



Radiation experiments with radiosondes: Current status

Christoph von Rohden
GRUAN Lead Centre, DWD

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- Sensor warming ΔT (shortwave solar radiation)
- Evidence from observations
- Quantitative estimate of ΔT
 - Chamber experiments
 - Approach for radiation correction of temperature in soundings
 - Discussion of shortcomings / limitations
- New experimental setup
- Conclusions

Effect of short wave solar radiation on sonde temperature sensors (ΔT)

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Wetter und Klima aus einer Hand

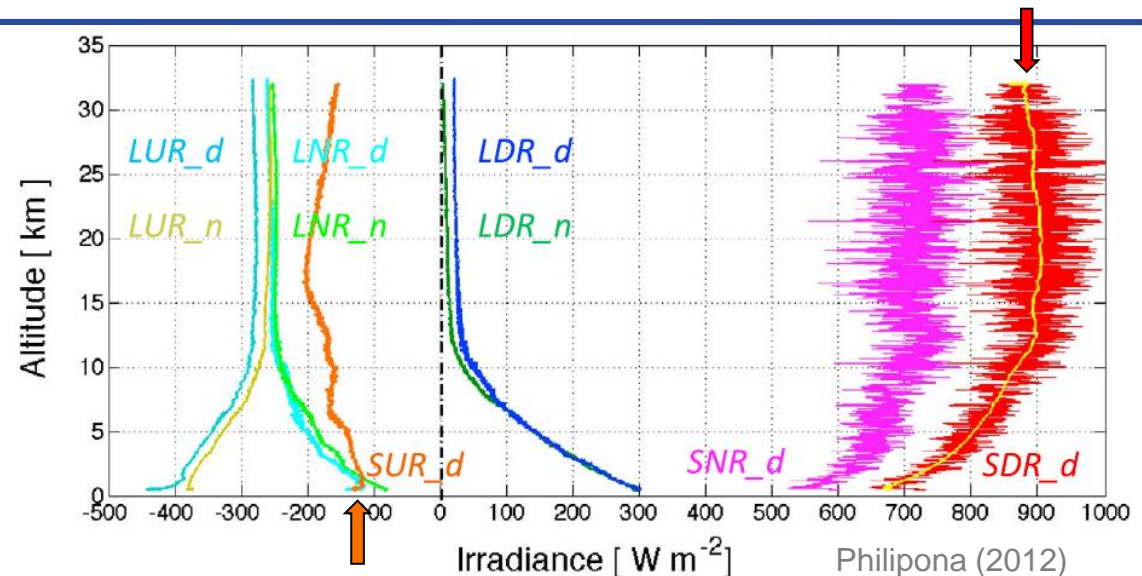


Shortwave (solar) radiation

- | | |
|--------------------------------------|-------------------------------------|
| Downwards (\downarrow) | Upwards (\uparrow),
(albedo) |
| - direct | |
| - diffuse
(small in stratosphere) | - diffuse |

Actual T -bias (warming) result of:

- Magnitude of actinic flux ($\downarrow + \uparrow$)
- Surface and material properties:
 - reflectance, thermal conductivity, shape (boom & sensor)
 - differential warming, conduction,
 - complex response (more than one time constant)
- Heat exchange with air (ventilation)
 - air density (altitude)
 - ascent speed
 - most of all cooling
- Direction of irradiation:
 - SEA
 - angle of sensor boom
 - azimuth angle (rotational motion)
 - deflection angle (pendulum motion)
- Longwave cooling (?)



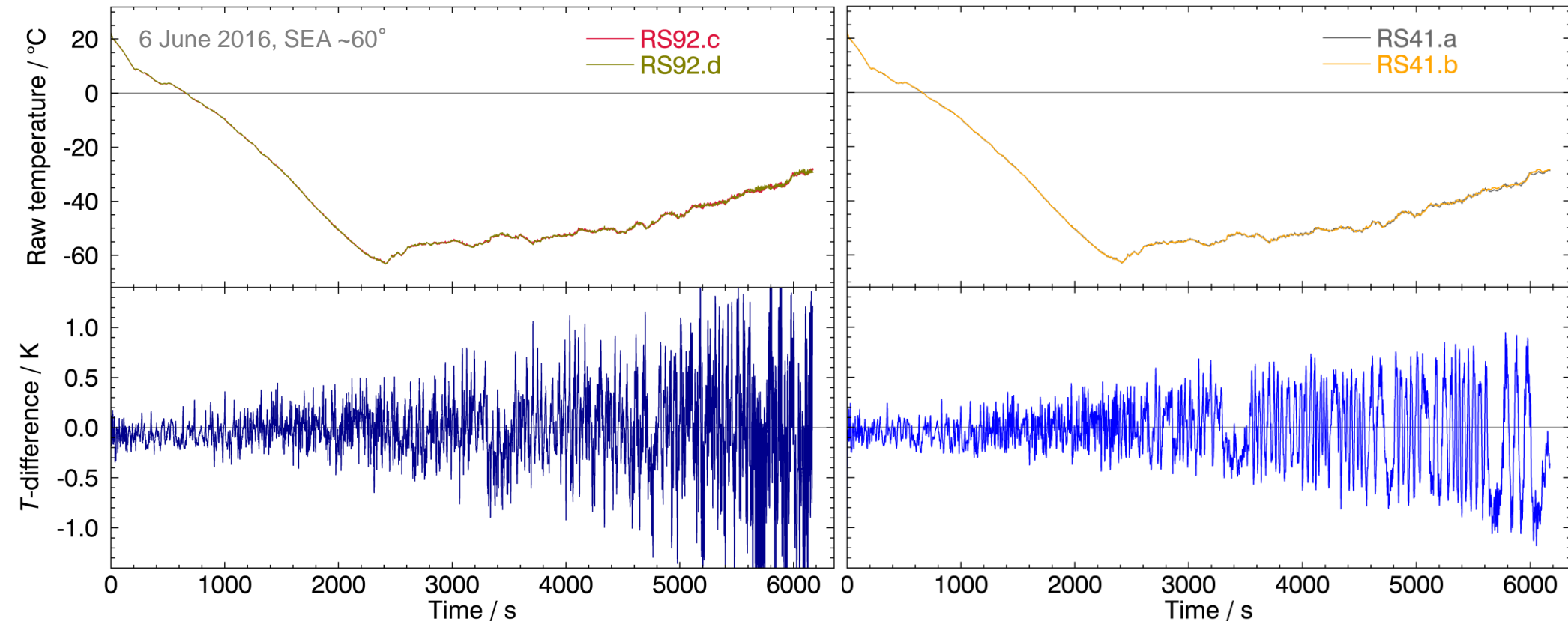
→ Lack of information to calc. T -bias by solving heat balance equation

→ Semi-empirical approach for average bias as function of known parameters (I_a, v, p)

→ Laboratory measurements as quantitative basis

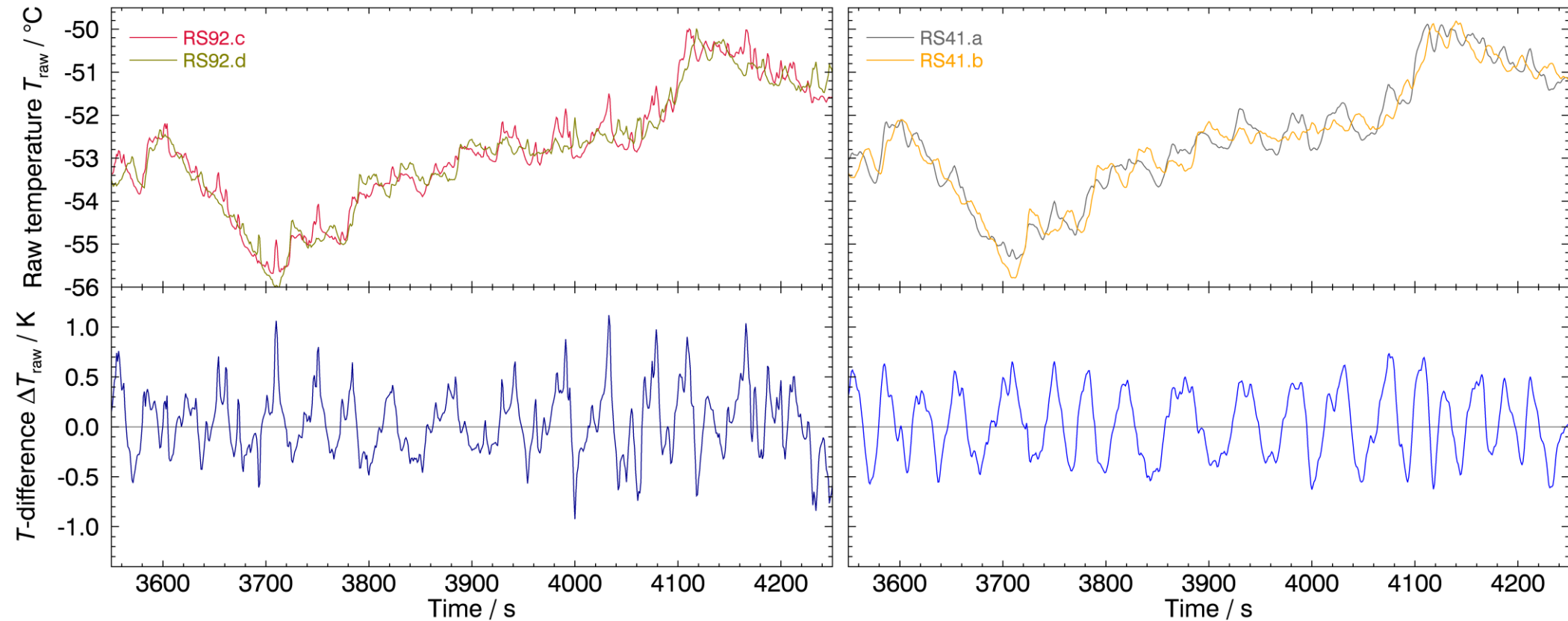


Orientation dependence of T -effect with direct solar irradiation, dual flight, sensors facing in opposite direction



- T -differences up to **1.5 K** for **RS92**, **1 K** for **RS41**, caused by different orientations relative to sun
- Absolute T -bias may be larger (includes warming from diffuse radiation)

Orientation dependence of T -effect with direct solar irradiation, dual flight, sensors facing in opposite direction

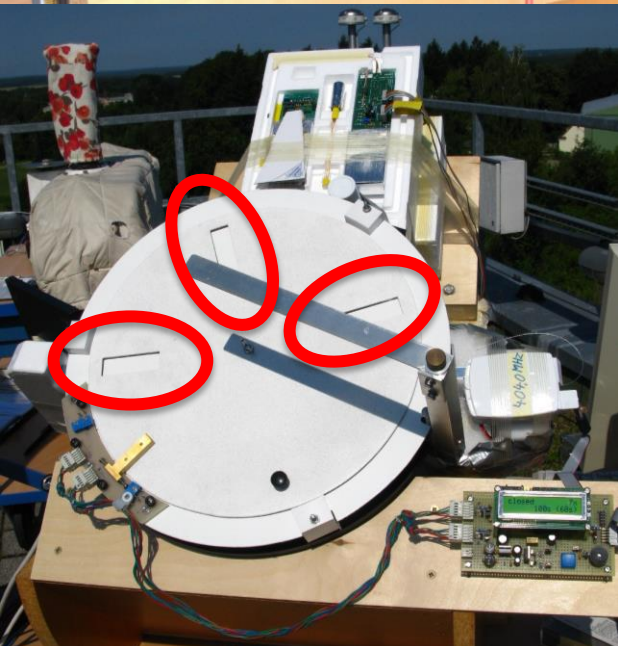
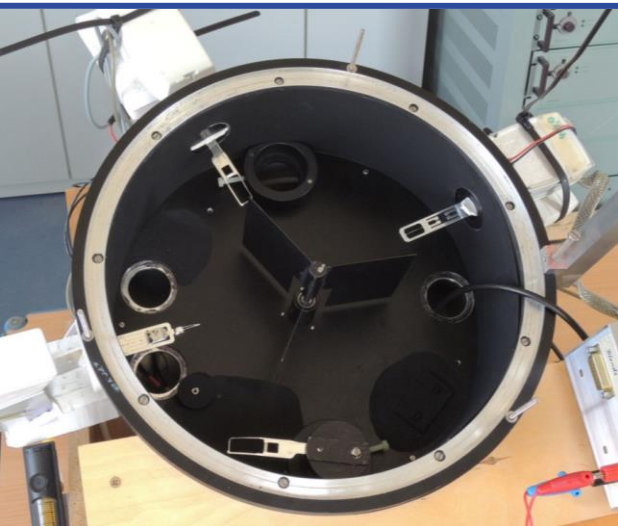


- Two types of rig movements (rotation, pendulum)
- Different temporal responses of RS92 and RS41

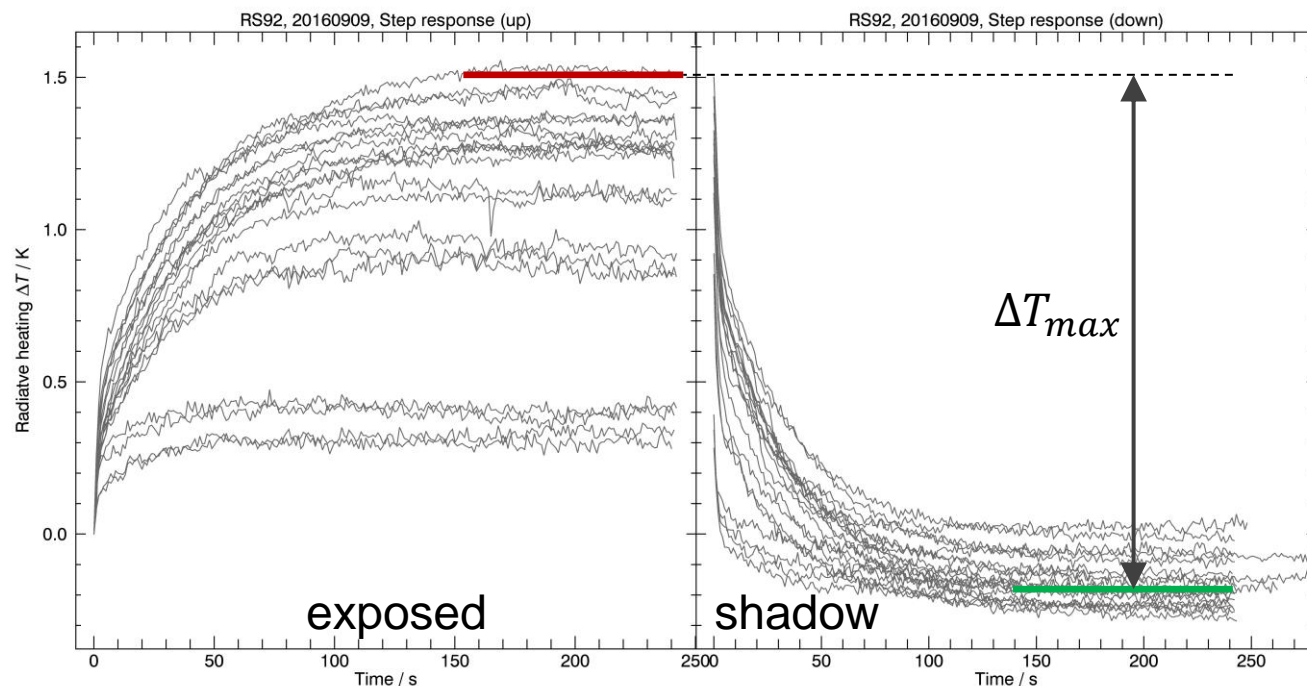
Experimental approach

Lindenberg radiation chamber

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- Sun as light source (direct)
- Vertical irradiation, major part of sensor boom
- Controlled parameters:
 - Irradiance I : (200–1000) $\text{W}\cdot\text{m}^{-2}$
 - Pressure p : (3–1020) hPa
 - Ventilation v : (0–10) $\text{m}\cdot\text{s}^{-1}$
- $\Delta T_{max} = T(\text{test sonde}) - T(\text{reference sonde, shadow})$
(thermal equilibrium)



Radiation correction, initial approach

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- Lab experiments:

$$\Delta T_{max}(I, p, v) = a \cdot \left(\frac{I}{p^j \cdot v^k} \right)^b$$

a, b, j, k from fits to experimental data

- Relate exp. results to conditions during soundings:

- Separate components of actinic flux (I_{dir}, I_{diff})
(RS92 GDP: Streamer model, representative scenario)
- Sonde rotation: Scaling of I_{dir} with effective *average* surface A of sensor boom exposed to sun

$$I_a = I_{diff} + f_{geo} \cdot I_{dir}$$

- T-bias (correction): $\Delta T = a \cdot \left(\frac{I_a}{p^j \cdot v^k} \right)^b$

- Results:

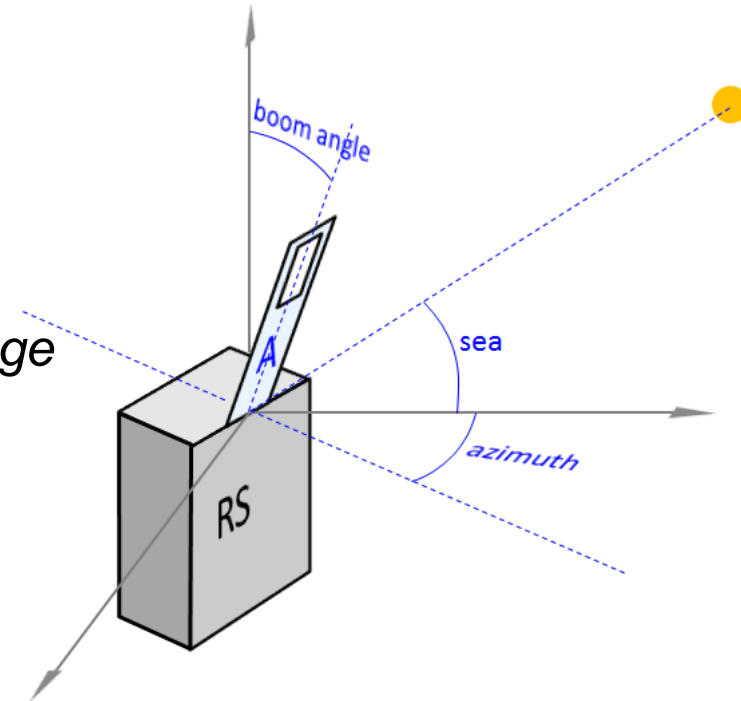
Sonde	RS92	RS41	$p = 10 \text{ hPa},$ $v = 5 \text{ m} \cdot \text{s}^{-1},$ $I_a = 1000 \text{ W} \cdot \text{m}^{-2}$
$\Delta T_{max}/K$	2.80	0.89	

→ large for RS92 ($p < 100 \text{ hPa}$)

Inconsistencies: RS92/RS41 dual flights: T -differences after bias correction $>$ raw T -diff.

Day-night comparisons: daytime- T after bias correction $<$ nighttime- T

→ Model assumptions / limitations of experimental setup



Assumptions for actual correction approach:

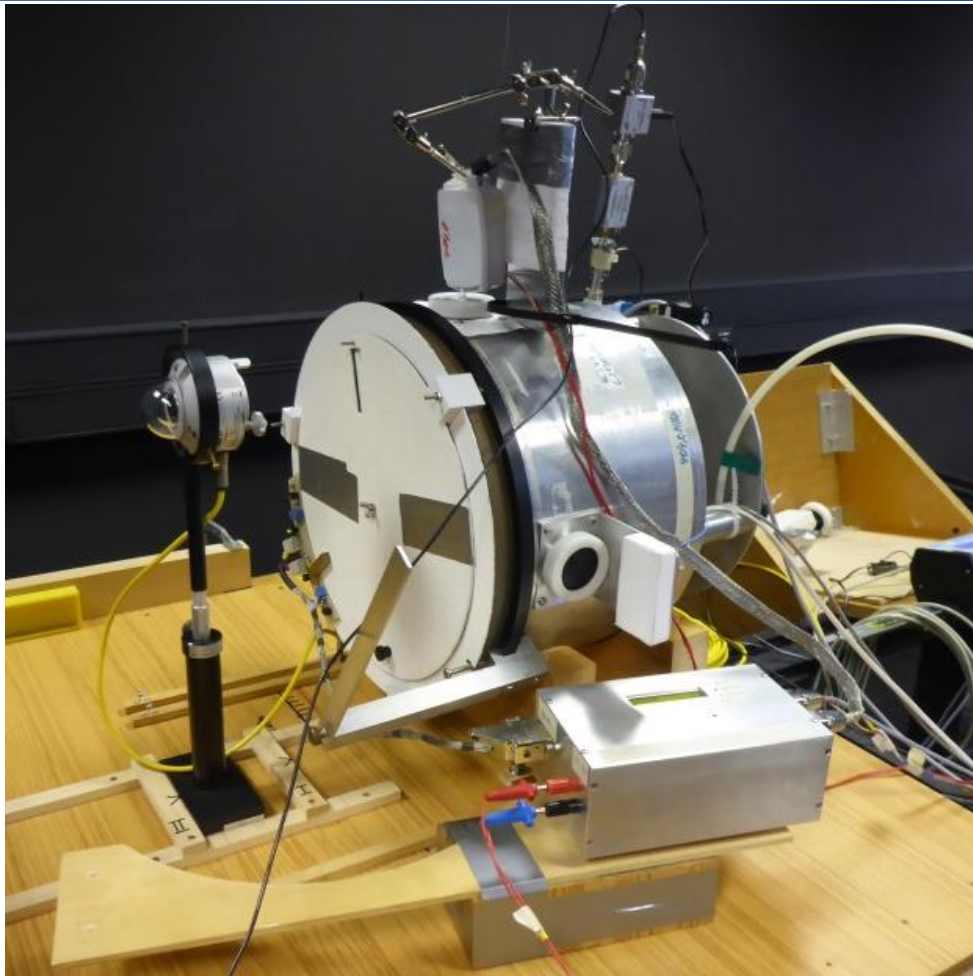
- Uniform response of T -sensor and boom to radiation (\rightarrow use of f_{geo})
 - Top and bottom side of boom behave the same
- I_a (modelled actinic flux during sounding) can directly be related to I_{exp}
- Response the *same* for *diffuse and direct radiation*
- Warming by diffuse radiation *independent of orientation*
- **Not taken into account:** Temporal response
(T -sensor not in thermal equilibrium!);
pendulum motion; effects by thermal radiation

Technical/conceptual limitations of experimental setup:

- Radiation incident angle fixed (vertical) (*next slides*); single side
- Air flow: direction not sufficiently well defined (mainly lateral);
magnitude controlled by fan voltage (not stable)
- No tests with diffuse radiation
- Tests at ~ 300 K (no simulation of cold atmospheric temp.)

Latest experimental results (lab): ΔT as function of angle of radiation incidence

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- Xe-lamp
- $I_a = 1478 \text{ W} \cdot \text{m}^{-2}$
- $v = 5 \text{ m} \cdot \text{s}^{-1}$
- $p = 9.6 \text{ hPa}$

a) Irradiation
of sensor
boom

RS92

RS41

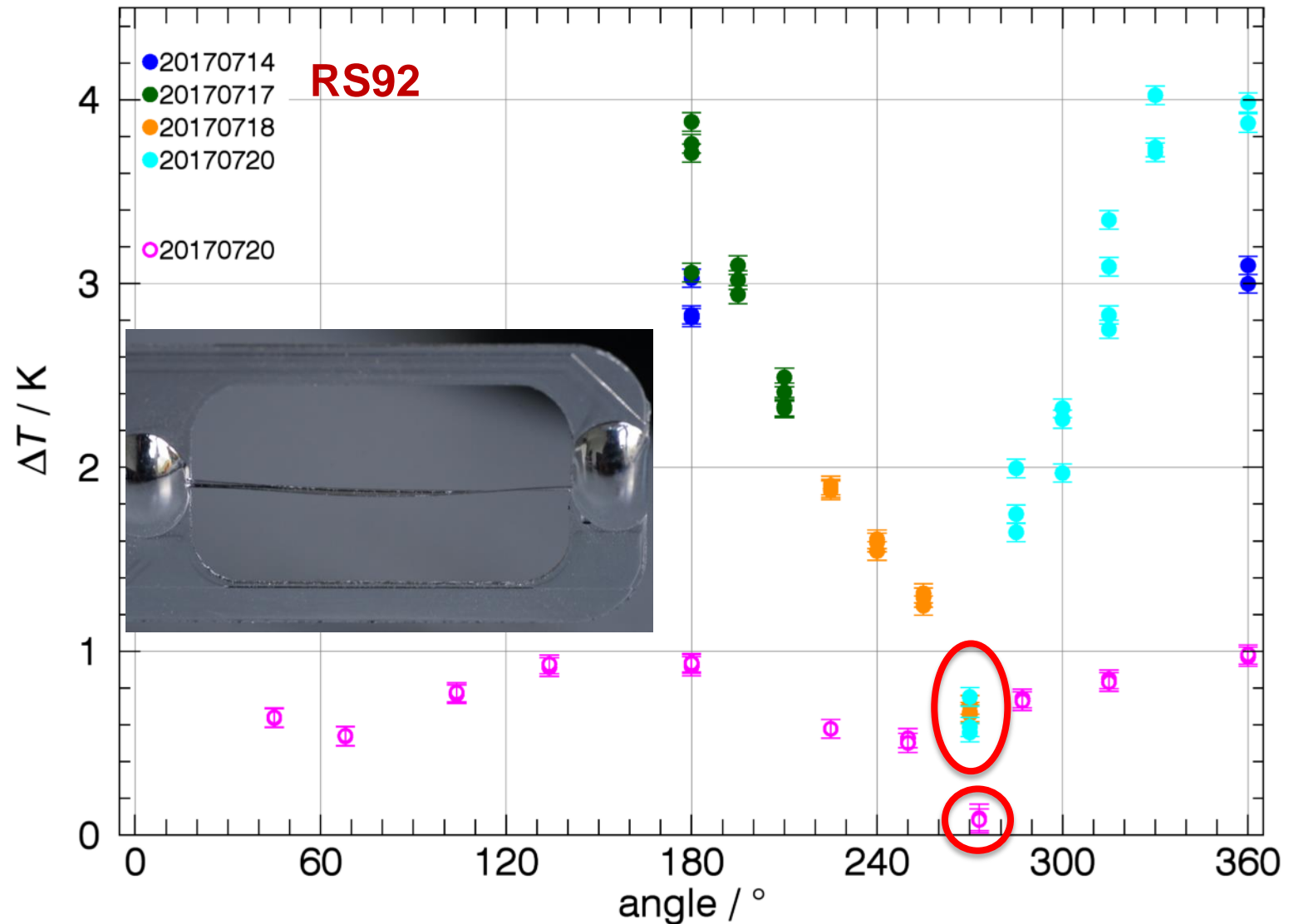


b) Irradiation
of sensor
element only



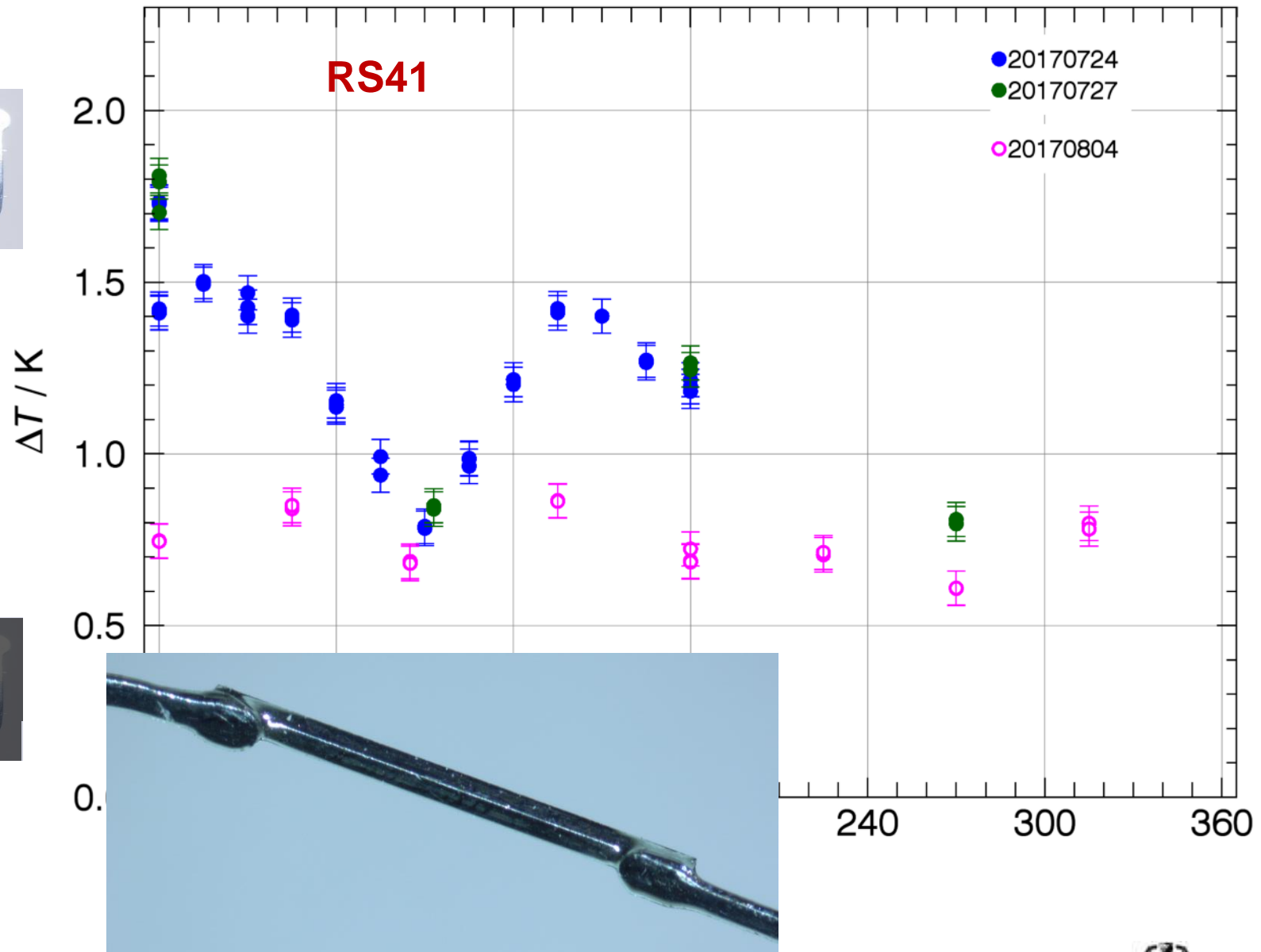
Latest experimental results: ΔT as function of angle of radiation incidence

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Latest experimental results: ΔT as function of angle of radiation incidence

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Latest experimental results: ΔT as function of angle of radiation incidence

Results:

- Minor part of variation in ΔT due to shape of sensor element
 - Major part from radiative response and shape of boom;
boom acts as *heat source* for sensor element (*heat conduction*)
- Care! Flow resistance of boom (i.e. cooling rate) and effective irradiation simultaneously changed with varying sonde angle (not separable)!
- Experiment: Steady state (thermal equilibrium)
 - Sounding: *changing* conditions (sonde rotation and pendulum motion)
 - Interference of different heat exchange processes in view of sensor (different time constants)



- Design as evacuable wind tunnel
- Larger dimensions: less susceptible to perturbations (T , p , I)
- Quartz glass tube ($l=1$ m, $\varnothing 180$ mm) as test volume: installation boom + electronics + dummy corpus; can be radiated through (less absorption); tests with direct & diffuse light
- Air flow: parallel stream lines; realistic boom ventilation; control by fan revolution
- Variable angles of incident radiation: free rotation of sonde (azimuth), simulation of SEA

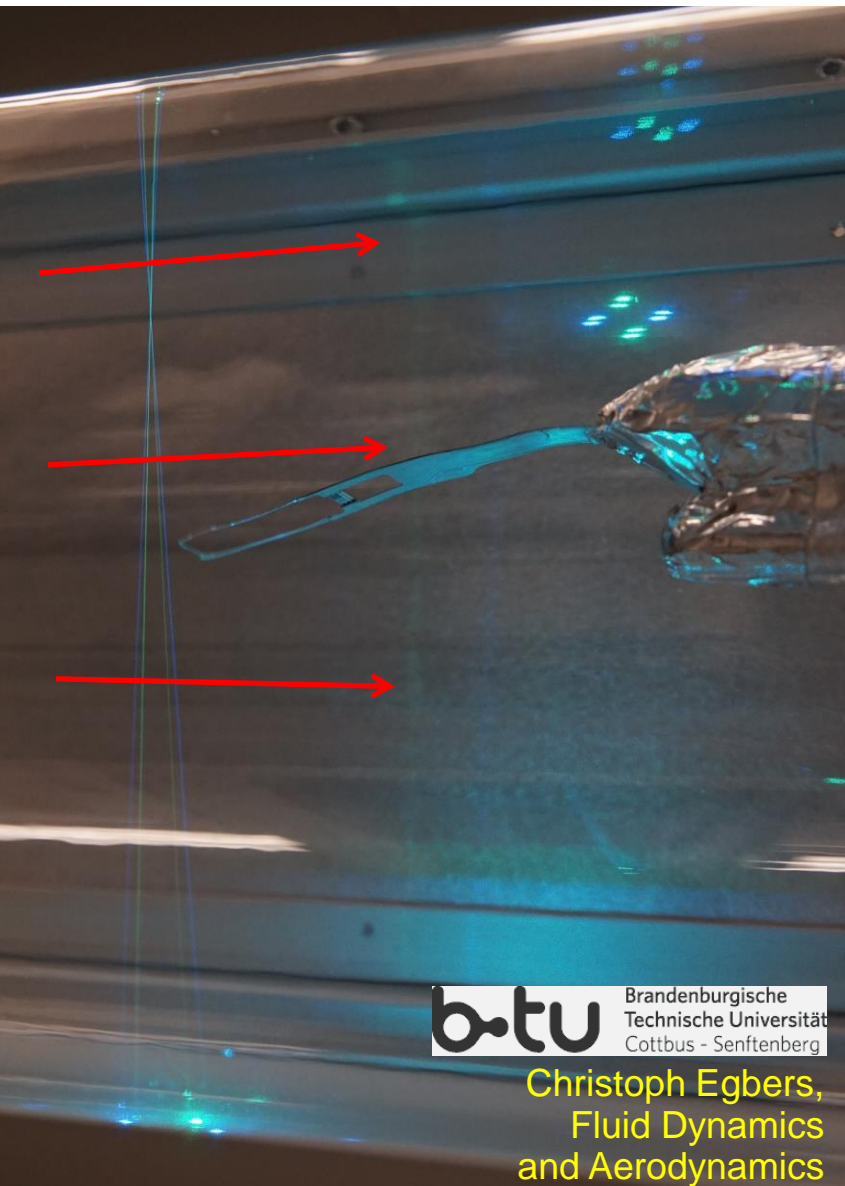
**Overall: more realistic simulation of ascent conditions;
independent testing for individual parameters**

New experimental setup

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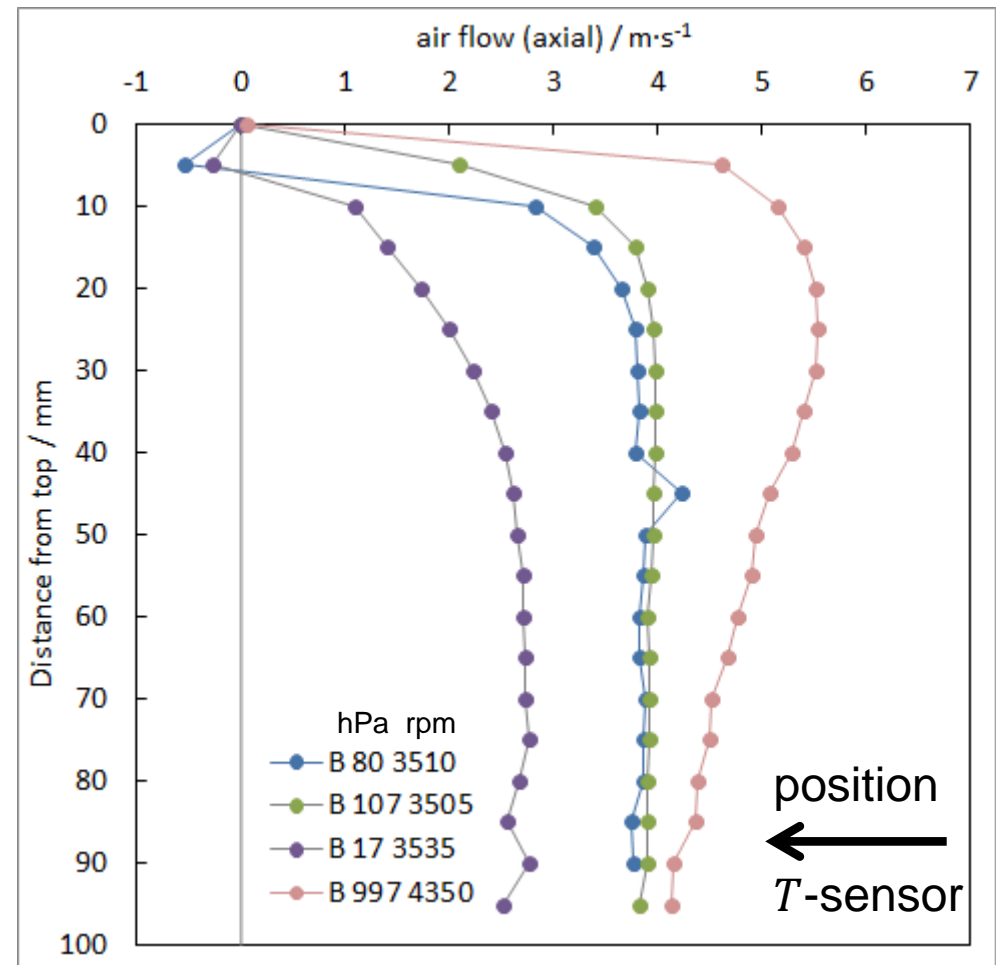
Characterization of flow field
(Laser Doppler Anemometry)



b-tu Brandenburgische
Technische Universität
Cottbus - Senftenberg

Christoph Egbers,
Fluid Dynamics
and Aerodynamics

First test of functionality and
shape of flow profile



- GRUAN radiation correction should rely on independent experiment-based estimates of T -effect
- Work with “old” chamber: **experience**; **limitations**
→ Development of new experimental setup
- “New” experiments:
 - Can results from “old” chamber be reproduced?
 - Include sonde rotation in testing (dynamic measurement)
 - Compare effects for diffuse and direct irradiation
- Correction model:
 - How to average over sonde rotations (to derive “effective” T -bias)?
 - How to estimate orientation-derived *uncertainty of T -bias*?
(= largest uncertainty contribution in RS92 GDP!)
- Time line:
 - Characterization of flow field (LDA) finished in May 2018
 - First measurements planned for Spring/Summer 2018

Thank you for your attention