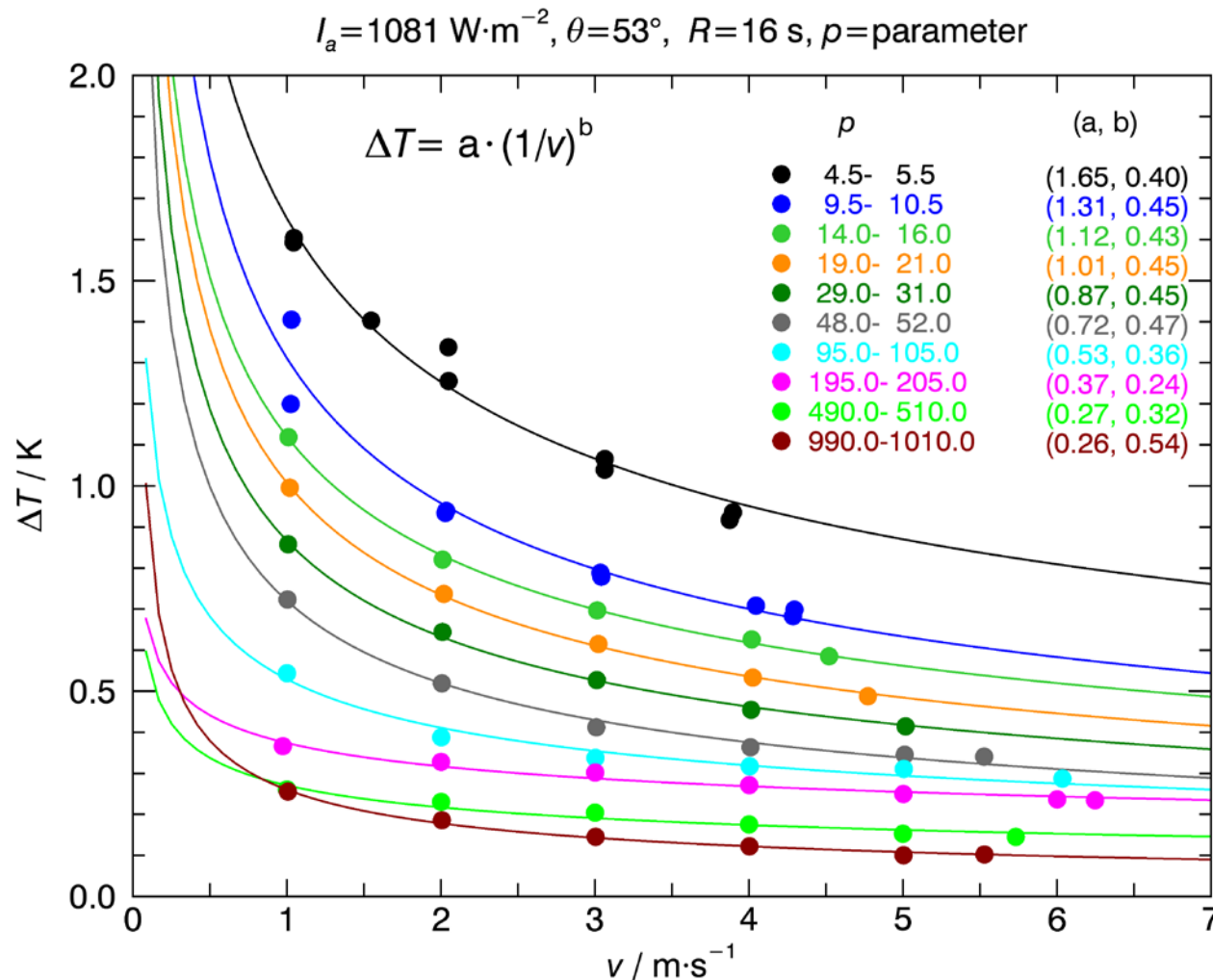


(I) Radiation correction

New experimental setup:

First results

- Ventilation

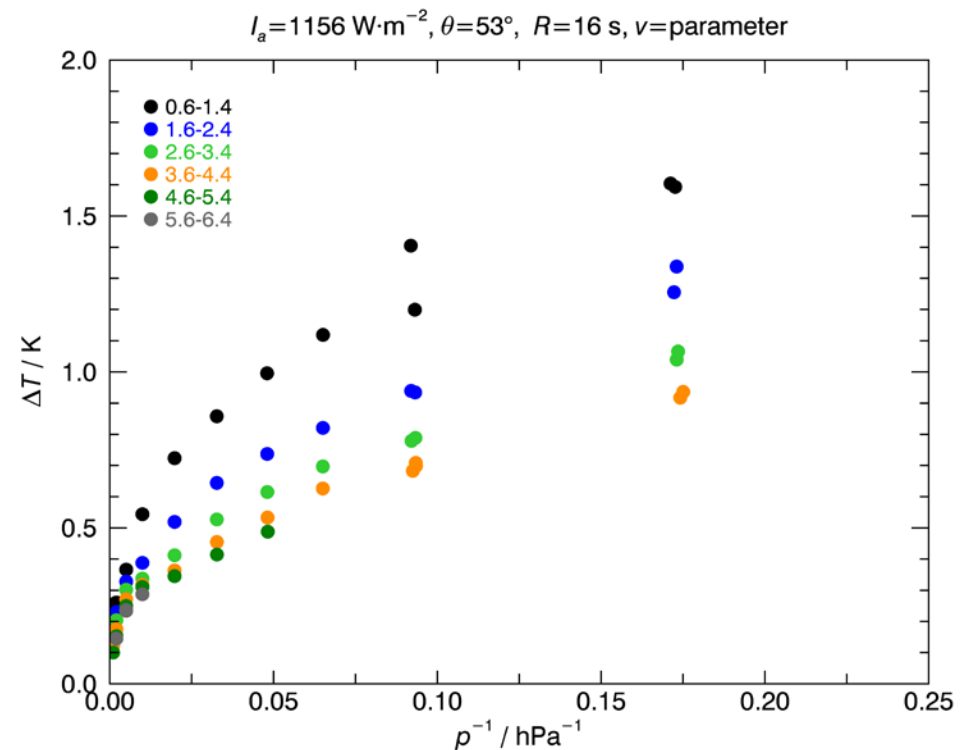
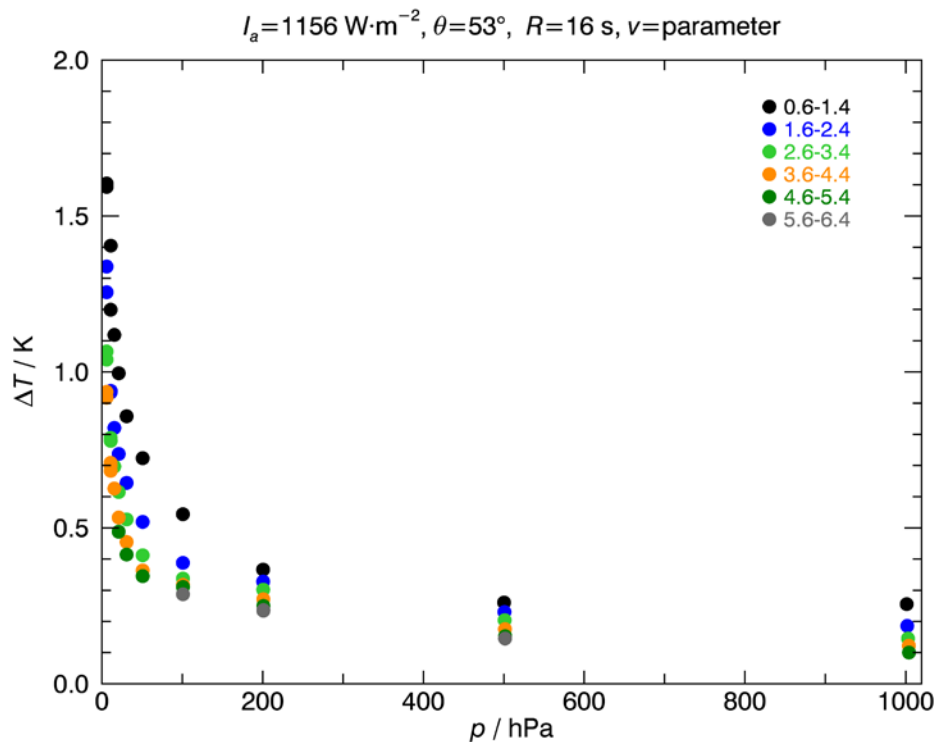


(I) Radiation correction

New experimental setup:

First results

- Pressure

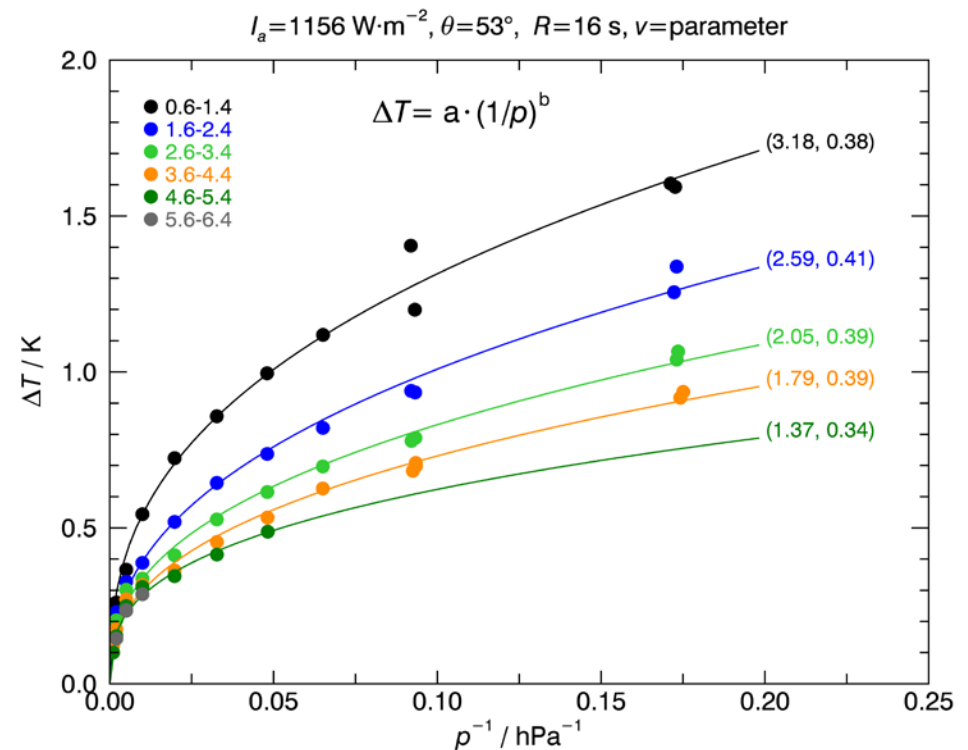
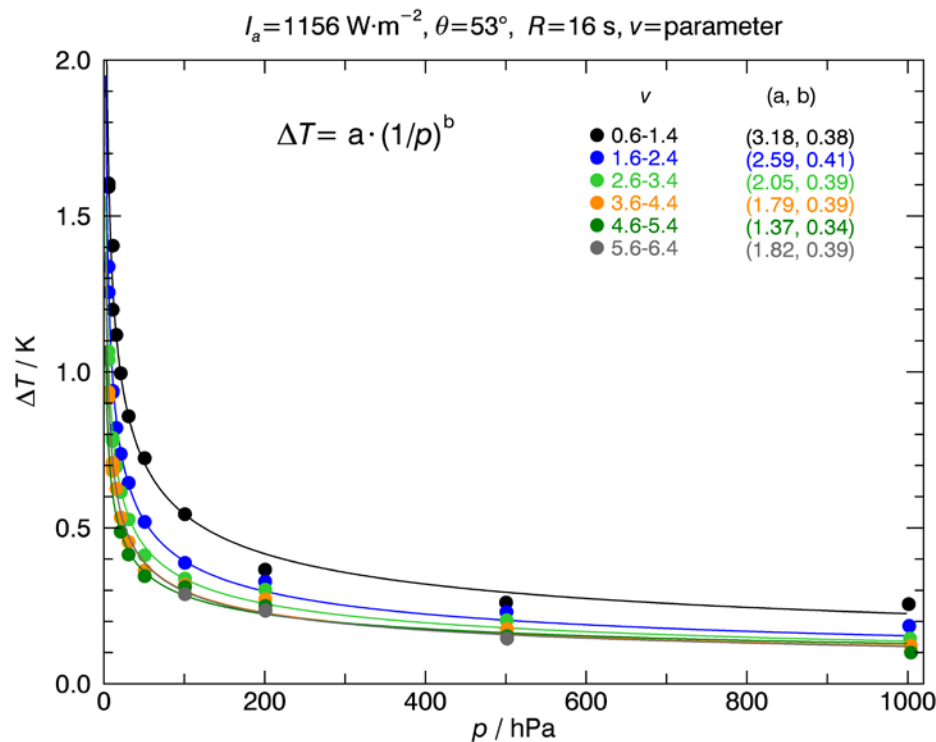


(I) Radiation correction

New experimental setup:

First results

- Pressure



(I) Radiation correction

Measurement plan and intended derivation of radiation correction

- ΔT shows smooth and systematic dependence on p and v
- 1) Select fixed setting for I_a , $\sim(1000-1500) \text{ Wm}^{-2}$
 - 2) - Measure ΔT as function of p and v for
 $p = (5, 10, 15, 20, 30, 50, 100, 200, 500, 1000) \text{ hPa}$
 $v = (1, 2, 3, 4, 5, 6, 7, 8, \dots) \text{ m s}^{-1}$
as average over continuous azimuth rotation with $T_{\text{rot}} = 16 \text{ s}$;

- Derive expression for $\Delta T(p, v)$ (2D-non linear regression)
 - 3) Repeat 2) for several settings of SEA ($= \theta$)
 - 4) Create look-up table from 3) to interpolate for any θ
 - 5) Scale ΔT linearly with I_a

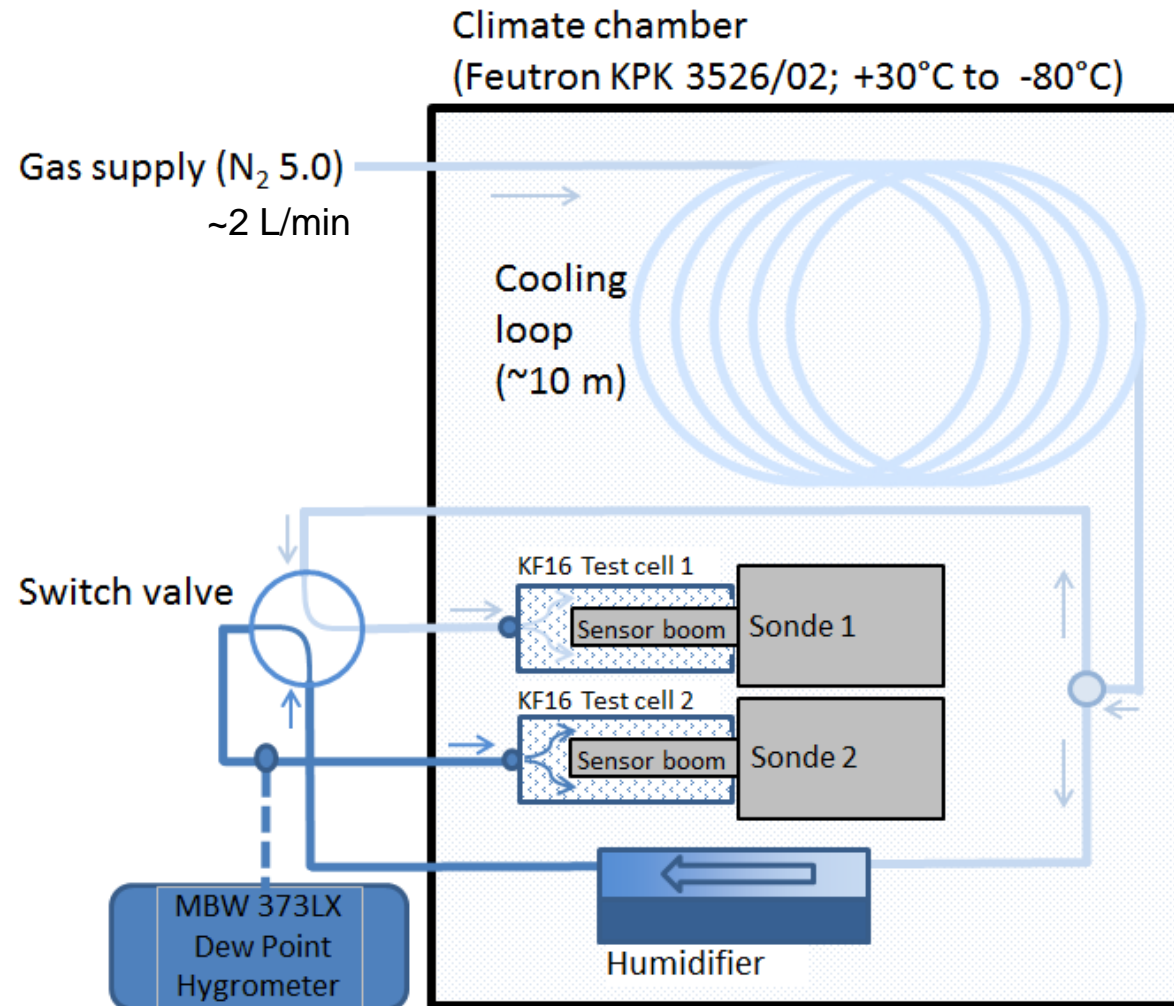
- New setup for radiation experiments operational (some constructive issues to be finished)
- First results for RS41 from ‚dynamical‘ measurements auspicious
- To be discussed/resolved:
 - Role of absolute temperature (see KRISS experiments)
 - More information about sonde movements (rotation) during real ascents needed to support exp. approach
- Time line:
 - Continuation of measurements with RS41 in Summer/Autumn 2019; evaluation and derivation of radiation correction; implementation in RS41-GDP

(II) RH Time lag RS41: Objective

- **Objective:**
Long response times of polymer sensor at low T ,
→ considerable time lag (smoothing) in UT and tropopause
(especially tropics)
- **Solution:** Apply time-lag correction based on measured sensor response behavior
- **Experimental approach / evaluation:**
 - Measure step response of rel. humidity over atmospheric T -range;
Assumption: response can be described with single time constant $\lambda = 1/\tau$
 - Evaluate response time τ as '63 %'-time for each step
 - Parameterize response time $\tau(T)$

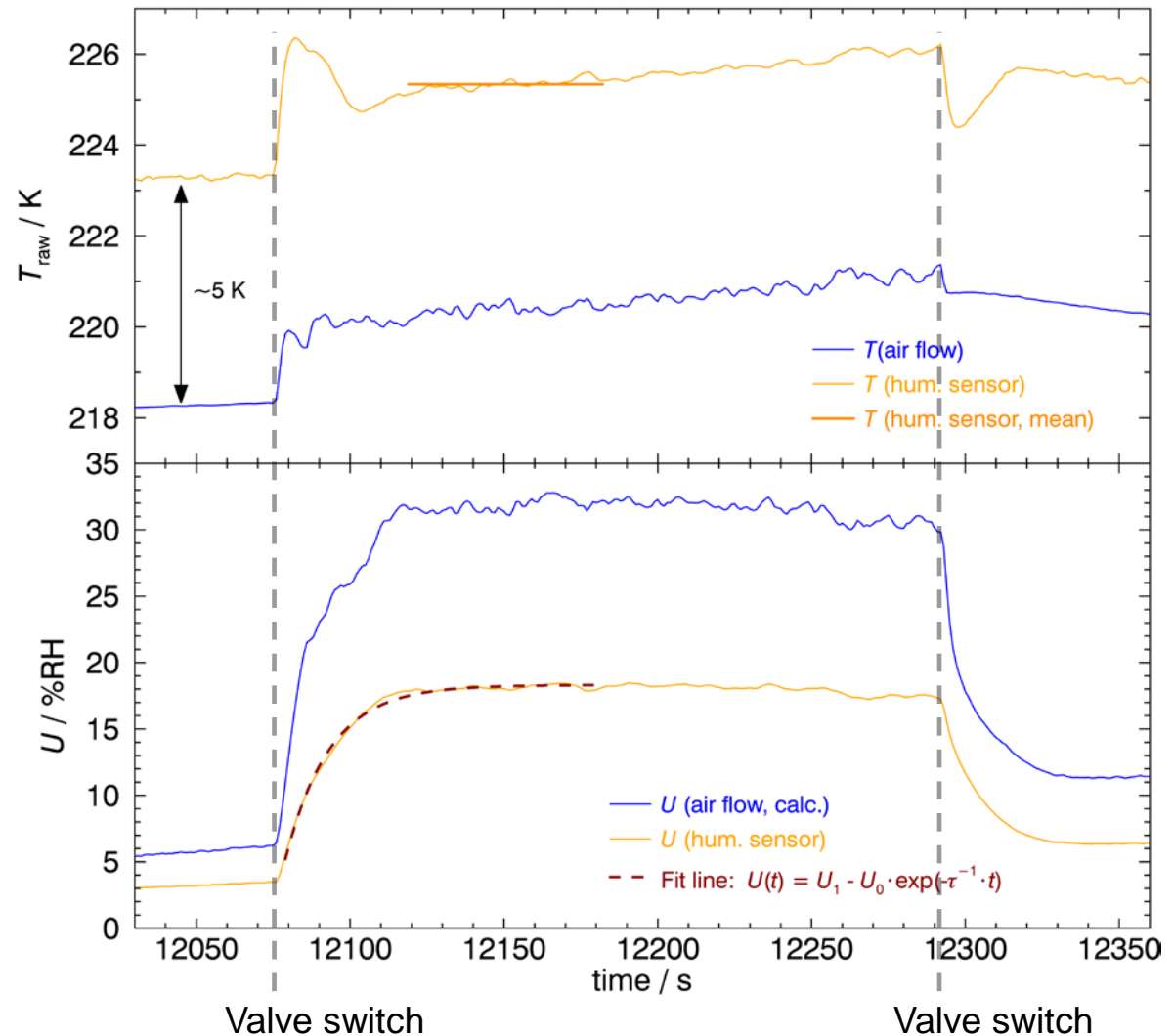
(II) RH Time lag RS41: Setup

- Step-like humidity changes by quick switches from dry to humid air flow over sensor boom
- Efficiency of humidifier not controlled
- Selection of T -points during self-warming of chamber (-70 °C ... -10 °C; T in chamber not stabilized after initial cooling phase)
- Valve outside chamber; switched by hand



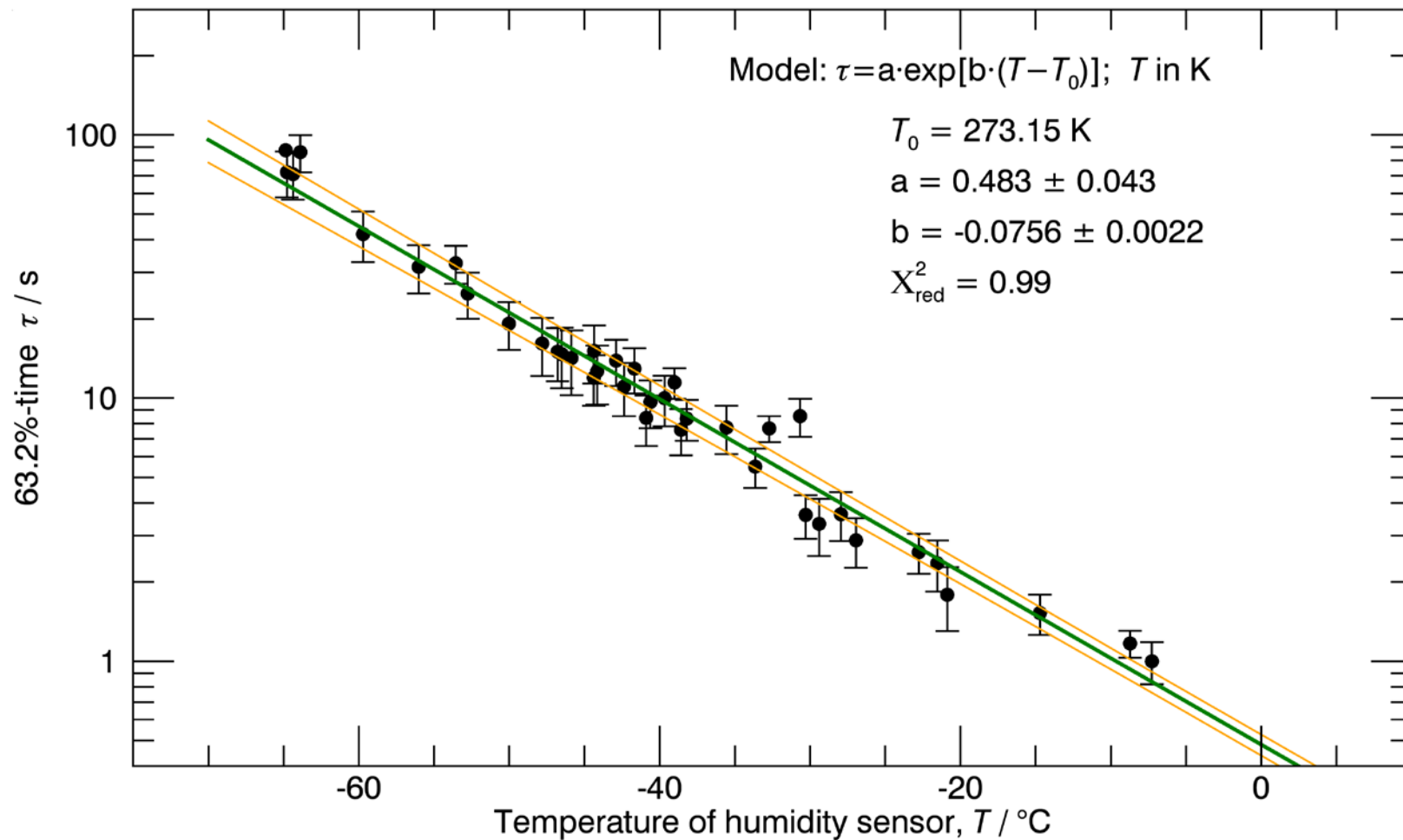
(II) RH Time lag RS41: Results

- U -sensor kept ~ 5 K above ambient air
 - τ derived for 'internal' U
 - τ related to 'internal' T (T of U -sensor)
- T at plateau taken as reference for U -response
- τ estimated from regression curve (fit parameter)



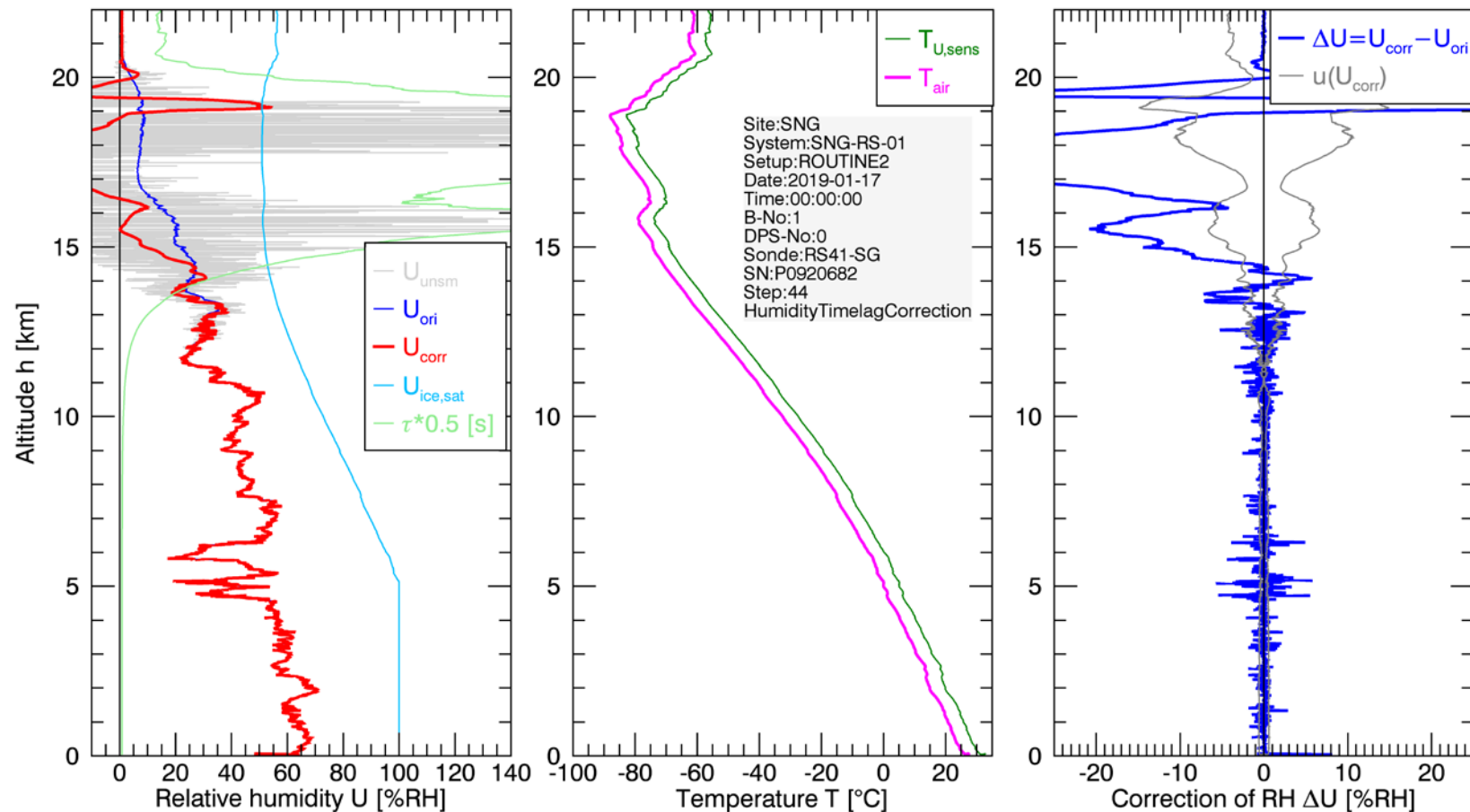
(II) RH Time lag RS41: Results

- Parameterization $\tau(T)$, T = temperature of humidity sensor



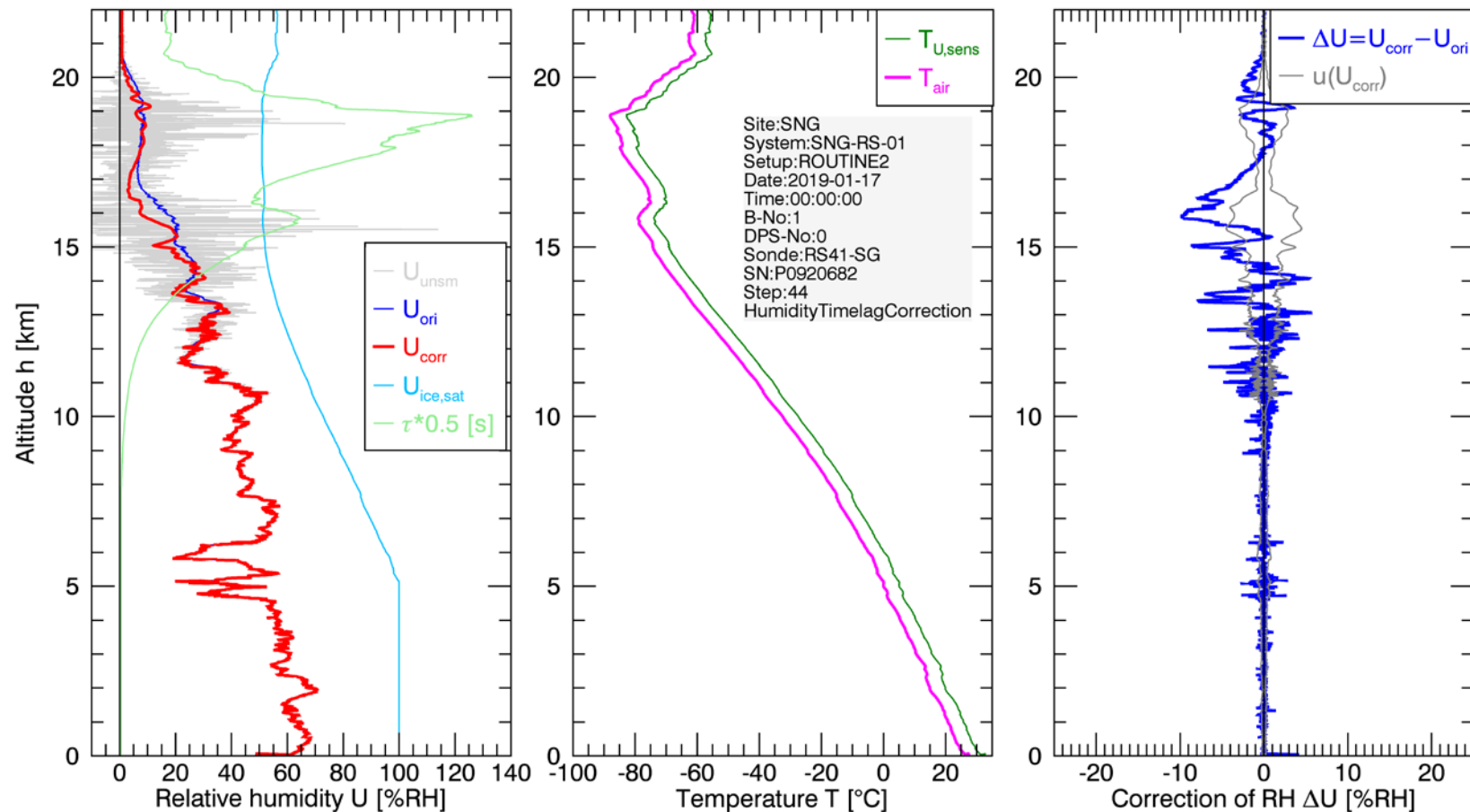
(II) RH Time lag RS41: Example (RS41-GDP-ALPHA.2)

SNG, 2019-01-17, 00:00:00, 'internal' rel. humidity



(II) RH Time lag RS41: Example (RS41-GDP-BETA)

SNG, 2019-01-17, 00:00:00, 'internal' rel. humidity



- Step response of RS41 humidity sensor measured at temperatures between 0 °C and -70 °C
- Re-analysis leads to more consistent time-lag correction for RS41
- Implementation in next version of RS41-GDP
- Measurements done at normal pressure:
→ transferrable to lower p of atmospheric profile?

Thank you.

Supplementary

(I) Radiation correction

New experimental setup:

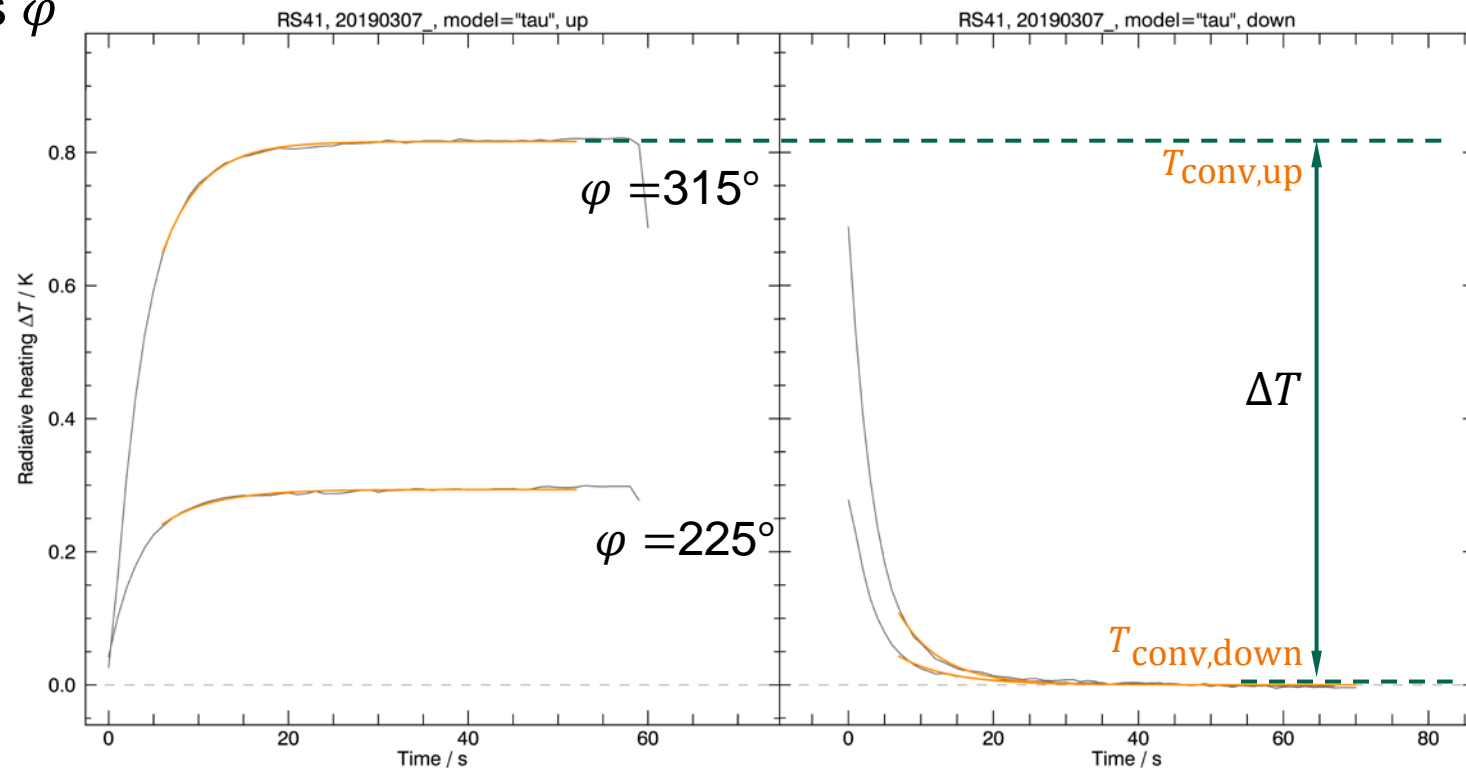
First results

Fit function ('up' and 'down'):

$$\Delta T = T_{\text{conv}} + c \cdot \exp\left(\frac{t}{\tau}\right)$$

- 'Static' measurements:
 - No continuous sonde rotation
 - fixed 'azimuth' angles φ
 - thermal equilibrium

$$p = 10 \text{ hPa}, v = 4.3 \text{ m}\cdot\text{s}^{-1}, \theta = 53^\circ$$

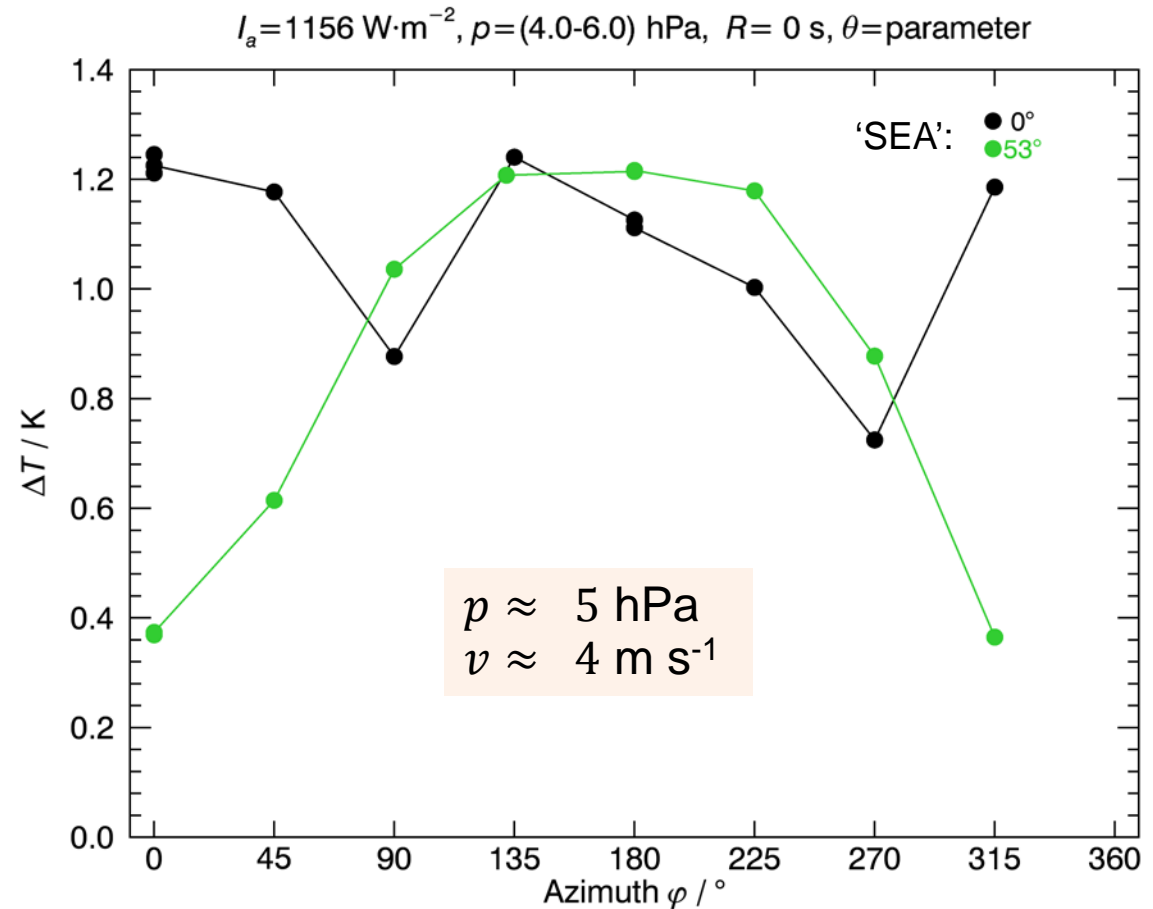


(I) Radiation correction

New experimental setup:

First results

- ,Static' measurements:
 - No continuous sonde rotation
 - fixed 'azimuth' angles φ
 - thermal equilibrium



(I) Radiation correction

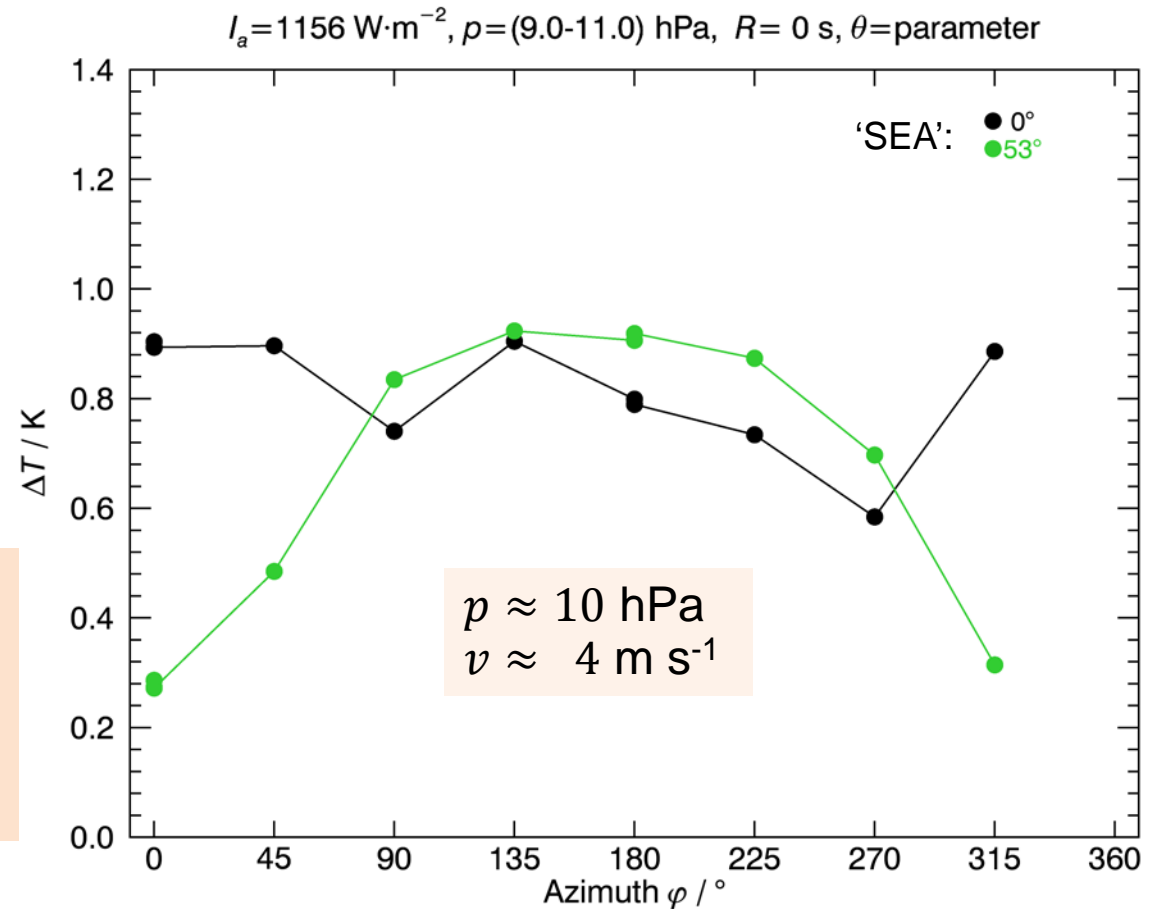
New experimental setup:

First results

- 'Static' measurements:
 - No continuous sonde rotation
 - fixed 'azimuth' angles φ
 - thermal equilibrium

→ Direction of incident radiation determines ΔT

→ Considerable proportion of ΔT from sensor boom



(I) Radiation correction Setup: Ventilation

$$v(p, f_{rot}) = c_{00} + c_{10}p^{1/2} + c_{20}p + c_{30}p^{3/2} + c_{01}f_{rot}^{1/2} + c_{11}p^{1/2} \cdot f_{rot}^{1/2} + c_{21}p \cdot f_{rot}^{1/2} + c_{31}p^{3/2} \cdot f_{rot}^{1/2} + c_{02}f_{rot} + c_{12}p^{1/2} \cdot f_{rot} + c_{22}p \cdot f_{rot} + c_{32}p^{3/2} \cdot f_{rot}$$

$$R = (70-100) \text{ mm}$$

$$X^2 = 31.95$$

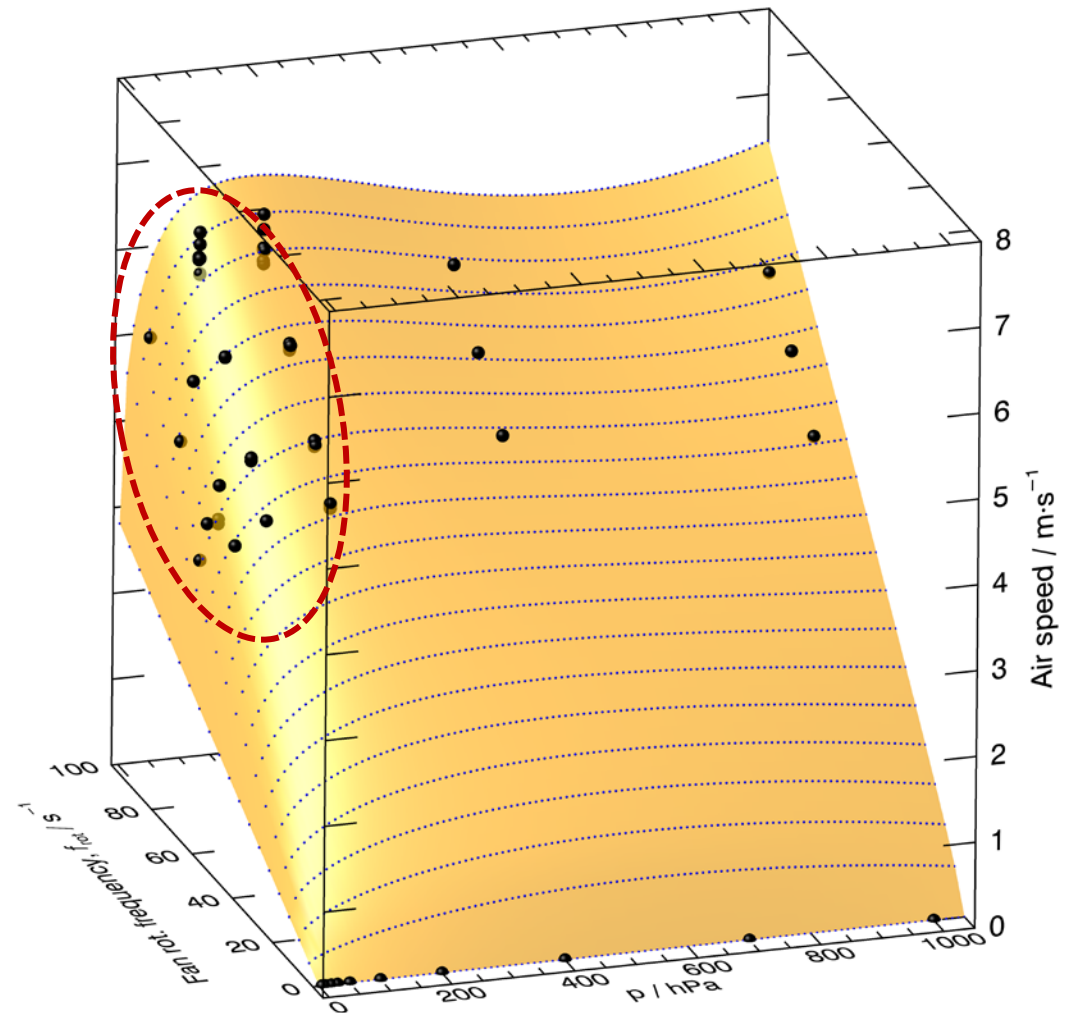
$$X_{red}^2 = 0.71$$

$$\text{deg}_p = 1.5$$

$$\text{deg}_{frot} = 1.0$$

$$\text{deg}_{comb} = 3.0$$

$$\begin{aligned} c_{00} &= 2.40651\text{E-}006 \\ c_{10} &= -6.00432\text{E-}007 \\ c_{20} &= 1.50143\text{E-}008 \\ c_{30} &= 6.76840\text{E-}011 \\ c_{01} &= -3.43153\text{E-}004 \\ c_{11} &= -1.30964\text{E-}002 \\ c_{21} &= 2.27332\text{E-}003 \\ c_{31} &= -5.52825\text{E-}005 \\ c_{02} &= 2.81044\text{E-}002 \\ c_{12} &= 7.87864\text{E-}003 \\ c_{22} &= -5.76137\text{E-}004 \\ c_{32} &= 1.11104\text{E-}005 \end{aligned}$$



- Air speed measured as cross-sectional profiles using Laser-Doppler-Anemometry (LDA)
- Derivation of expression for $v(p, f_{rot})$ for central axis of quartz cylinder at position in front of sensor boom (cylinder symmetry assumed)

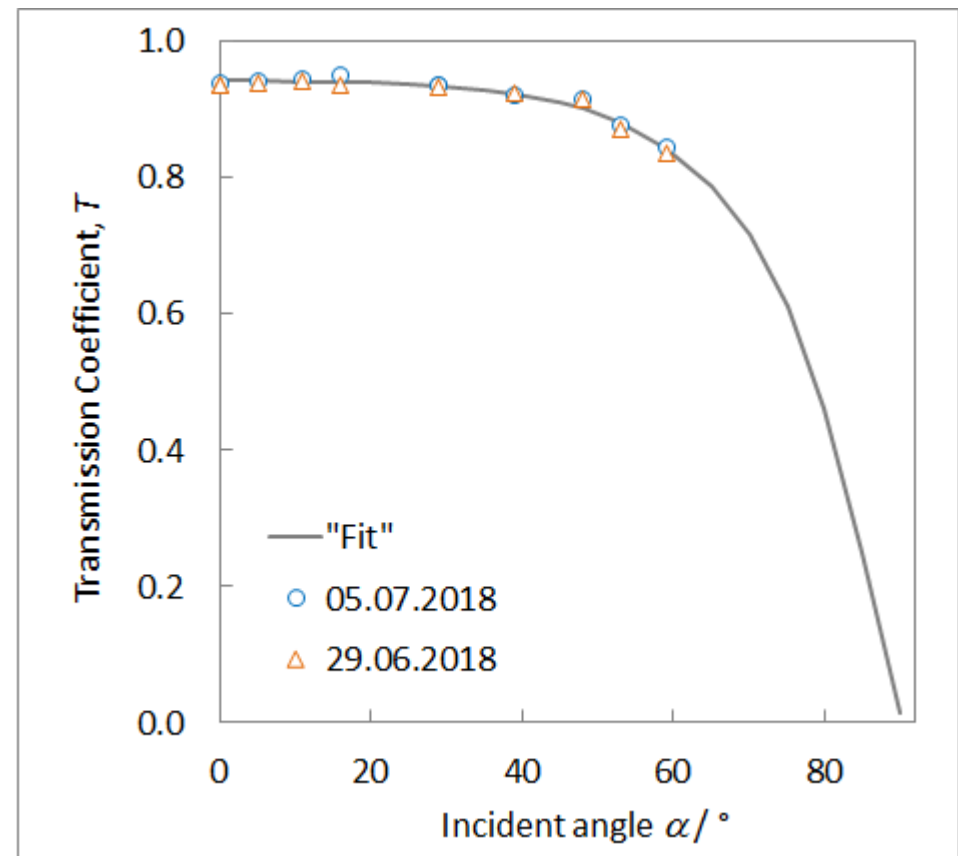
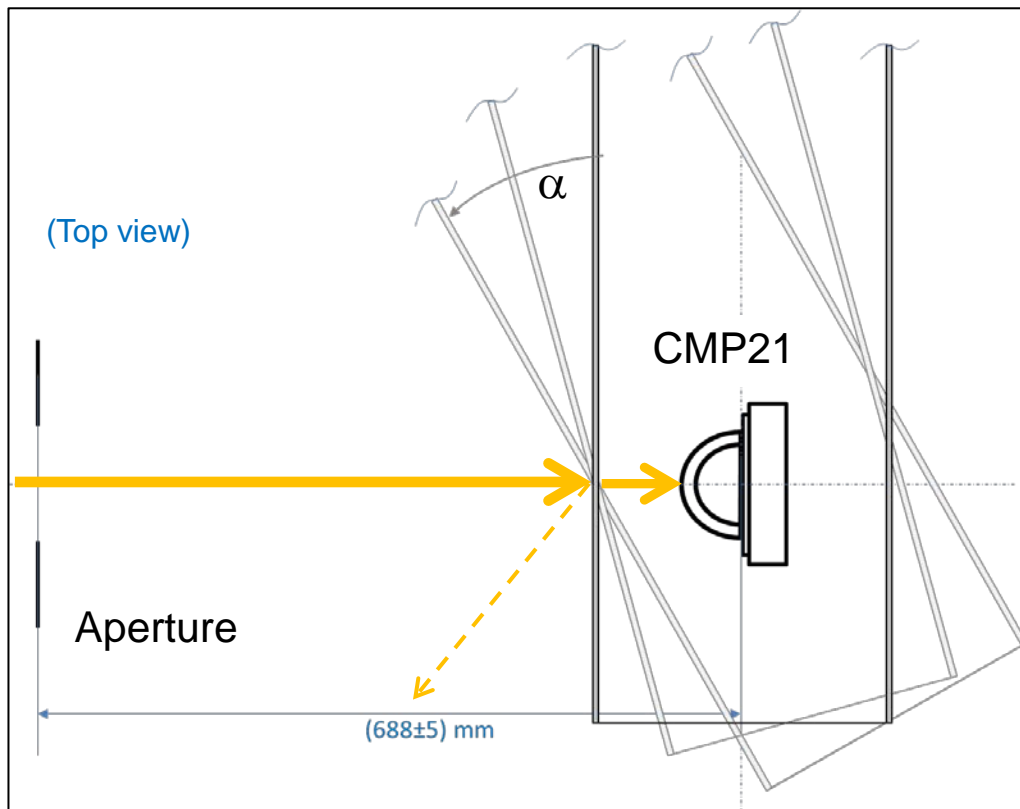
(I) Radiation correction

Setup: Transmission Quartz Cylinder

- Effective light transmission T measured by comparing irradiance inside and outside cylinder at different 'sun elevation' angles
- Empirical fit to data, based on Fresnel formula:

$$T = c_0 \cdot \frac{\tan(c_1 \cdot \alpha)}{\tan(c_3 \cdot \beta)} \cdot \left[\frac{2 \cos(c_2 \cdot \alpha)}{n_2 \cos(c_2 \cdot \alpha) + \cos(c_3 \cdot \beta)} \right]^2$$

$$\text{with } \beta = \sin^{-1} \left(\frac{\sin(c_1 \cdot \alpha)}{n_2} \right)$$



(I) Radiation correction

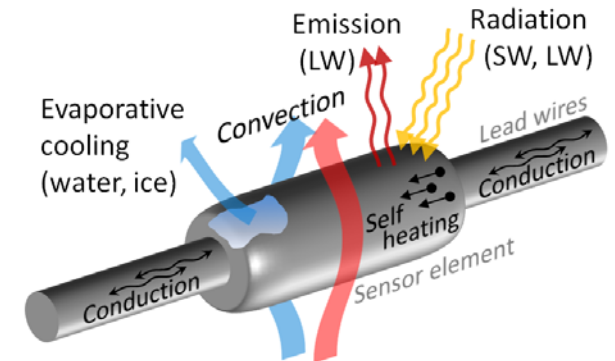
New experimental setup:

First results

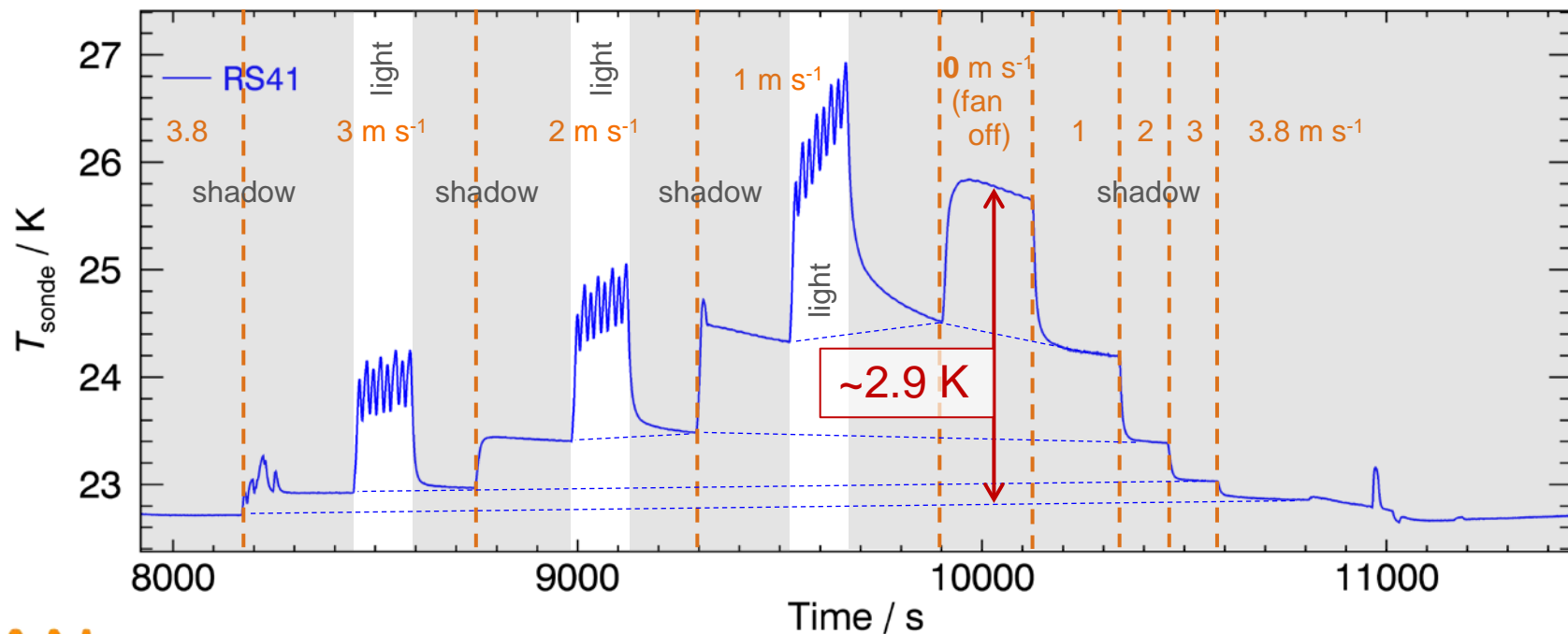
- ‚Contamination‘ from permanently heated (~ 5 K) humidity sensor

→ T sensitive to v at low ventilation ($< 4 \text{ m s}^{-1}$)

... Extra investigation/correction needed, independent of radiative heating?

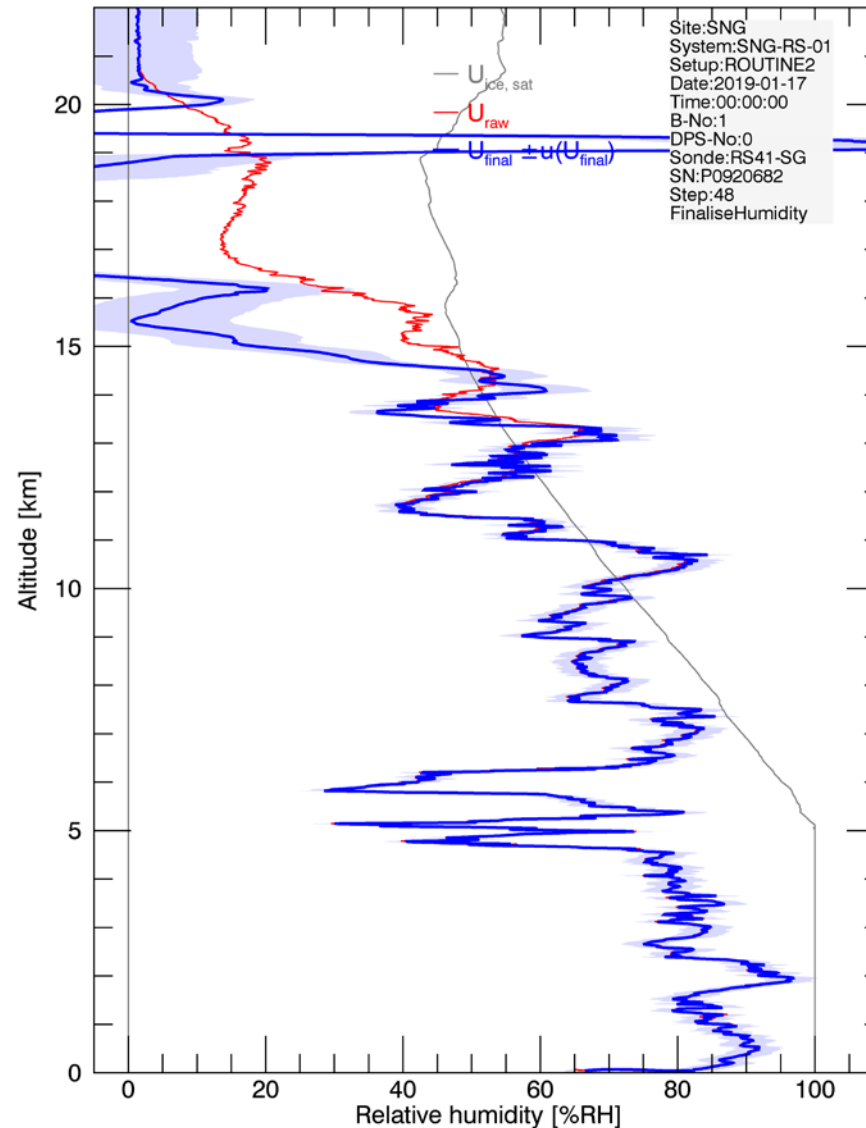


$p = 6 \text{ hPa}$, $\text{SEA} = 53^\circ$, $I_a = 1156 \text{ W} \cdot \text{m}^2$, v variable



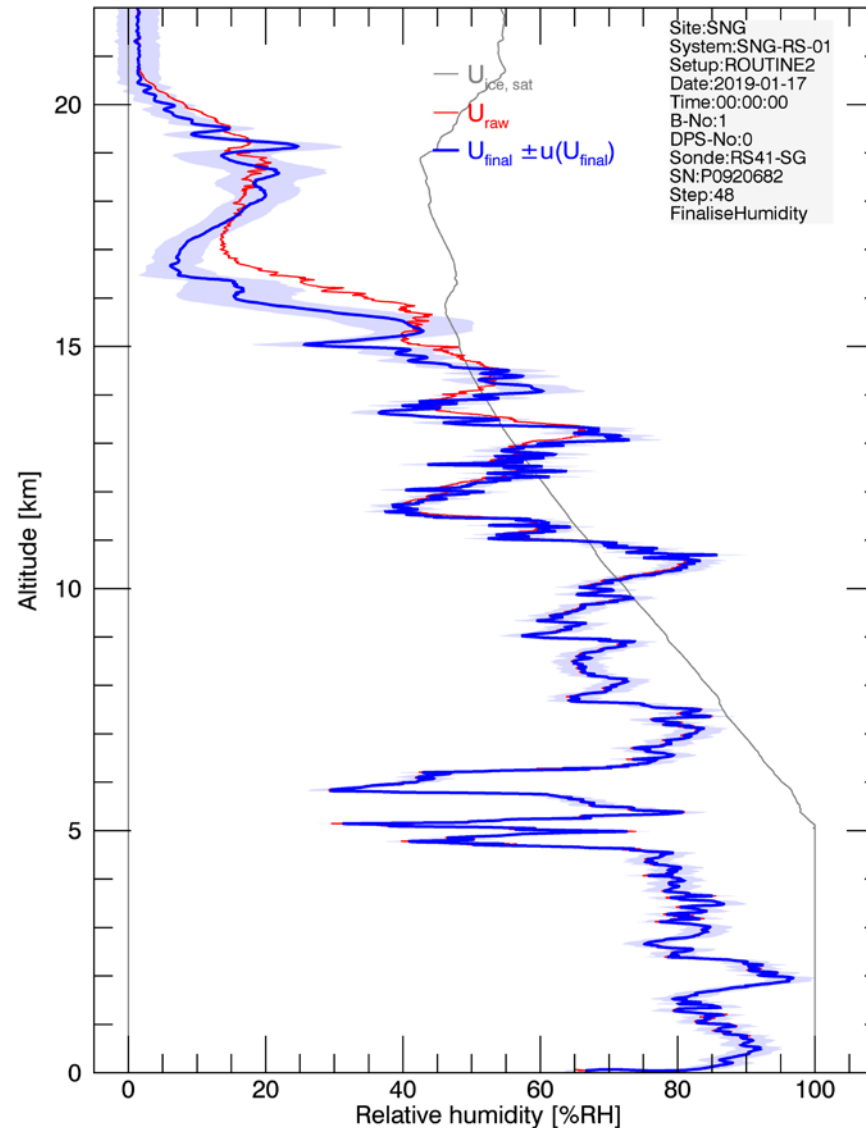
(II) RH Time lag RS41: Example (RS41-GDP-**ALPHA.3**)

SNG, 2019-01-17, 00:00:00, Rel. Humidity (after conversion to air temperature)



(II) RH Time lag RS41: Example (RS41 GDP v. ALPHA.3)

SNG, 2019-01-17, 00:00:00, Rel. humidity



(II) RH Time lag RS41: Results

- U -sensor kept ~ 5 K above ambient air
 - τ derived for 'internal' U
 - τ related to 'internal' T (T of U -sensor)
- U -steps accompanied by (undesired) T -steps

